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A SUBSIDIARY OF

Ford Motor Company

WDL DIVISION

PALO ALTO, CALIFORNIA

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**PROGRAMMER'S MANUAL FOR INTERPLANETARY
ERROR PROPAGATION PROGRAM**

Prepared by

PHILCO CORPORATION
A Subsidiary of Ford Motor Company
WDL Division
Palo Alto, California

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NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
GODDARD SPACE FLIGHT CENTER
Greenbelt, Maryland

ABSTRACT

WDL-TR2184
PROGRAMMER'S MANUAL FOR
INTERPLANETARY ERROR PROPAGATION PROGRAM
15 November 1963

UNCLASSIFIED

420 pages
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15732

This report discusses the subroutines that are used in the Interplanetary Error Propagation Program. A narrative description and card listing are provided for each subroutine; flow diagrams are included, if applicable. A listing of assigned locations in common is also presented.

Author

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FOREWORD

This report is submitted to the National Aeronautics and Space Administration, Goddard Space Flight Center, in fulfilling the requirements of Contract NAS 5-3342.

The documentation provided by Philco WDL in support of the Interplanetary Error Propagation Program consists of the following three volumes:

- WDL-TR2184, "Programmer's Manual for Interplanetary Error Propagation Program"
- WDL-TR2185, "User's Manual for Interplanetary Error Propagation Program"
- Guidance and Control System Engineering Department Technical Report No. 4, "The application of State Space Methods to Navigation Problems," by Stanley F. Schmidt

These volumes discuss the theory of the Schmidt-Kalman filter used in the program for data smoothing, the manner in which the program is used, and subroutine description and listing.

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PROGRAM SUBROUTINE LISTING

ARKTNS	Single Precision Arctangent
ARKTAN	Double Precision Arctangent
ASINH(X)	Function Evaluation
BODY	Calculates Accelerations Due to Perturbing Bodies
BVEC	Calculates B Vector
CHNGP	Determines when to Shift Body Center
COMPHQ	Computations for ONBTR and MONBTR Subroutines
CONST1	Array of Input Constants
CONVPI	Converts Input Covariance Matrix to 1950
CORRTP	Updates P Matrix
CROSS	Cross Product
(CSH)S	Fortran II Card Image Input Subroutine
DE6FN	Fap Integration Subroutine
DOT	Function Forming Dot Product
EARTR	Updates Covariance Matrix for Earth Based Tracking
ECLIP	Transforms Coordinates through Transformations
ENCKE	Calculates Perturbation due to Deviation from CONIC
ERP	Prints Out Ephemeris Error
ERPT	Prints Out Time of Ephemeris Error
FINP	Data Input Subroutine
FNORM	Norm of A Vector
GHA	Greenwich Hour Angle
GOTOB	Main Subroutine for Integration of Trajectories
GOTOR	Iterates to Solve Kepler's Equation
GUID	Performs Guidance Calculations
HOURL	Reads Printer Clock
HPHT	Performs Matrix Multiplication H*P*HT
INPUT	Converts Inputs to Equinox of 1950 Reference
INTR	FAP Ephemeris Subroutine
INV3	Inverts Up to a 6 By 6 Matrix
INVAO	Forms Inverse of Transition Matrix
LOADO	Obtains Transition Matrix From T Array

LOADT	Puts Unit ICS On Perturbation Equations
MASS	Arranges Gravitational Constants of Bodies Considered
MATRX	Multiplies $A*B=C$ or $A*B*AT=C$ Max Dimension (10.10)
MATSUB	Error Propagation Logic Subroutine
MNA	Transformation to Selenocentric Coordinates
MNAND	Transformation for Selenocentric Velocities
MONBTR	Updates Covariance Matrix for Moon Beacons
MULT	Multiplies Two 3 by 3 Matrices
NUTAIT	Calculates Nutation Matrix
OBLN	Calculates Acceleration Due to Oblateness
ONBTR	Updates Covariance Matrix for Onboard Tracking
ORTC	Outputs Orbital Parameters
OUTC	Outputs Trajectory
OUTDAT	Outputs Calendar Date
OUTP	Outputs RMS Values of Orbital Parameters
PTRAN	Transforms P Matrix
RETRO	Performs Retro Fire
ROTATE	Calculates Transformation for Rotation About an Axis
ROTEQ	Calculates Matrix from Equinox 1950 to Mean Equinox of Date
RVIN	Transforms Coordinates From Spherical to Cartesian
RVOUT	Transforms Coordinates from Cartesian to Spherical
SDEC	Second Derivative Subroutine
SETN	Set Read and Write Tape Numbers
SHIFTP	Shifts Body Center
STPC	Move Along Conic in Time
TIMEC	Converts Calendar Date to Days from 1950
TIMED	Converts Days Hours Min Sec to Seconds
TRAC	Tracking Station Coordinates
TRANSH	Transforms H Matrix From Date to 1950

WDL-TR2184

PROGRAMMER'S MANUAL FOR INTERPLANETARY ERROR
PROPAGATION PROGRAM

SECTION 1

INTRODUCTION

1.1 GENERAL

This manual contains subroutine descriptions, logic, and FORTRAN listings for the Interplanetary Error Propagation Program. Listings of the quantities which are in the four common storage arrays (T,S,C, and IC) are also included.

1.2 GENERAL DESCRIPTION OF METHOD OF ORBIT DETERMINATION USED IN PROGRAM

The classical approach to the determination of an orbit from tracking data is the maximum likelihood, least-squares technique. This program uses a different approach to this problem. The relationships between the observed tracking data and the initial conditions (or an equivalent set of parameters) which determine the orbit are highly nonlinear. Therefore, it is assumed that a preliminary estimate of the initial conditions and, therefore, the orbit, is known. The equations are then linearized about this "nominal" orbit and an adjustment to the nominal orbit found from the differences between the observed tracking data and the predicted tracking data based on the nominal orbit. In the least-squares technique, the data is processed in parallel in the sense that the normal equations are summed over all the available tracking data before a modification to the nominal orbit is determined.

The Schmidt-Kalman technique differs from the classical least-squares approach in two ways: first, the estimate used is based upon the minimization of a risk function different from that used in the least-squares approach and, second, the data is processed serially instead of in parallel. The Schmidt-Kalman technique depends upon a linearization of the relations between the orbit parameters and the observed tracking data. Therefore, it assumes some nominal trajectory and an associated error estimate (covariance matrix) for the nominal trajectory.

GENERAL FLOW DIAGRAM
OF OVERALL ERROR PROPAGATION PROGRAM

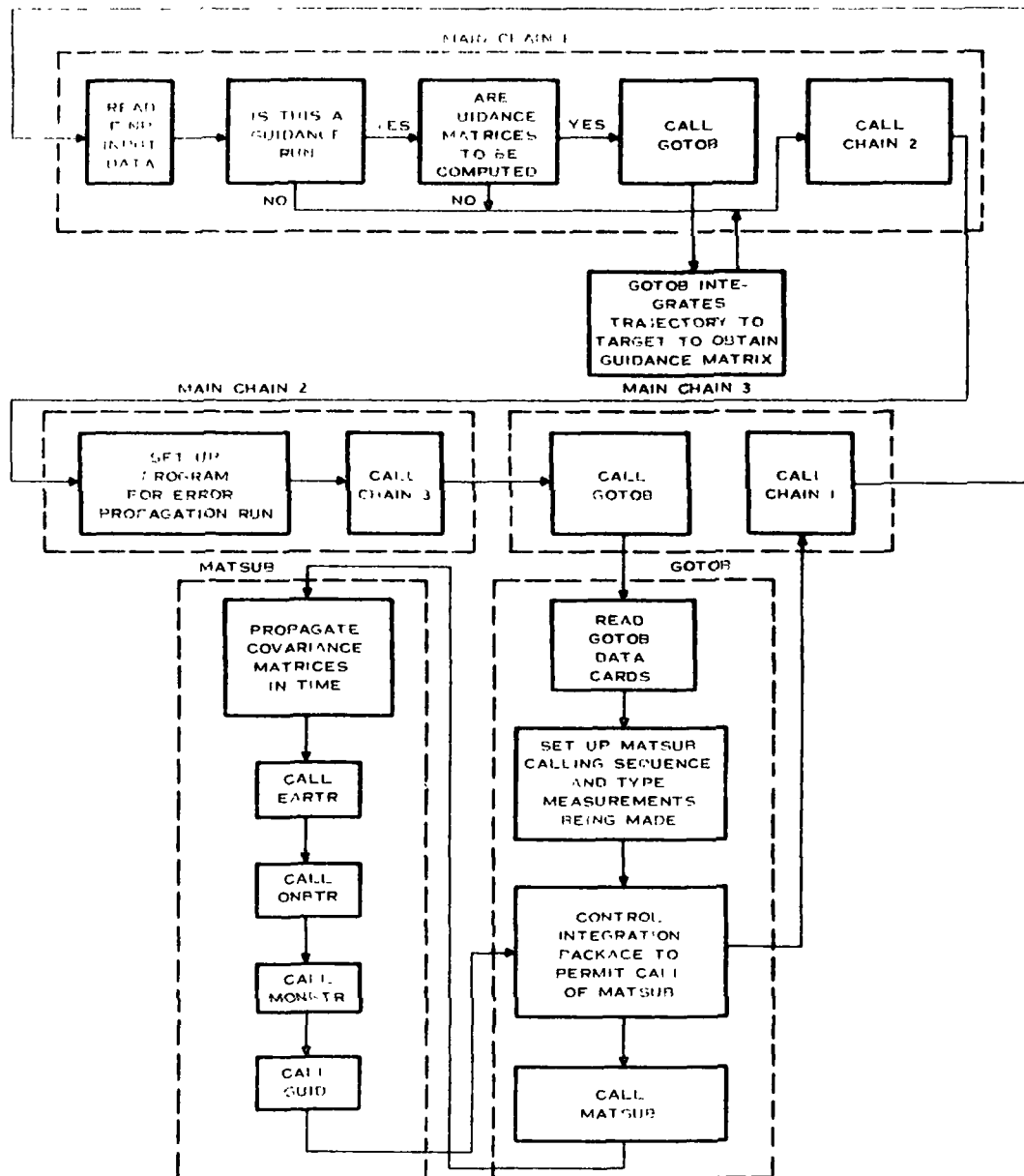


Figure 1-1

The serial processing of the tracking data and associated updating of the nominal orbit occurs as follows: At the start of the time period for which tracking data are to be processed and an improved estimate of the orbit is to be obtained, it is assumed that an estimate of the orbit (a set of state variables) and an error estimate exist. Both of these estimates are updated to an instant of time when tracking data are available. Based upon the available tracking data at this time, a revised estimate of the nominal trajectory is obtained together with a revised estimate of the associated covariance matrix. These two estimates are then propagated along the orbit until additional tracking data become available. In this way, the orbit is updated and tracking data are processed serially.

1.3 GENERAL PROGRAM DESCRIPTION

This program is capable of error studies and their propagation along lunar and planetary trajectories. The design of the program is such as to facilitate the accurate and rapid evaluation of tracking systems for a given lunar or interplanetary trajectory. The program is also able to analyze the errors based on ground tracking as well as on-board tracking independently and in combination. The program has the option to calculate the errors and their projection to the target planets for a probe or a spacecraft based on the following type of measurements.

a. Earth-based tracking

1. Range
2. Range rate
3. Azimuth
4. Elevation
5. Minitrack data

b. On-board tracking

1. Right ascension
2. Declination
3. Range
4. Range rate
5. Range and range rate from beacons on the target planets.

The program is also capable of propagating guidance covariance matrices along the nominal trajectory. The program has the facility of using two types of guidance laws: (1) Fixed time of arrival, and (2) Variable time of arrival with the constraint that the energy with respect to the target be held constant.

The program is composed of three chains. Each link is complete in itself; that is, each contains a main program and all necessary sub-routines. Control is passed from one link to the next by the CALL CHAIN statement. The program requires an ephemeris tape for operation. Figure 1-1 shows a general block diagram of the flow through the program.

The following tables show the assigned locations in "common storage":

Table 1-1:	"C" Array	-----	Floating Point Variables
Table 1-2:	"S" Array	-----	Floating Point Constants
Table 1-3:	"IC" Array	-----	Fixed Point Variables
Table 1-4:	"T" Array	-----	Storage for Integration Routine

TABLE 1-1

LIST OF ASSIGNED QUANTITIES IN COMMON "C" ARRAY

DIMENSION 1000			
CELL	FORTTRAN NAME	DIMENSION	DESCRIPTION
C(10)	TW		Whole days from 1950 at last rectification
C(11)	TF		Fractional days from 1950 at last rectification
C(12)	TSECO		Time in seconds at last rectification
C(13)	TP1		Time in whole days
C(14)	TP2		Time in fractional days
C(15)	XP	(3)	X, Y, Z, equinox of 1950
C(18)	VXP	(3)	\dot{X} , \dot{Y} , \dot{Z} equinox of 1950
C(21)	AE	(3)	Acceleration due to deviation from conic
C(24)	AO	(3)	Acceleration due to oblateness
C(27)	CA	(3)	Acceleration due to perturbing bodies
C(30)	TSEC		Seconds from start - zero reference time
C(33)	X	(3)	Reference conic X, Y, Z
C(36)	VX	(3)	Reference conic \dot{X} , \dot{Y} , \dot{Z}
C(46)	XSO	(3)	Initial position for STEPC conic
C(49)	VXSO	(3)	Initial velocity for STEPC conic
C(55)	μ		Gravity constant of central body
C(56)	VKB	(6)	Gravitational constants of bodies used
C(62)	PO	(22)	Ephemeris positions of bodies
C(84)	VE	(22)	Ephemeris velocities of bodies
C(106)	RBO	(6)	Distances to bodies

DIMENSION 1000			
CELL	FORTTRAN NAME	DIMENSION	DESCRIPTION
C(112)	RBOP	(6)	Distances to bodies
C(120)	EN	(3,3)	Nutation matrix
C(129)	EA	(3,3)	Transformation from 1950 to mean equinox of date
C(138)	AN	(3,3)	Transformation from 1950 to true equator of date
C(147)	ECL	(3,3)	Transformation from 1950 to ecliptic of date
C(156)	ECX	(3)	Position: ecliptic coordinates
C(159)	ECV	(3)	Velocity: ecliptic coordinates
C(162)	BET		Angle from line of nodes to radius vector
C(163)	THT		True anomaly
C(171)	BP	(3,3)	Acceleration partials for use in variational equations
C(180)	SMA		Semi-Major Axis
C(181)	ECC		Eccentricity
C(182)	RCA		Radius of closest approach
C(183)	OINC		Orbital inclination
C(184)	OMG		Longitude of ascending node
C(185)	BEP		Argument of periapsis
C(186)	XED	(3)	Position: equator date
C(189)	VED	(3)	Velocity: equator date
C(192)	RCV	(3)	$\vec{R} \times \vec{v}$
C(195)	RCV2		$ \vec{R} \times \vec{v} ^2$
C(196)	R2		R^2

DIMENSION 1000			
CELL	FORTTRAN NAME	DIMENSION	DESCRIPTION
C(197)	v^2		v^2
C(198)	RDV		$\frac{1}{R} \cdot \frac{1}{v}$
C(199)	C3		$C_3 = v^2 - \frac{2u}{R}$
C(460)	PFTA	(6,6)	Deviation From Nominal Covariance Matrix
C(568)	TRANS	(3,6)	Guidance partial matrix being used on runs
C(622)	TLAST	(4,6)	Delta time since last observation in ONBTR
C(647)	TOUT		Time to output for MATSUB
C(648)	TGUIDE		Time to make guidance correction
C(649)	TSECP		LAST TIME through MATSUB
C(650)	TPRINT		Output print interval
C(651)	TSTART		Start time
C(652)	P	(6,6)	Knowledge of state covariance matrix
C(752)	AOS	(6,6)	Transition matrix from start to present time
C(788)	STPARS	(3,3)	Station partials MONBTR
C(797)	CIOMP		Compute guidance matrices
C(800)	STPARD	(3,3)	Station partials MONBTR
C(888) } C(900) }			Constants used in COMPHQ
C(973)	OUTPUT	(6)	Data for output purposes

TABLE 1-2

LIST OF ASSIGNED QUANTITIES IN COMMON "S" ARRAY

DIMENSION 1000			
CELL	FORTTRAN NAME	DIMENSION	DESCRIPTION
S(1)			Earth Planetary Mass
S(2)			Moon Planetary Mass
S(3)			Sun Planetary Mass
S(4)			Venus Planetary Mass
S(5)			Mars Planetary Mass
S(6)			Jupiter Planetary Mass
S(7)			SPARE
S(8)			SPARE
S(9)			SPARE
S(10) S(19)			Earth Constants
S(20) S(29)			Moon Constants
S(30) S(39)			Sun Constants
S(40) S(49)			Venus Constants
S(50) S(59)			Mars Constants
S(60) S(69)			Jupiter Constants
S(70)			86400. Conversion factor days to seconds
S(71)			1/86400. Conversion factor seconds to days

DIMENSION 1000			
CELL	FORTTRAN NAME	DIMENSION	DESCRIPTION
S(72)			.017453296 Conversion factor for degrees to radians
S(73)			57.29578 Conversion factor for radians to degrees
S(80)	AT		Launch latitude - degrees
S(81)	ON		Launch longitude - degrees
S(82)	AL		Launch altitude - km.
S(83)	TLTI		Time from launch to injection, days hours. min sec
S(84)	FAZ		Firing azimuth
S(110)	TSTOP		Time to stop calling MATSUB
S(111)	TIM		Type of input
S(112)	DATE		Start date
S(113)	FDATE		Fractional start date
S(114)	CIBDY		Central body
S(115)	X	(3)	Initial position
S(118)	VX	(3)	Initial velocity
S(121)	TIBDY		Target Body
S(122)	OUTTP		Type of output
S(124)	SKTB		Type of stop

EARTH BASED TRACKING DATA

N = 0 - 19

CELL	DESCRIPTION	UNITS
S(125)+N*15	Variance of range	KM ²
S(126)+N*15	Variance of azimuth	RAD ²
S(127)+N*15	Variance of elevation	RAD ²
S(128)+N*15	Variance of range rate	KM ² /SEC ²
S(129)+N*15	Variance of latitude	RAD ²
S(130)+N*15	Variance of longitude	RAD ²
S(131)+N*15	Variance of altitude	KM ²
S(132)+N*15	Variance of azimuth biases	RAD ²
S(133)+N*15	Variance of elevation biases	RAD ²
S(134)+N*15	Latitude of station	DEG
S(135)+N*15	Longitude of station	DEC
S(136)+N*15	Altitude of station	KM
S(137)+N*15	Station name	
S(138)+N*15	Period of observation	SEC
S(139)+N*15	Variance of time bias	SEC ²
S(425)	Velocity of light error	KM ² /SEC ²

ON-BOARD TRACKING DATA

S(426)	Variance of range	KM ²
S(427)	Variance of right ascension	RAD ²
S(428)	Variance of declination	RAD ²
S(429)	Variance of range rate	KM ² /SEC ²
S(430)	Variance of range bias	KM ²
S(431)	Variance of right ascension bias	RAD ²

CELL	DESCRIPTION	UNITS
S(432)	Variance of declination bias	RAD^2
S(433)	Variance of range rate bias	KM^2/SEC^2
S(434)	Variance of clock time bias	SEC^2
S(435)	Spare	
S(436)	Spare	

N = 0 - 5 EARTH, MOON, SUN, VENUS, MARS, JUPITER

CELL	FORTTRAN NAME	DIMENSION	DESCRIPTION	UNITS
S(437)+4*N			Period of range observation	SEC
S(438)+4*N			Period of right ascension Observation	SEC
S(439)+4*N			Period of declination Observation	SEC
S(440)+4*N			Period of range rate Observation	SEC
S(471)			Shutoff Error (Rocket)	$(\%)^2$
S(473)			Pointing Error (Motor)	$(\text{RAD})^2$
S(475)			Type of guidance decision 0-Time + Ratio	
S(476)	TGUID	(6)	Times for guidance correction	
S(483)	GDCOR		Ratio for making guidance correction	
S(484)	DMON		Error in monitoring guidance correction	$(\%)^2$
S(485)	ENKE		Correction criteria for deivation from reference conic	

CELL	FORTRAN NAME	DIMENSION	DESCRIPTION	UNITS
		MOON BEACON TRACKING DATA N = 0 - 9		
S(500)+N*15			Variance of range	KM ²
S(501)+N*15			Variance of right ascension	RAD ²
S(502)+N*15			Variance of declination	RAD ²
S(503)+N*15			Variance of range rate	KM ² /SEC ²
S(504)+N*15			Variance of range bias	KM ²
S(505)+N*15			Variance of right ascension bias	RAD ²
S(506)+N*15			Variance of declination bias	RAD ²
S(507)+N*15			Variance range rate bias	KM ² /SEC ²
S(508)+N*15			Variance clock bias	SEC ²
S(509)+N*15			Latitude of station	DEG
S(510)+N*15			Longitude of station	DEG
S(511)+N*15			Altitude of station	KM
S(512)+N*15			Station name	
S(513)+N*15			Period of observation	SEC
S(514)+N*15			SPARE	
S(650)	PARI	(21)	Initial deviation from nominal covariance matrix	
S(671)	PI	(21)	Initial knowledge of state covariance matrix	
S(720)	PUPIN		Type of coordinates for PI	
S(721)	PARIN		Type of coordinates for PARI	
S(722)	FTA	(3,6)	Guidance transition matrix fixed time arrival	

CELL	FORTTRAN NAME	DIMENSION	DESCRIPTION	UNITS
S(740)	CTE	(3,6)	Guidance transition matrix constant energy WRT* target	

MOON BEACON DATA

N = 0 - 9

S(758)+N*3			Variance of station latitude	RAD ²
S(759)+N*3			Variance of station longitude	RAD ²
S(760)+N*3			Variance of station altitude	KM ²

EARTH BASED TRACKING DATA

N = 0 - 19

S(788)+N*5			Tracking Station horizon	RAD
S(789)+N*5			Variance of M dircos	
S(790)+N*5			Variance of M dircos bias	
S(791)+N*5			Variance of L dircos	
S(792)+N*5			Variance of L dircos bias	
S(888)	RETR		Key to call subroutine RETRO	
S(900)	RAD	(6)	Radius to bodies	
* with respect to				

TABLE 1-3

LIST OF ASSIGNED QUANTITIES IN COMMON "IC" ARRAY

DIMENSION 300			
CELL	FORTTRAN NAME	DIMENSION	DESCRIPTION
IC(1)	N		# of sets of equations
IC(2)	IOR		body center
IC(3)	NOR		new body center
IC(4)	KSTP		type stop
IC(5)	KTYPE		switch indicating type stop
IC(6)	ITARG		target body
IC(7)	KOUT		type of output
IC(8)	IMMSUB		key to test if MATSUB is to be called
IC(10)			+ if tracking station 1 considered
IC(11)			+ if tracking station 2 considered
IC(12)			+ if tracking station 3 considered
.			
.			
.			
.			
IC(29)			+ if station 20 considered
IC(30)			+ range, 0 no range
IC(31)			+ AZ-EL, 0 no AZ-EL
IC(32)			+ dircos, 0 no dircos
IC(33)			+ range rate, 0 no range rate
.			
.			
.			
.			
.			

} Station
1

CELL	FORTTRAN NAME	DIMENSION	DESCRIPTION
IC(106)			+ range, 0 no range
IC(107)			+ AZ-EL, 0 no AZ-EL
IC(108)			+ dircos 0 no dircos
IC(109)			+ range rate, 0 no range rate
IC(110)			Earth observed + yes, 0 no
IC(111)			Moon observed, + yes, 0 no
IC(112)			Sun observed, + yes, 0 no
IC(113)			Venus observed, + yes, 0 no
IC(114)			Mars observed, + yes, 0 no
IC(115)			Jupiter observed, + yes, 0 no
IC(116)			range, + yes, 0 no
IC(117)			rt. ascension, + yes, 0 no
IC(118)			declination, + yes, 0 no
IC(119)			range rate, + yes, 0 no
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.			
.			
IC(136)			range, + yes, 0 no
IC(137)			rt. ascension, + yes, 0 no
IC(138)			declination, + yes, 0 no
IC(139)			range rate, + yes, 0 no
IC(140)			+ Moon beacon station 1
.			0
.			
IC(149)			+ Moon beacon station 10
			0

Station
20

Earth on-board
measurements

Jupiter on-board
measurements

10 Moon beacon
stations

CELL	FORTRAN NAME	DIMENSION	DESCRIPTION
IC(150)			+ range o
IC(151)			+ right ascension o
IC(152)			+ declination o
IC(153)			+ range rate o
.			
.			
.			
.			
.			
IC(186)			+ range o
IC(187)			+ right ascension o
IC(188)			+ declination o
IC(189)			+ range rate o
IC(190)	LSTAT		Key for earth based tracking
IC(191)	LONB		Key for on-board tracking
IC(192)	LMB		Key for moon beacon tracking
IC(193)	IGUID		Positive if guidance run
IC(194)	ISTAT	(20)	Keep account which of 20 trackers saw vehicle last time in MATSUB
IC(214)	NOUT		Output indicator
IC(215)	PUPIN		type of P matrix input
IC(216)	PARIN		type of PAR matrix input
IC(217)	IGDTP		type of guidance
IC(218)	IGDKEY		guidance key set in main
IC(219)	IGD		number of guidance corrections
IC(220)	IMOONB	(20)	Keep account which of 10 moon beacons saw vehicle last time in MATSUB
IC(231)	NSTEP		Key for STEPC

TABLE 1-4
LIST OF ASSIGNED QUANTITIES IN COMMON "T" ARRAY

This is the common storage block for the integration package. See the sub-routine writeup for DE6FN for definitions of the quantities in storage.

DIMENSION 1360			
CELL	DESCRIPTION		
T(1)	N	No. of Equations	} initial conditions which must be supplied
T(2)	X		
T(3)	H	Step Size	
T(4)	y_i	$i = 1, N$	
T(N+4)	y_i'	$i = 1, N$	
T(2N+4)	y_i''	$i = 1, N$	second derivatives stored by V subroutine
T(3N+4)	y_i'	$i = 1, N$	most significant
T(4N+4)	y_i'	$i = 1, N$	least significant
T(5N+4)	$\Delta y_i'$	$i = 1, N$	
T(6N+4)	$\Delta y_i'$	$i = 1, N$	
T(7N+4)	y_i	$i = 1, N$	most significant
T(8N+4)	y_i	$i = 1, N$	least significant
T(9N+4)	y_{i3}	$i = 1, N$	} saved for central difference equations
T(10N+4)	y_{i3}'	$i = 1, N$	

DIMENSION 1360	
CELL	DESCRIPTION
T(11N+4)	y''_{i0} $i = 1, N$
T(12N+4)	y''_{i1} $i = 1, N$
T(13N+4)	y''_{i2} $i = 1, N$
T(14N+4)	y''_{i3} $i = 1, N$
T(15N+4)	y''_{i4} $i = 1, N$
T(16N+4)	y''_{i5} $i = 1, N$
T(17N+4)	y''_{i6} $i = 1, N$
T(18N+4)	used only if coordinates changed.
T(19N+4)	11 N storages. N sets of differences saved for next cowell step.
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.	
.	
.	
T(30N-8)	

MAIN CHAINS

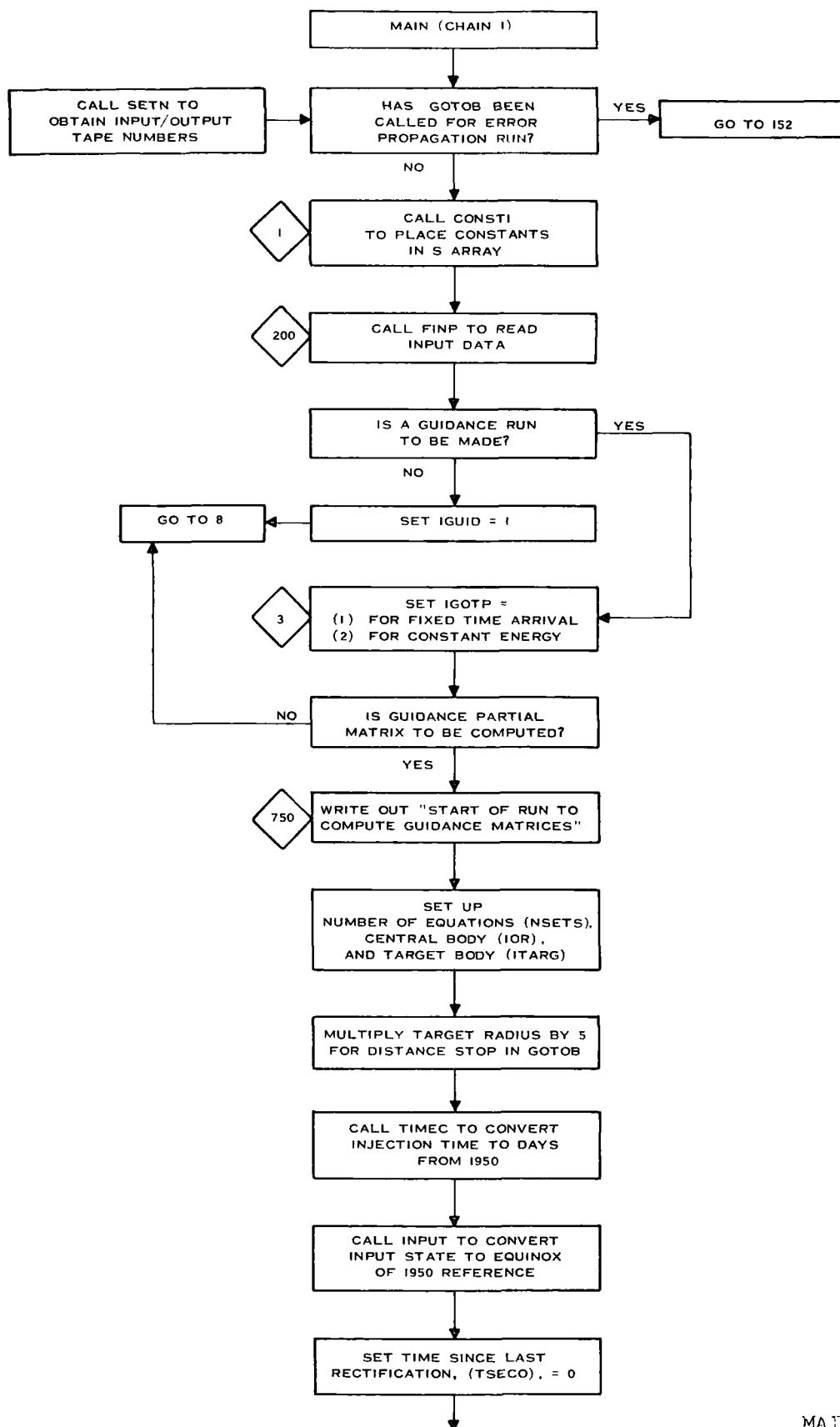
M-1

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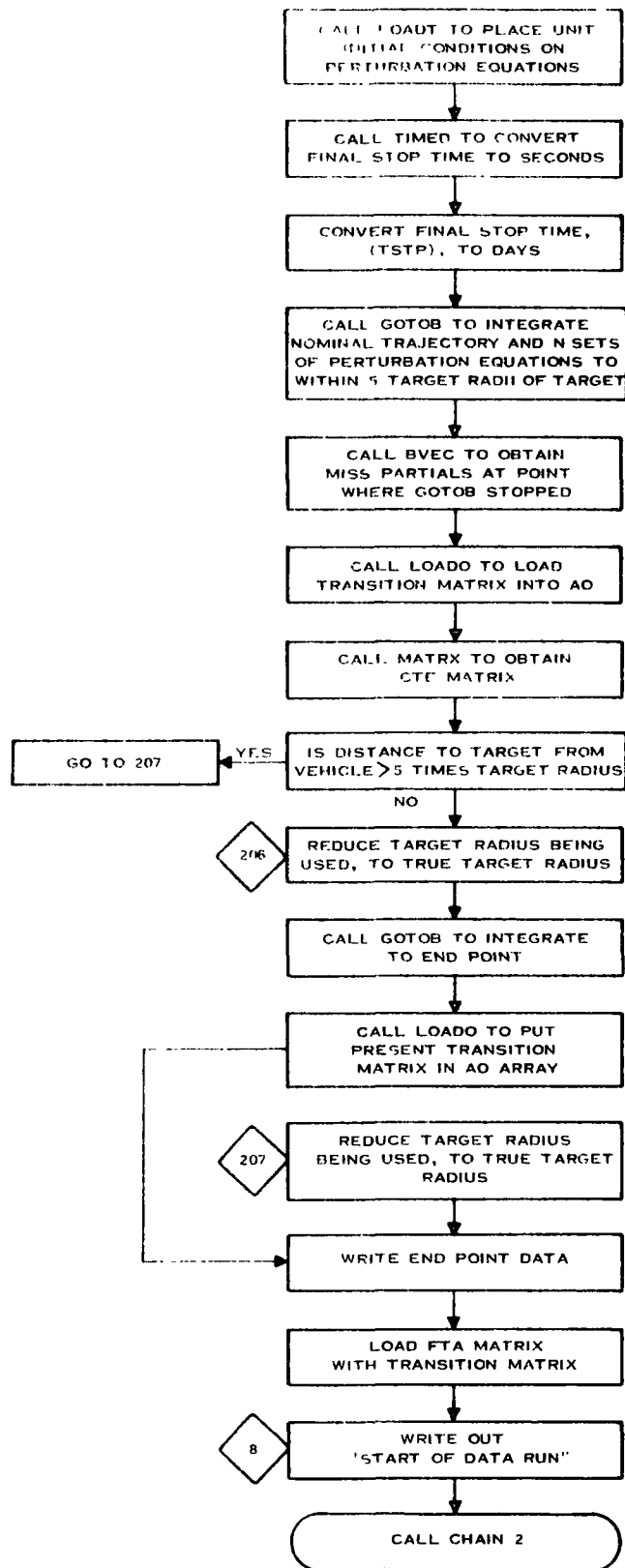
Subroutine: MAIN (Chain 1)

Purpose: Set up program to perform guidance runs to obtain transition and partial matrices. Call Chain 2 for error propagation runs and write out end point data after program returns from Chain 3.

Common storages used or required:	<u>T, S, C, IC</u>
Subroutines required:	<u>BVEC, CHAIN, CONST1, FINP, GOTOB,</u> <u>INPUT, INVAO, LOADO, LOADT, MATRX,</u> <u>RETRO, TIMEC, TIMED</u>
Functions required:	<u>None</u>
Approximate number of storages required:	<u>793 DEC</u>

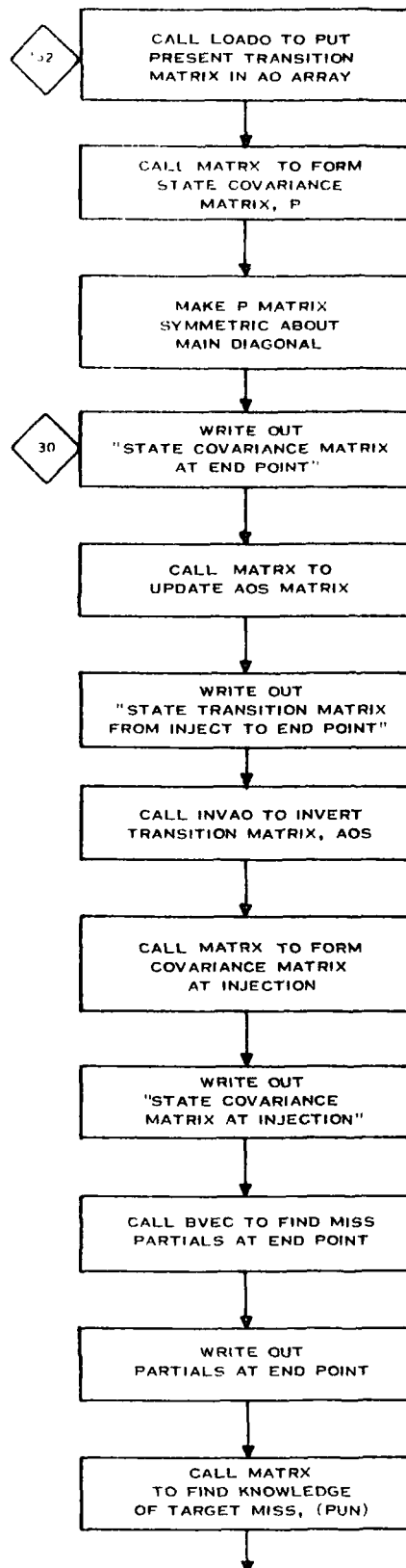


MAIN (CHAIN-1) -2



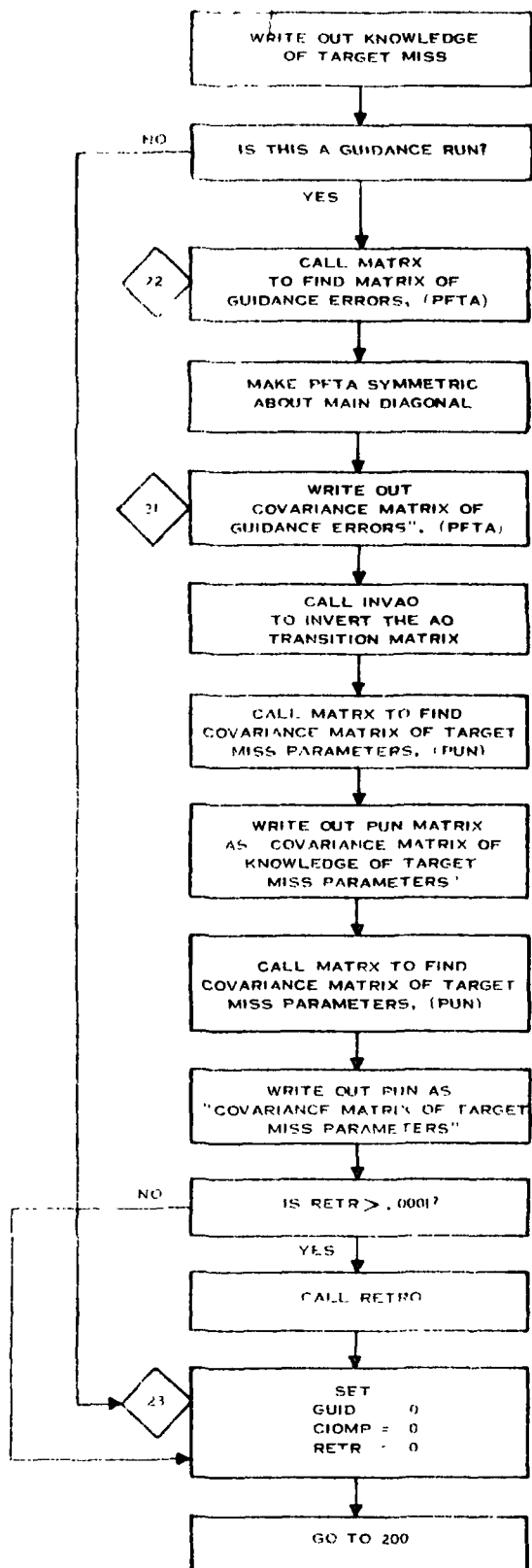
M 5

MAIN (CHAIN-1)-3



M-6

MAIN (CHAIN-1)-4



MAIN (CHAIN 1)

* LABEL		MAI1
CEC20D2	MAIN PROGRAM	MAI10000
C	ERROR PROPAGATION	MAI10010
C	ALONG INTERPLANETARY TRAJECTORIES	MAI10015
C	REQUIRES FOLLOWING SUBROUTINES AND FUNCTIONS	MAI10020
C	ARKTNS SINGLE PRECISION ARCTANGENT	MAI10030
C	ARKTAN DOUBLE PRECISION ARCTANGENT	MAI10040
C	ASINH(X) FUNCTION EVALUATION	MAI10050
C	BODY CALCULATES ACCELERATIONS DUE TO PERTURBING BODIES	MAI10060
C	BVEC CALCULATES B VECTOR	MAI10070
C	CHNGP DETERMINES WHEN TO SHIFT BODY CENTER	MAI10090
C	COMPHQ COMPUTATIONS FOR ONBTR AND MONBTR SUBROUTINES	MAI10095
C	CONST1 ARRAY OF INPUT CONSTANTS	MAI10100
C	CONVPI CONVERTS INPUT COVARIENCE MATRIX TO 1950	MAI10110
C	CORHTP UPDATES P MATRIX	MAI10020
C	CROSS CROSS PRODUCT	MAI10130
C	DOT FUNCTION FORMING DOT PRODUCT	MAI10140
C	DE6FN FAP INTEGRATION SUBROUTINE	MAI10160
C	EARTR UPDATES COVARIANCE MATRIX FOR EARTH BASED TRACKING	MAI10170
C	ECLIP TRANSFORMS COORDINATES THROUGH TRANSFORMATIONS	MAI10180
C	ENCKE CALCULATES PERTURBATION DUE TO DEVIATION FROM CONIC	MAI10190
C	ERP PRINTS OUT EPHEMERIS ERROR	MAI10195
C	ERPT PRINTS OUT TIME OF EPHEMERIS ERROR	MAI10197
C	FINP DATA INPUT SUBROUTINE	MAI10200
C	FNORM NORM OF A VECTOR	MAI10210
C	GHA GREENWICH HOUR ANGLE	MAI10220
C	GOTOB MAIN SUBROUTINE FOR INTEGRATION OF TRAJECTORIES	MAI10230
C	GOTOR ITERATES TO SOVE KEPLERS EQUATION	MAI10235
C	GUID PERFORMS GUIDANCE CALCULATIONS	MAI10240
C	HPHT PERFORMS MATRIX MULTIPLICATION H*P*HT	MAI10245
C	INPUT CONVERTS INPUTS TO EQUINOX OF 1950 REFERENCE	MAI10250
C	INTR FAP EPHEMERIS SUBROUTINE	MAI10260
C	INVAO FORMS INVERSE OF TRANSITION MATRIX	MAI10270
C	INV3 INVERTS UP TO A 6 BY 6 MATRIX	MAI10280
C	LOADO OBTAINS TRANSITION MATRIX FROM T ARRAY	MAI10290
C	LOADT PUTS UNIT ICS ON PERTURBATION EQUATIONS	MAI10300
C	MASS ARRANGES GRAVITATIONAL CONSTANTS OF BODIES CONSIDERED	MAI10310
C	MATRX MULTIPLIES A*B=C OR A*B*AT=C MAX DIMENSION(10,10)	MAI10320
C	MATSUB ERROR PROPOGATION LOGIC SUBROUTINE	MAI10330
C	MNA TRANSFORMATION TO SELENOCENTRIC COORDINATES	MAI10340
C	MNAND TRANSFORMATION FOR SELENOCENTRIC VELOCITIES	MAI10345
C	MONBTR UPDATES COVARIANCE MATRIX FOR MOON BEACONS	MAI10350
C	MULT MULTIPLIES TWO 3 BY 3 MATRICES	MAI10370
C	NUTAIT CALCULATES NUTATION MATRIX	MAI10380
C	OBLIN CALCULATES ACCELERATION DUE TO OBLATENESS	MAI10390
C	ONBTR UPDATES COVARIANCE MATRIX FOR ONBOARD TRACKING	MAI10400
C	ORTC OUTPUTS ORBITAL PARAMETERS	MAI10420
C	OUTC OUTPUTS TRAJECTORY	MAI10440
C	OUTDAT OUTPUTS CALENDAR DATE	MAI10430
C	OUTP OUTPUTS RMS VALUES OF ORBITAL PARAMETERS	MAI10450
C	PTRAN TRANSFORMS P MATRIX	MAI10452

MAIN (CHAIN 1) (Cont'd)

RETRO	PERFORMS RETRO FIRE	MAI10455
ROTATE	CALCULATES TRANSFORMATION FOR ROTATION ABOUT AN AXIS	MAI10460
ROTEQ	CALCULATES MATRIX FROM EQUINOX 1950 TO MEAN EQUINOX OF DATE	MAI10465
		MAI10468
RVIN	TRANSFORMS COORDINATES FROM SPHERICAL TO CARTESIAN	MAI10470
RVOUT	TRANSFORMS COORDINATES FROM CARTESIAN TO SPHERICAL	MAI10480
SDEC	SECOND DERIVATIVE SUBROUTINE	MAI10530
SETN	SET READ AND WRITE TAPE NUMBERS	MAI10535
SHIFTP	SHIFTS BODY CENTER	MAI10540
STEPIC	MOVE ALONG CONIC IN TIME	MAI10545
TIMC	CONVERTS CALENDAR DATE TO DAYS FROM 1950	MAI10550
TIMED	CONVERTS DAYS HOURS.MIN SEC TO SECONDS	MAI10560
TRAC	TRACKING STATION COORDINATES	MAI10570
TRANSH	TRANSFORMS H MATRIX FROM DATE TO 1950	MAI10580
COMMON T,S,C,IC		MAI10600
DIMENSION T(1360),S(1000),C(1000),IC(300),X(3)		MAI10610
1,VX(3),XP(3),VXP(3),AN(3,3),UM(6),BV(4),PBV(3,6)		MAI10620
2,AO(6,6),PARI(21),PI(21),ISTAT(20),FTA(3,6)		MAI10630
3,TRANS(3,6)		MAI10640
4,PFTA(6,6),P(6,6),TGUID(6)		MAI10650
DIMENSION AOS(6,6),RAD(6), RBOP(6),CTE(3,6),AOI(6,6),PUN(3,3)		MAI10660
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),(IC,IDUM),		MAI10670
1(IC(8),IMMSUB),(S(112),DATE),(S(113),FDATE),(S(115),X),(S(118),VX)		MAI10680
2,(IC(193),IGUID),(S(110),TSTOP),(IC(2),IOR),(S(111),TIM)		MAI10690
3,(IC(6),ITARG),(IC(4),KSTP),(IC(1),NSETS),(C(10),TW),(C(11),TF)		MAI10700
4,(C(138),AN),(C(12),TSECO),(S(71),STD),(S(1),UM),(C(15),XP)		MAI10710
5,(C(18),VXP),(C(13),TP1),(C(14),TP2),(S(671),PI),(S(650),PARI)		MAI10720
6,(IC(194),ISTAT),(IC(7),KOUT),(C(649),TSECP),(S(122),OUTTP)		MAI10730
7,(C(460),PFTA),(C(652),P)		MAI10740
8,(S(114),CIBDY),(S(121),TIBDY),(S(722),FTA),(S(124),SKTB)		MAI10750
9,(S(720),PUPIN),(S(721),PARIN)		MAI10760
EQUIVALENCE (C(752),AOS),(S(900),RAD),(C(112),RBOP),(C(30),TSEC)		MAI10770
1,(S(740),CTE),(C(648),TGUIDE),(C(850),AOI),(C(850),PUN)		MAI10780
EQUIVALENCE (S(476),TGUID),(IC(219),IGD)		MAI10790
1,(IC(218),IGDKY),(IC(217),IGDTP),(C(568),TRANS)		MAI10800
EQUIVALENCE (T(1358),TSTP),(C(797),COMP),(S(888),RETR)		MAI10810
CALL SETN(NIN,NUTS)		MAI10811
IF(T(1359)-1359.)1,152,1		MAI10820
1 CALL CONST1		MAI10830
THE CONSTS OF S ARRAY ARE READ IN		MAI10840
200 CONTINUE		MAI10850
WRITE OUTPUT TAPE NUTS,700		MAI10851
700 FORMAT(26H1 START OF FINP INPUT DATA)		MAI10855
CALL FINP(22,S,TIM,CIBDY,TIBDY,GUID,SKTB,CIOMP		MAI10860
1,TSTOP,X,VX,DATE,FDATE,FTA,PI,PARI,TGUID,GID,PUPIN,PARIN,CTE,		MAI10865
2RETR,OUTTP,		MAI10870
2S TIM CIBDY TIBDY GUID SKTB CIOMP TSTOP X VX DATE	132H	MAI10880
3FDATE FTA PI PARI TGUID GID PUPIN PARIN CTE RETR OUTTP		MAI10885
4)		MAI10890
GUID IS SET POSITIVE IF GUIDANCE IS CONSIDERED		MAI10900
IF(GUID) 2,2,3		MAI10910

MAIN (CHAIN 1) (Cont'd)

2	CONTINUE	MAT1092
	IGUID=1	MAT1093
	GO TO 8	MAT1094
3	CONTINUE	MAT1095
	IGD=GID	MAT1096
	IGDTP = GUID	MAT1097
	IF(IGDTP-3) 204,204,205	MAT1098
205	CONTINUE	MAT1099
	IGDTP=2	MAT1100
204	CONTINUE	MAT1101
	IGUID=2	MAT1102
C	CIOMP IS SET POSITIVE IF MATRICES ARE TO BE COMPUTED	MAT1103
	IF(CIOMP) 8,8,4	MAT1104
4	CONTINUE	MAT1105
	COMP=CIOMP	MAT1106
	WRITE OUTPUT TAPE NUTS,750	MAT1107
750	FORMAT(43H1START OF RUN TO COMPUTE GUIDANCE MATRICIES)	MAT1108
	NSETS=7	MAT1109
	IOR=S(114)	MAT1110
	ITARG=S(121)	MAT1111
	RAD(ITARG)=5.*RAD(ITARG)	MAT1112
	KIN=S(111)	MAT1113
	CALL TIMEC(DATE,FDATE,TW,TF)	MAT1114
	CALL INPUT(KIN,XP,VXP,TW,TF,AN,X,VX)	MAT1115
	TSECO =0.	MAT1116
	KSTP=1	MAT1117
	CALL LOADT	MAT1118
	CALL TIMED(TSTOP,TSTPS)	MAT1119
	TSTP=TSTPS*STD	MAT1120
	IMMSUB=1	MAT1121
	CALL GOTOB(TSTP)	MAT1122
	CALL BVEC(IOR,ITARG,XP,VXP,BV,PBV,TP1,TP2,UM)	MAT1123
	CALL LOADO(AO)	MAT1124
	CALL MATRX(PBV,AO,CTE,3,6,6,0)	MAT1125
	IF(RBOP(ITARG)-RAD(ITARG))206,206,207	MAT1126
206	CONTINUE	MAT1127
	RAD(ITARG)=RAD(ITARG)/5.	MAT1128
	TSECO=TSEC	MAT1129
	CALL GOTOB(TSTP)	MAT1130
	CALL LOADO(AO)	MAT1131
	GO TO 208	MAT1132
207	CONTINUE	MAT1133
	RAD(ITARG)=RAD(ITARG)/5.	MAT1134
208	CONTINUE	MAT1135
	WRITE OUTPUT TAPE NUTS,706,((AO(I,J),J=1,6),I=1,6)	MAT1136
706	FORMAT(31H0TRANSITION MATRIX TO END POINT//(6E17,8))	MAT1137
	WRITE OUTPUT TAPE NUTS,707,((CIE(I,J),J=1,6),I=1,3)	MAT1138
707	FORMAT(49H0B VECTOR TRANSITION MATRIX. BY ROWS B,T,B,R,VINF//	MAT1139
	1(6E17,8))	MAT1140
	DO 6 I=1,3	MAT1141
	DO 6 J=1,6	MAT1142

MAIN (CHAIN 1) - (Cont'd)

	FTA(I,J)=AO(I,J)	MAT11430
4	CONTINUE	MAT11440
4	CONTINUE	MAT11450
	WRITE OUTPUT TAPE NUTS,751	MAT11460
751	FORMAT(18H1START OF DATA RUN)	MAT11470
	CALL CHAIN(2,B3)	MAT11480
152	CALL LOADO(AO)	MAT11490
	AO IS TRANSITION MATRIX FROM LAST TIME IN MATSUB	MAT11500
	CALL MATRX(AO,P,P,6,6,6,1)	MAT11510
	DO 30 I=1,6	MAT11511
	DO 30 J=I,6	MAT11512
	P(I,J)=(P(I,J)+P(J,I))/2.	MAT11514
	P(J,I)=P(I,J)	MAT11516
30	CONTINUE	MAT11518
	P IS STATE COVARIANCE MATRIX AT END POINT	MAT11520
	WRITE OUTPUT TAPE NUTS,800,((P(I,J),J=1,6),I=1,6)	MAT11530
800	FORMAT(38H0 STATE COVARIANCE MATRIX AT END POINT	MAT11540
	1/(6E17.8))	MAT11550
	CALL MATRX(AO,AOS,AOS,6,6,6,0)	MAT11560
	AOS IS TRANSITION MATRIX FROM INJECTION TO END POINT	MAT11570
	WRITE OUTPUT TAPE NUTS,801,((ACS(I,J),J=1,6),I=1,6)	MAT11580
801	FORMAT(50H0 STATE TRANSITION MATRIX FROM INJECT TO END POINT	MAT11590
	1/(6E17.8))	MAT11600
	CALL INVAO(AOS,AOI)	MAT11610
	FORMS INVERSE OF AOS	MAT11620
	CALL MATRX(AOI,P,ACS,6,6,6,1)	MAT11630
	WRITE OUTPUT TAPE NUTS,802,AOS	MAT11640
802	FORMAT(38H0 STATE COVARIANCE MATRIX AT INJECTION	MAT11650
	1/(6E17.8))	MAT11660
	CALL BVEC(IOR,ITARG,XP,VXP,BV,PBV,TP1,TP2,UM)	MAT11670
	WRITE OUTPUT TAPE NUTS,810,((PBV(J,I),I=1,6),J=1,3)	MAT11680
810	FORMAT(40H0 B*T,B*R,VINF PARTIALS AT END POINT PBV	MAT11690
	1/(6E17.8))	MAT11700
	CALL MATRX(PBV,P,PUN,3,6,6,1)	MAT11710
	WRITE OUTPUT TAPE NUTS,811,PUN	MAT11720
811	FORMAT(47H0 COVARIANCE MATRIX OF KNOWLEGE OF B*T,B*R,VINF	MAT11730
	1/(3E20.8))	MAT11740
	IGUID = IGUID	MAT11750
	GO TO (23,22),IGUID	MAT11760
22	CONTINUE	MAT11770
	CALL MATRX(AO,PFTA,PFTA,6,6,6,1)	MAT11780
	DO 31 I=1,6	MAT11781
	DO 31 J=I,6	MAT11782
	PFTA(I,J)=(PFTA(I,J)+PFTA(J,I))/2.	MAT11784
	PFTA(J,I)=PFTA(I,J)	MAT11786
31	CONTINUE	MAT11788
	WRITE OUTPUT TAPE NUTS,804,((PTFA(I,J),J=1,6),I=1,6)	MAT11790
804	FORMAT(38H0 COVARIANCE MATRIX OF GUIDANCE ERRORS	MAT11800
	1/(6E17.8))	MAT11810
	CALL INVAO(AO,AOI)	MAT11820
	CALL MATRX(TRANS,AOI,TRANS,3,6,6,0)	MAT11830

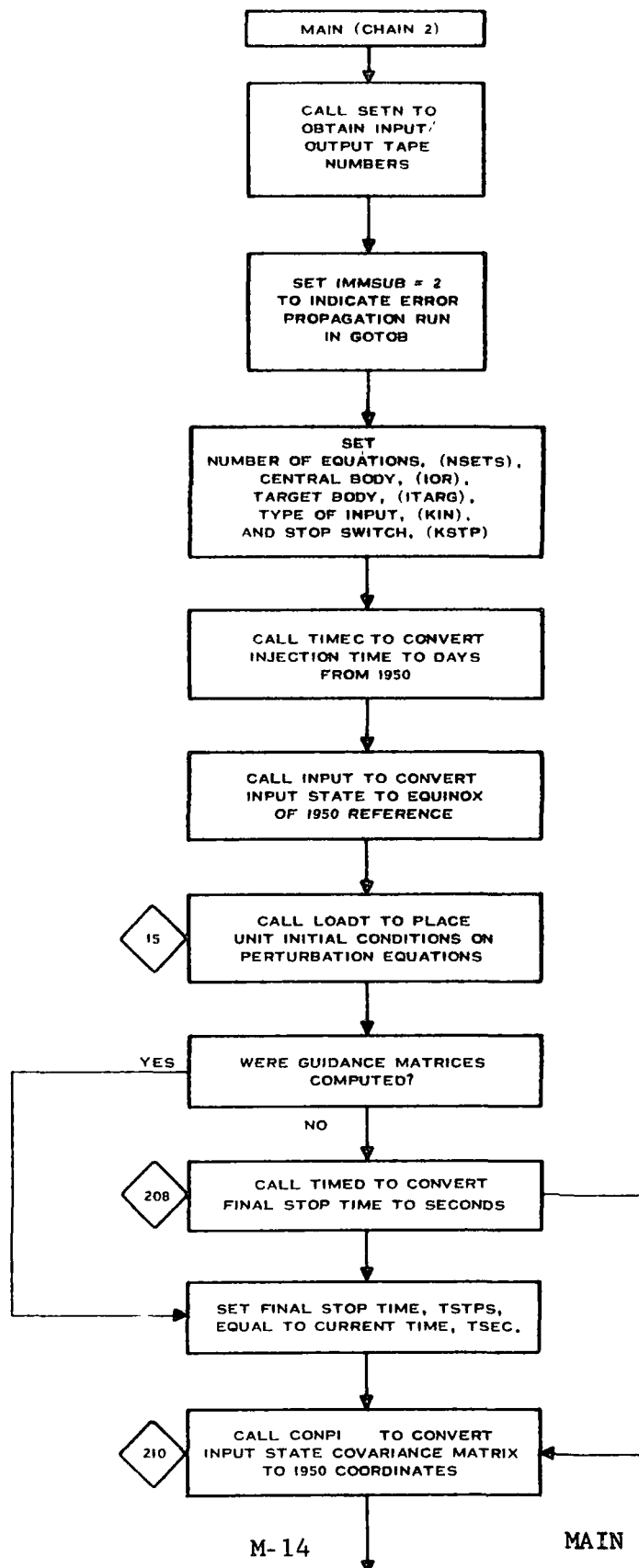
MAIN (CHAIN 1) (Cont'd)

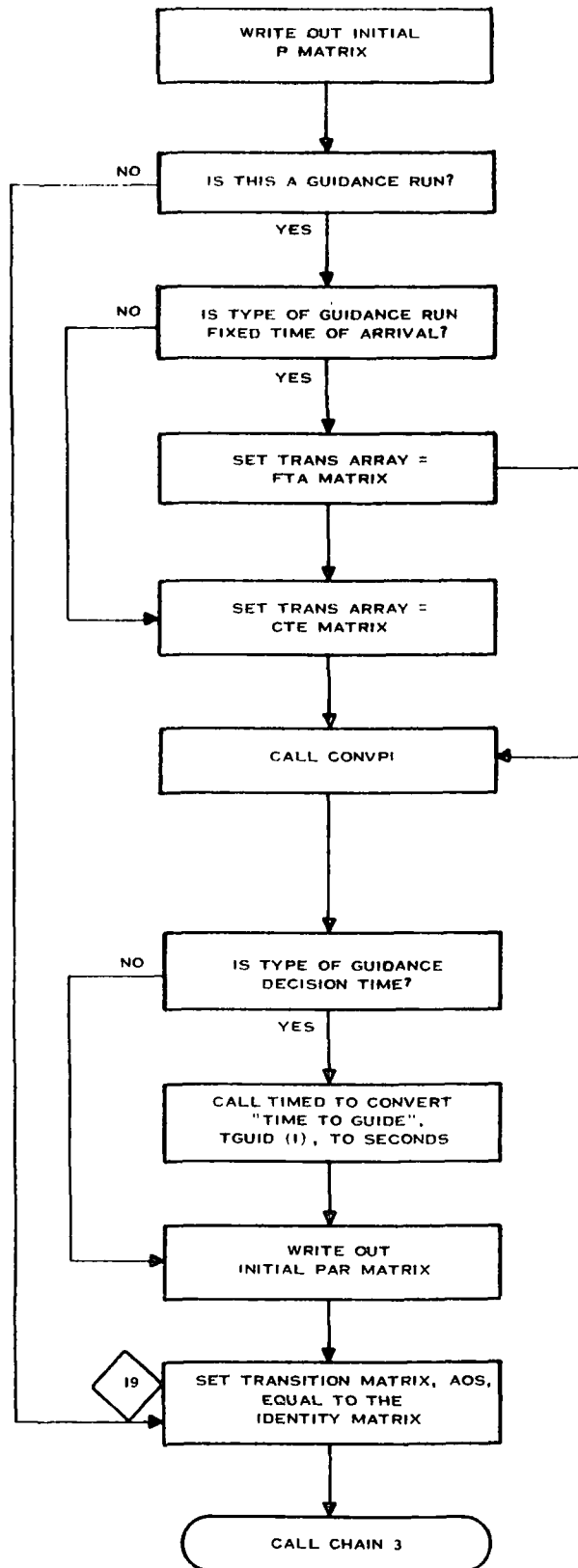
CALL MATRX(TRANS,P,PUN,3,6,6,1)	MAI1184
WRITE OUTPUT TAPE NUTS,803,PUN	MAI1185
803 FORMAT(58H0 COVARIANCE MATRIX OF KNOWLEDGE OF TARGET MISS PARAMETE	MAI1186
1RS	MAI1187
2/(3E20.8))	MAI1188
CALL MATRX(TRANS,PFTA,PUN,3,6,6,1)	MAI1189
WRITE OUTPUT TAPE NUTS,807,PUN	MAI1190
807 FORMAT(45H0 COVARIANCE MATRIX OF TARGET MISS PARAMETERS	MAI1191
1/(3E20.8))	MAI1192
IF(RETR=.0001)23,23,10	MAI1192
10 CONTINUE	MAI1192
CALL RETRO	MAI1192
23 CONTINUE	MAI1193
RETR=0.	MAI1193
GUID=0	MAI1194
CIOMP=0	MAI1195
GO TO 200	MAI1196
END	MAI1

Subroutine: MAIN (Chain 2)

Purpose: Set up program to perform error propagation run. Call Chain 3 to make data run.

Common storages used or required:	<u>T, S, C, IC</u>
Subroutines required:	<u>CHAIN, CONVPI, INPUT, TIMEC, TIMED</u>
Functions required:	<u>None</u>
Approximate number of storages required:	<u>317 DEC</u>





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MAIN (CHAIN 2) -3

MAIN (CHAIN 2)

* LABEL	MAI2
* SYMBOL TABLE	MAI2
CEC20E2 PART 2 MAIN CONTINUED	MAI20000
COMMON T,S,C,IC	MAI20010
DIMENSION T(1360),S(1000),C(1000),IC(300),X(3)	MAI20020
1,VX(3),XP(3),VXP(3),AN(3,3),UM(6),BV(4),PBV(3,6)	MAI20030
2,AO(6,6),PARI(21),PI(21),ISTAT(20),FTA(3,6)	MAI20040
3,TRANS(3,6)	MAI20050
4,PFTA(6,6),P(6,6),TGUID(6)	MAI20060
DIMENSION AOS(6,6),RAD(6),RBOP(6),CTE(3,6),AOI(6,6),PUN(3,3)	MAI20070
EQUIVALENCE(T,TDUM),(S,SDUM),(C,CDUM),(IC,IDUM),	MAI20080
1(IC(8),IMMSUB),(S(112),DATE),(S(113),FDATE),(S(115),X),(S(118),VX)	MAI20090
2,(IC(193),IGUID),(S(110),TSTOP),(IC(2),IOR),(S(111),TIM)	MAI20100
3,(IC(6),ITARG),(IC(4),KSTP),(IC(1),NSETS),(C(10),TW),(C(11),TF)	MAI20110
4,(C(138),AN),(C(12),TSECO),(S(71),STD),(S(1),UM),(C(15),XP)	MAI20120
5,(C(18),VXP),(C(13),TP1),(C(14),TP2),(S(671),PI),(S(650),PARI)	MAI20130
6,(IC(194),ISTAT),(IC(7),KOUT),(C(649),TSECP)	MAI20140
7,(C(460),PFTA),(C(652),P)	MAI20150
8,(S(114),CIBDY),(S(121),TIBDY),(S(722),FTA),(S(124),SKTB)	MAI20160
9,(S(720),PUPIN),(S(721),PARIN)	MAI20170
EQUIVALENCE(C(752),AOS),(S(900),RAD),(C(112),RBOP),(C(30),TSEC)	MAI20180
1,(S(740),CTE),(C(648),TGUIDE),(C(850),AOI),(C(850),PUN)	MAI20190
EQUIVALENCE(S(476),TGUID),(IC(219),IGD)	MAI20200
1,(IC(218),IGDKY),(IC(217),IGDTP),(C(568),TRANS)	MAI20210
EQUIVALENCE(T(1358),TSTP),(C(797),COMP)	MAI20220
CALL SETN(NIN,NOUT)	MAI20225
IMMSUB=2	MAI20230
NSETS=7	MAI20240
IOR =S(114)	MAI20250
ITARG=S(121)	MAI20260
KIN =S(111)	MAI20270
KSTP=S(124)	MAI20280
CALL TIMEC(DATE,FDATE,TW,TF)	MAI20290
CALL INPUT(KIN,XP,VXP,TW,TF,AN,X,VX)	MAI20300
TSECO =0.	MAI20310
DO 15 I=1,20	MAI20320
ISTAT(I)=0	MAI20330
15 CONTINUE	MAI20340
KOUT=S(122)	MAI20350
CALL LOADT	MAI20360
TSECP=0.	MAI20370
IF(COMP)208,208,209	MAI20380
208 CONTINUE	MAI20390
CALL TIMED(TSTOP,TSTPS)	MAI20400
GO TO 210	MAI20410
209 TSTRS=TSEC	MAI20420
210 CONTINUE	MAI20430
TSTP=TSTPS*STD	MAI20440
INPUP=PUPIN	MAI20450
CALL CONVPI(INPUP,PI,P)	MAI20460
WRITE OUTPUT TAPE NOUT,708	MAI20470

AIN (CHAIN 2) (Cont'd)

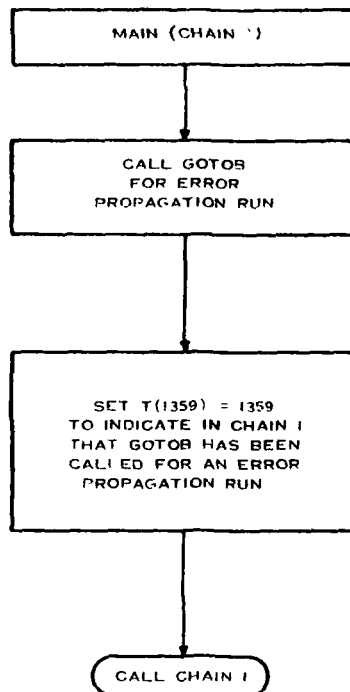
708	FORMAT(18H0INITIAL P MATRIX)	MAI20480
	WRITE OUTPUT TAPE (NOUT,709,P	MAI20490
709	FORMAT(6E17,8)	MAI20500
	IGUID=IGUID	MAI20510
	GO TO (19,18), IGUID	MAI20520
18	CONTINUE	MAI20530
	IGDTP=IGDTP	MAI20540
	GO TO(211,212,212),IGDTP	MAI20550
211	CONTINUE	MAI20560
	DO 202 I=1,3	MAI20570
	DO 202 J=1,6	MAI20580
	TRANS(I,J)=FTA(I,J)	MAI20590
202	CONTINUE	MAI20600
	GO TO 214	MAI20610
212	DO 213 I=1,3	MAI20620
	DO 213 J=1,6	MAI20630
213	TRANS(I,J)=CTE(I,J)	MAI20640
214	CONTINUE	MAI20650
	IGDKY=1	MAI20660
	INPAR=PARIN	MAI20670
	CALL CONVPI(INPAR,PARI,PFTA)	MAI20680
	S(475) CONTAINS TYPE OF GUIDANCE DECISION 0 TIME + RATIO	MAI20690
	IF(S(475))17,17,20	MAI20700
17	CONTINUE	MAI20710
	CALL TIMED(TGUID(1),TGUIDE)	MAI20720
20	CONTINUE	MAI20730
	WRITE OUTPUT TAPE (NOUT,710	MAI20740
710	FORMAT(20H0 INITIAL PAR MATRIX)	MAI20750
	WRITE OUTPUT TAPE (NOUT,709,PFTA	MAI20760
19	CONTINUE	MAI20770
	DO 150 I=1,6	MAI20780
	DO 151 J=1,6	MAI20790
151	AOS (I,J) =0,	MAI20800
150	AOS (I,I)=1,	MAI20810
	CALL CHAIN(3,B3)	MAI20820
	END	MAI2

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Subroutine: MAIN (Chain 3)

Purpose: Call subroutine GOTOB to perform integration of trajectory for an error propagation run. Set cell T(1359) = 1359 to indicate GOTOB has been called and call Chain 1.

Common storages used or required:	T
Subroutines required:	GOTOB
Functions required:	None
Approximate number of storages required:	



IN (CHAIN 3)

```

    LABEL
    SYMBOL TABLE
C20C2      CHAIN 3 GOTOB ONLY
    COMMON T
    DIMENSION T(1360)
    EQUIVALENCE(T(1358),TSTP)
    CALL GOTOB(TSTP)
    T(1359)=1359,
    CALL CHAIN(1,B3)
    END

```

```

MAI3
MAI3
MAI30000
MAI30010
MAI30020
MAI30030
MAI30040
MAI30050
MAI30060
MAI3

```

MAIN (CHAIN 3) -3

M-21

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SUBROUTINES

(Subroutine discussion is presented in the following manner: (1) subroutine description, (2) subroutine flow diagrams, if applicable, (3) subroutine listings.)

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Function: ARKTAN

Purpose: To find the double precision arctangent θ of (Y/X) in the proper quadrant. $-\pi \leq \theta \leq \pi$ for $N = 180$; $0 \leq \theta \leq 360$ for $N = 360$.

Calling Sequence:

Z = ARKTAN (N, X, Y)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	N	1			$N = 180 \text{ or } 360, \text{ as above}$
I	X	1			
I	Y	1			
O	ARKTAN			radians	$\tan^{-1} (Y/X)$

Common storages used or required:

None

Subroutines required:

None

Functions required:

DATAN, other double precision routines

Approximate number of storages required:

```

* LABEL
* SYMBOL TABLE
CEC2021 FUNCTION ARKTAN
  CALL SETN(NIN,NOUT)
  FUNCTION ARKTAN(N,X,Y)
D   P=3.14159265
    K=N/180
D   ARKTAN = ATANF(ABSF(Y/X))
    IF(Y)1,2,3
      1 GO TO (4,5),K
      4 IF (X)10,11,12
D   10 ARKTAN = ARKTAN=P
    GO TO 9
D   11 ARKTAN = -P*.5
    GO TO 9
D   12 ARKTAN = -ARKTAN
    GO TO 9
      5 IF (X)13,14,15
D   13 ARKTAN = P+ARKTAN
    GO TO 9
D   14 ARKTAN = 3.*.5*P
    GO TO 9
D   15 ARKTAN = 2.*P-ARKTAN
    GO TO 9
      2 IF (X)16,17,9
D   16 ARKTAN = P
    GO TO 9
    17 WRITE OUTPUT:TAPE NOUT,18
    18 FORMAT (90H0
      1 FAILED - ARKTAN(0/0) IS UNDEFINED/1H0)
    GO TO 9
      3 IF(X)8,19,9
D   8 ARKTAN = P-ARKTAN
    GO TO 9
D   19 ARKTAN = .5*P
      9 RETURN
    END

```

THE ARKTAN FUNCTION HAS

```

ARKT
ARKT
ARKT0000
ARKT0015
ARKT0010
ARKT0020
ARKT0030
ARKT0040
ARKT0050
ARKT0060
ARKT0070
ARKT0080
ARKT0090
ARKT0100
ARKT0110
ARKT0120
ARKT0130
ARKT0140
ARKT0150
ARKT0160
ARKT0170
ARKT0180
ARKT0190
ARKT0200
ARKT0210
ARKT0220
ARKT0230
ARKT0240
ARKT0250
ARKT0260
ARKT0270
ARKT0280
ARKT0290
ARKT0300
ARKT0310
ARKT0320
ARKT

```

Function: ARKTNS

Purpose: To find the arctangent θ of (Y/X) in the proper quadrant.

$-\pi \leq \theta \leq \pi$ for $N = 180$; $0 \leq \theta < 360$ for $N = 360$.

Calling Sequence:

$Z = \text{ARKTNS}(N, X, Y)$

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	N	1			$N = 180$ or 360 , as above
I	X	1			
I	Y	1			
O	ARKTNS			radians	$\tan^{-1}(Y/X)$

Common storages used or required:

None

Subroutines required:

None

Functions required:

ATANF

Approximate number of storages required:

* LABEL	ARKS
* SYMBOL TABLE	ARKS
CEC2022 FUNCTION ARKTNS	ARKS0000
FUNCTION ARKTNS(N,X,Y)	ARKS0010
CALL SETN(NIN,NOUT)	ARKS0015
P=3.14159265	ARKS0020
K=N/180	ARKS0030
ARKTNS = ATANF(ABSF(Y/X))	ARKS0040
IF(Y)1,2,3	ARKS0050
1 GO TO (4,5),K	ARKS0060
4 IF (X)10,11,12	ARKS0070
10 ARKTNS = ARKTNS-P	ARKS0080
GO TO 9	ARKS0090
11 ARKTNS = -P+.5	ARKS0100
GO TO 9	ARKS0110
12 ARKTNS = -ARKTNS	ARKS0120
GO TO 9	ARKS0130
5 IF (X)13,14,15	ARKS0140
13 ARKTNS = P+ARKTNS	ARKS0150
GO TO 9	ARKS0160
14 ARKTNS = 3.*.5*P	ARKS0170
GO TO 9	ARKS0180
15 ARKTNS = 2.*P-ARKTNS	ARKS0190
GO TO 9	ARKS0200
2 IF (X)16,17,9	ARKS0210
16 ARKTNS = P	ARKS0220
GO TO 9	ARKS0230
17 WRITE OUTPUT TAPE NOUT,18	ARKS0240
18 FORMAT (90H0	THE ARKTAN FUNCTION HAS
1 FAILED - ARKTAN(0/0) IS UNDEFINED/1H0)	ARKS0250
GO TO 9	ARKS0260
3 IF(X)8,19,9	ARKS0270
8 ARKTNS = P-ARKTNS	ARKS0280
GO TO 9	ARKS0290
19 ARKTNS = .5*P	ARKS0300
9 RETURN	ARKS0310
END	ARKS0320
	ARKS

Function: ASINH

Purpose: To compute $\theta = \operatorname{arcsinh}(X) = \log_e (X + \sqrt{X^2 + 1})$

Calling Sequence:

$Y = \operatorname{ASINH}(X)$

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	X				
O	ASINH			radians	$\sinh^{-1}(X) = \log_e (X + \sqrt{X^2 + 1})$

Common storages used or required:

None

Subroutines required:

None

Functions required:

LOGF

Approximate number of storages required:

ASINH

WDL-TR2184

```
* LABEL
* SYMBOL TABLE
  FUNCTION ASINH(X)
  ASINH=LOGF(X+SQRTF(X*X+1.0))
  RETURN
END
```

```
ASIN
ASIN
ASIN000
ASIN001U
ASIN0020
ASIN
```


Subroutine: BODY

Purpose: To compute the perturbing acceleration due to the perturbing bodies included in the ephemeris. It also computes the first variation of the perturbing acceleration for use in the integration of the variational equations.

Calling Sequence:

CALL BODY (XP, PO, VKB, RBO, RBOP, CA, NOR, BP, T, NEQ, U)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	XP	3	\vec{R}	Km	Position vector
I	PO	22	\vec{R}_i	Km	Positions of bodies in ephemeris
I	VKB	6	μ_i	Km^3/sec^2	Gravitational constants of bodies
					being considered
O	RBOP	6	$ \vec{R}_{Hv} $	Km	Magnitude of position of vehicle
					relative to i th body
O	RBO	6	\vec{R}_i	Km	Position of i th body relative to
					central body

(Cont'd.)

Common storages used or required:

None

Subroutines required:

None

Functions required:

FNORM

Approximate number of storages required:

445 DEC

(Cont'd.)

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	CA	3			Perturbation accelerations
I	NOR	1			Number of central body
O	BP	3,3	$\frac{\partial x_i}{\partial x_j}$		First variation of perturbation accelerations
I/O	T	1360			Common T Block
I	NEQ	1			Number of equations being integrated
I	U	1	μ	Km ³ /sec ²	Central body gravitational constant

Equation Being Solved

The perturbation term due to the n bodies being considered is:

$$\vec{P} = - \sum_{j=1}^n \mu_j \frac{\vec{R}_{jp}}{R_{jp}^3} + \frac{\vec{R}_j}{R_j^3}$$

where $\vec{R}_{jp} = \vec{R} - \vec{R}_j$.

The vector \vec{P} is placed in the cells called CA.

If the number of equations being solved is greater than three, the first variation of \vec{P} with respect to position is determined and placed in the T block for the integration package

$$AP = \frac{\partial \ddot{x}_i}{\partial x_j} \quad \begin{matrix} i = 1,3 \\ j = 1,3 \end{matrix}$$

The form of AP is obtained by differentiating

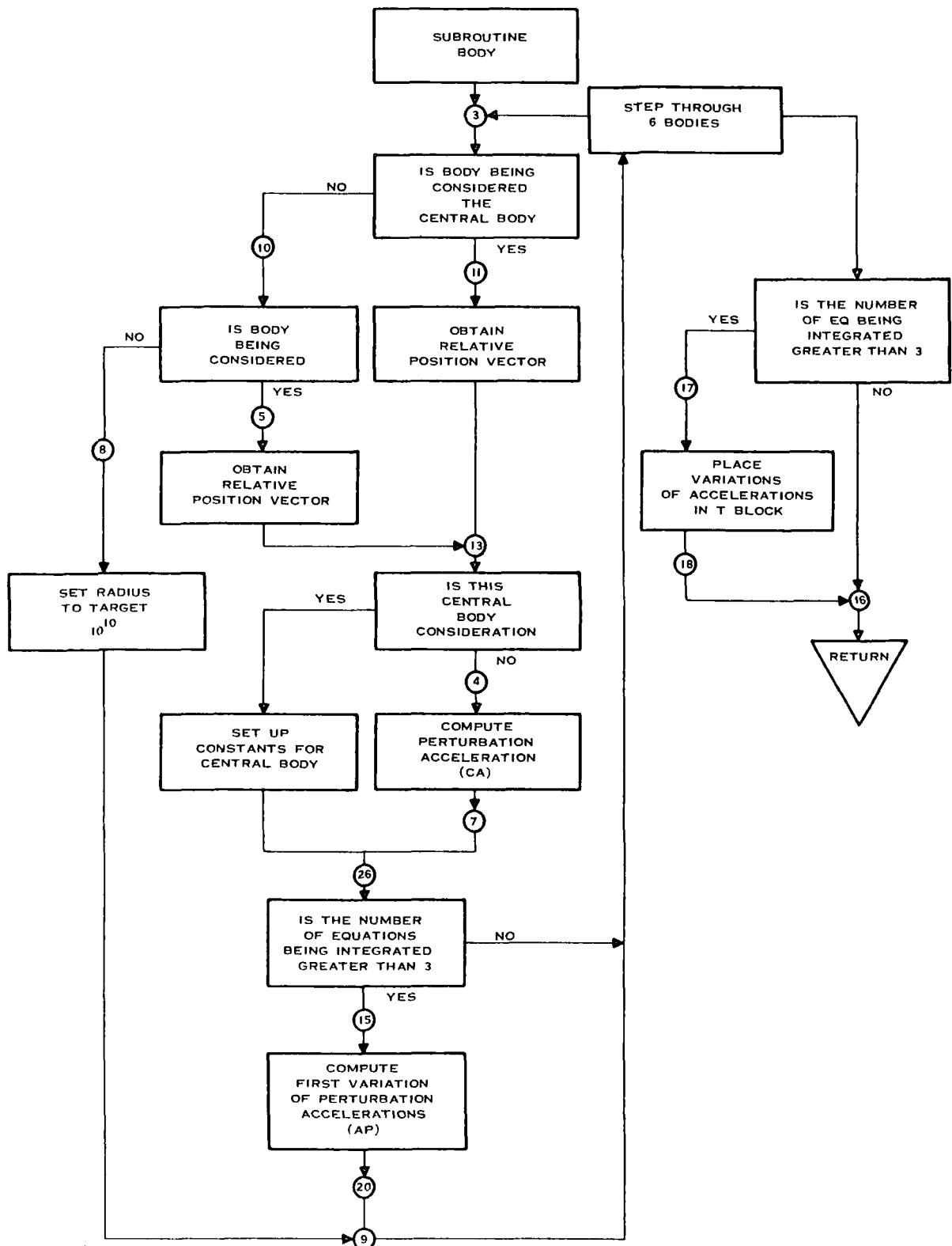
$$-\mu \frac{\vec{R}}{R^3} + \vec{P}$$

with respect to X_j . This yields:

$$AP_{ij} = - \sum_{k=0}^n \mu_k \left\{ \frac{1}{R_{kp}^3} \frac{\partial \vec{R}}{\partial X_j} - \frac{3}{R_{kp}^5} \left(\vec{R}_{kp} \cdot \frac{\partial \vec{R}}{\partial X_j} \right) \vec{R}_{kp} \right\}$$

with $\mu_0 = \mu$ and $\vec{R}_{0p} = \vec{R}$

$$\text{or } AP_{ij} = \sum_{k=0}^n \frac{\mu_k}{R_{kp}^3} \left\{ 3 \frac{\vec{R}_{kp} \vec{R}_{kp}^T}{R_{kp}^3} - I \right\}$$



BODY		BODY
*	LABEL	BODY
*	SYMBOL TABLE	BODY
	SUBROUTINE BODY(X,PO,VKB,RBO,RBOP,CA,NOR,AP,T,NEQ,U)	BODY000
	DIMENSION X(3),PO(22),VKB(6),RBO(6),RBOP(6),CA(3),XN(18),RJP(3),	BODY001
	1AP(3,3),T(1360)	BODY002
	N = NOR	BODY003
	DO 1 I=1,15	BODY004
	J = 23-I	BODY005
1	XN(I) = PO(J)	BODY006
	DO 2 I=16,18	BODY007
	J = 20-I	BODY008
2	XN(I) = PO(J)	BODY009
	DO 3 I=1,3	BODY010
	CA(I)=0.	BODY011
3	CONTINUE	BODY012
	DO 9 I=1,6	BODY013
	K1 = 3*I-3	BODY014
	IF(I-N)10,11,10	BODY015
11	CONTINUE	BODY016
	DO 12 J=1,3	BODY017
	RJP(J)=X(J)	BODY018
12	CONTINUE	BODY019
	GO TO 13	BODY020
10	CONTINUE	BODY021
	IF (VKB(I)) 5,8,5	BODY022
5	DO 6 J=1,3	BODY023
	K = K1+J	BODY024
	RJP(J) = X(J) - XN(K)	BODY025
6	CONTINUE	BODY026
13	CONTINUE	BODY027
	RBOP(I) = FNORM(RJP)	BODY028
	RBO(I) = FNORM(XN(K1+1))	BODY029
	R3 = RBOP(I)**3	BODY030
	X3 = RBO(I)**3	BODY031
	FAC=VKB(I)/R3	BODY032
	FAX=VKB(I)/X3	BODY033
	IF(I-N)4,23,4	BODY034
4	CONTINUE	BODY035
C	ACCELERATIONS (NEGATIVE) DUE TO PERTURRING BODIES	BODY036
	DO 7 J=1,3	BODY037
	K1J = K1 + J	BODY038
	CA(J)=CA(J)+FAC*RJP(J)+FAX*XN(K1J)	BODY039
7	CONTINUE	BODY040
	GO TO 26	BODY041
23	CONTINUE	BODY042
	FAC=U/R3	BODY043
	FAX=U/X3	BODY044
26	CONTINUE	BODY045
	DO 24 J=1,3	BODY046
	RJP(J)=RJP(J)/RBOP(I)	BODY047
24	CONTINUE	BODY048

BODY - 5

```

C      RJP IS NOW A UNIT VECTOR
      IF(NEQ-3)14,14,15
15 CONTINUE
C      PARTIALS FOR PERTURBATION EQUATIONS
      DO 20 J=1,3
      J=J
      DO 20 K=J,3
      AP(J,K)=AP(J,K)+FAC*(3.*RJP(J)*RJP(K))
      IF(J-K)21,22,21
21 CONTINUE
      AP(K,J)=AP(J,K)
      GO TO 20
22 CONTINUE
      AP(J,J)=AP(J,J)-FAC
20 CONTINUE
25 FORMAT(3E16,8)
14 CONTINUE
      GO TO 9
      8 RBOP(I) = 1,E10
      9 CONTINUE
      NS=NEQ/3-1
      IF(NS)16,16,17
16 CONTINUE
      RETURN
17 CONTINUE
      DO 18 I=1,NS
      NST=2*NEQ+3+3*I
      NSTP=3+3*I
      DO 19 J=1,3
      KK=NST+J
      T(KK)=0.
      DO 19 K=1,3
      JJ=NSTP+K
      T(KK)=T(KK)+AP(J,K)*T(JJ)
19 CONTINUE
18 CONTINUE
      GO TO 16
      END

```

```

BODY0490
BODY0500
BODY0510
BODY0520
BODY0530
BODY0540
BODY0550
BODY0560
BODY0570
BODY0580
BODY0590
BODY0600
BODY0610
BODY0620
BODY0630
BODY0640
BODY0650
BODY0660
BODY0670
BODY0680
BODY0690
BODY0700
BODY0710
BODY0720
BODY0730
BODY0740
BODY0750
BODY0760
BODY0770
BODY0780
BODY0790
BODY0800
BODY0810
BODY0820
BODY0830
BODY0840
BODY0850
BODY

```

Subroutine: BVEC

Purpose: To obtain the matrix of target miss partials; B·T, B·R, and V infinity with respect to the state.

Calling Sequence:

CALL BVEC (IOR, ITARG, X, V, BV, PBV, TW, TF, UM)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	IOR	1			Central body
I	ITARG	1			Target body
I	X	3	\vec{R}		Position vector
I	V	3	\vec{U}		Velocity vector
O	BV	4			Nominal Miss Parameters
O	PBV	(3,6)			Matrix of Miss Partial
I	TW	1	t	days	Whole days from 1950
I	TF	1	t	days	Fractional days from 1950
I	UM	1	μ	Km ³ /sec ²	Gravitational constant

Common storages used or required:

None

Subroutines required:

DOT, INTRI, CROSS

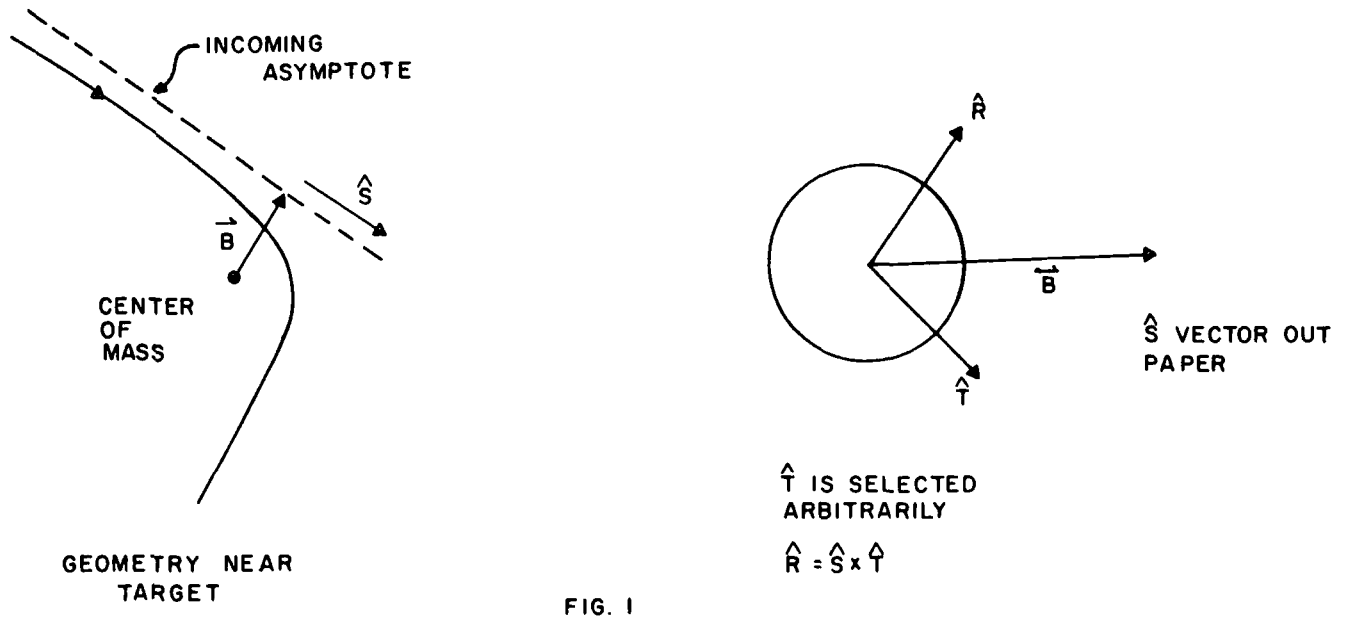
Functions required:

FNORM

Approximate number of storages required:

Derivation of the \vec{B} , \vec{S} , \vec{T} , and \vec{R} vectors

The B , R , S , and T vectors are used to define a target miss (see Fig. 1 below)



\vec{B} , the position vector in the plane of the trajectory originating at the center of gravity of the target and directed perpendicularly to the incoming asymptote of the hyperbola, is approximately the vector miss which would occur if the target had no mass.

To determine the target miss direction relative to the target, a set of orthogonal vectors is computed. Let \hat{S} be a unit vector in the direction of the incoming asymptote, \hat{T} be a unit vector perpendicular to \hat{S} that lies in a fixed plane of interest such as the equatorial plane, and \hat{R} be a unit vector to form a right-handed system.

$$\hat{R} = \hat{S} \times \hat{T}$$

Since \vec{B} is perpendicular to \hat{S} , it lies in the plane determined by \hat{R} and \hat{T} . The variables which are used to describe the miss relative to a plane of interest are the projections of \vec{B} on \hat{T} and \hat{R} , i.e., $\vec{B} \cdot \hat{T}$ and $\vec{B} \cdot \hat{R}$.

The quantities used in the derivation of the vectors are the following:

$$h = |\vec{R} \times \vec{v}| \quad C_3 = v^2 - \frac{2\mu}{R}$$

$$e = \sqrt{1 + \frac{h^2 C_3}{\mu^2}} \quad p = \frac{h^2}{\mu}$$

True anomaly

$$\theta = \cos^{-1} \left[\frac{1}{e} \left(\frac{p}{R} - 1 \right) \right]$$

Unit vectors to specify orientation of conic

$$\vec{\zeta} = \frac{\vec{R} \times \vec{v}}{|\vec{R} \times \vec{v}|} \quad \vec{M} = \vec{\zeta} \times \frac{\vec{R}}{|\vec{R}|}$$

$$\vec{\xi} = \frac{\vec{R}}{|\vec{R}|} \cos \theta - \vec{M} \sin \theta$$

$$\vec{h} = \vec{\zeta} \times \vec{\xi}$$

The unit vector in the direction of the asymptote is given by

$$\hat{S} = \frac{1}{e} \vec{\xi} + \sqrt{1 - \left(\frac{1}{e}\right)^2} \vec{n}$$

The impact parameter

$$\vec{B} = |\vec{B}| \left[\sqrt{1 - \left(\frac{1}{e}\right)^2} \vec{s} - \frac{1}{e} \vec{n} \right]$$

where $|\vec{B}| = \frac{\mu}{c^3} \sqrt{e^2 - 1}$

Also
$$T_X = \frac{S_Y}{\sqrt{S_X^2 + S_Y^2}}$$

$$T_Y = - \frac{S_X}{\sqrt{S_X^2 + S_Y^2}}$$

$$T_Z = 0$$

and
$$\hat{R} = \hat{S} \times \hat{T}$$

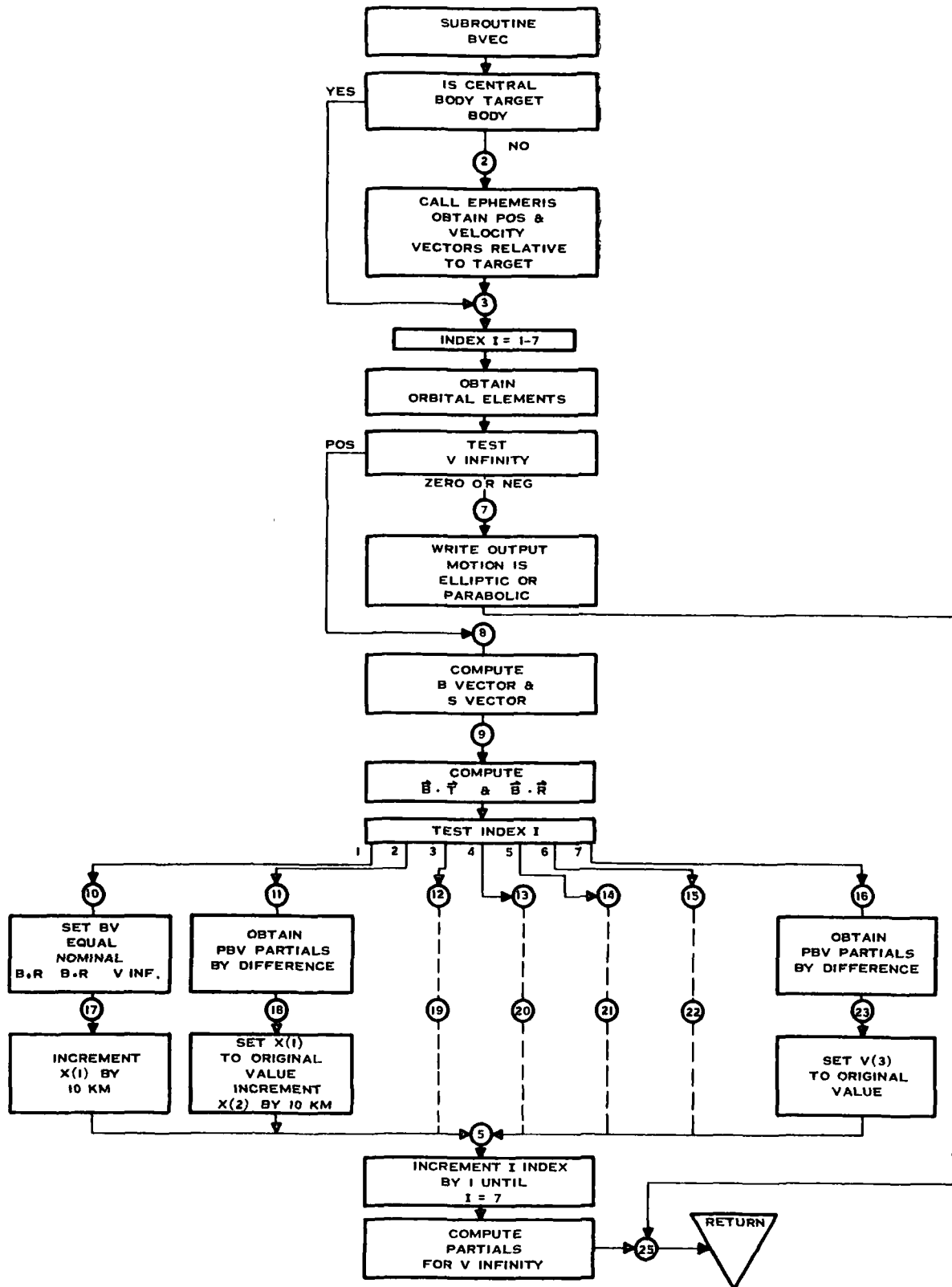
Derivation of partials of V infinity with respect to the state

$$V_{INF} = \sqrt{v^2 - \frac{2\mu}{R}}$$

$$\frac{\partial V_{INF}}{\partial X_i} = \frac{\mu X_i}{(V_{INF})^3} \quad i = 1, 2, 3$$

$$\frac{\partial V_{INF}}{\partial X_i} = \frac{X_i}{(V_{INF})} \quad i = 1, 2, 3$$

Reference: JPL EXTERNAL PUBLICATION NO. 674



* LABEL	BVEC
* SYMBOL TABLE	BVEC
CEC2001 SUBROUTINE BVEC	BVEC0000
SUBROUTINE BVEC (IOR,ITARG,X,V,BV,PBV,TW,TF,UM)	BVEC0010
DIMENSION X(3),V(3),XP(3),VP(3),BV(4),PBV(3,6),PO(22),VE(22)	BVEC0020
1,BD(3),CP(3),RB(3),RM(3),UM(6),PP(3),QQ(3),S(3),B(3),RR(3),TT(3)	BVEC0030
CALL SETN(NIN,NOUT)	BVEC0035
D=2,E6	BVEC0040
DO 1 I=1,3	BVEC0050
XP(I)=X(I)	BVEC0060
VP(I)=V(I)	BVEC0070
1 CONTINUE	BVEC0080
IF (IOR=ITARG) 2,3,2	BVEC0090
2 CONTINUE	BVEC0100
N=IOR=1	BVEC0110
CALL INTR1(TW,TF,N,PO,1,VE,D)	BVEC0120
IC=26=3*ITARG	BVEC0130
DO 4 I=1,3	BVEC0140
IB=IC=I	BVEC0150
XP(I)=XP(I)+PO(IB)	BVEC0160
VP(I)=VP(I)+VE(IB)	BVEC0170
4 CONTINUE	BVEC0180
3 CONTINUE	BVEC0190
DO 5 I=1,7	BVEC0200
CALL CROSS(XP,VP,CP)	BVEC0210
D=FNORM(CP)	BVEC0220
R=FNORM(XP)	BVEC0230
DO 6 J=1,3	BVEC0240
CP(J)=CP(J)/D	BVEC0250
RB(J)=XP(J)/R	BVEC0260
6 CONTINUE	BVEC0270
CALL CROSS(CP,RB,RM)	BVEC0280
U=UM(ITARG)	BVEC0290
C3=DOT(VP,VP)=2.*U/R	BVEC0300
IF (C3) 7,7,8	BVEC0310
7 CONTINUE	BVEC0320
WRITE OUTPUT TAPE NOUT,100	BVEC0330
100 FORMAT(32H MOTION IS ELLIPTIC OR PARABOLIC)	BVEC0340
GO TO 25	BVEC0350
8 CONTINUE	BVEC0360
P=D**2/U	BVEC0370
E2=1.+P*C3/U	BVEC0380
E = SQRTF(E2)	BVEC0390
A=U/C3	BVEC0400
SEM2=E2=1.	BVEC0410
SEM1=SQRTF(SEM2)	BVEC0420
ASE=A*SEM2/E	BVEC0430
SE = SEM1/E	BVEC0440
RDOT=DOT(XP,VP)/R	BVEC0450
CTHET=(P-R)/(E+R)	BVEC0460
STHET=(RDOT*SQRTF(P/U))/E	BVEC0470

BVEC - 6

DO 9 J=1,3	BVEC0480
PP(J)=CTHET*RB(J)-STHET*RM(J)	BVEC0490
QQ(J)=STHET*RB(J)+CTHET*RM(J)	BVEC0500
S(J)=PP(J)/E+SE*QQ(J)	BVEC0510
B(J)=ASE*PP(J)-A*SE*QQ(J)	BVEC0520
9 CONTINUE	BVEC0530
S2=SQRTF(S(1)**2+S(2)**2)	BVEC0540
TT(1)=S(2)/S2	BVEC0550
TT(2)=-S(1)/S2	BVEC0560
TT(3)=0,	BVEC0570
CALL CROSS(S,TT,RR)	BVEC0580
BD(1)=DOT(B,TT)	BVEC0590
BD(2)=DOT(B,RR)	BVEC0600
I=I	BVEC0610
GO TO (10,11,12,13,14,15,16),I	BVEC0620
10 CONTINUE	BVEC0630
DO 17 J=1,2	BVEC0640
BV(J)=BD(J)	BVEC0650
17 CONTINUE	BVEC0660
BV(3)=SQRTF(C3)	BVEC0670
XP(1)=XP(1)+10.	BVEC0680
GO TO 5	BVEC0690
11 CONTINUE	BVEC0700
DO 18 J=1,2	BVEC0710
PBV(J,1)=(BD(J)-BV(J))/10.	BVEC0720
18 CONTINUE	BVEC0730
XP(1)=XP(1)-10.	BVEC0740
XP(2)=XP(2)+10.	BVEC0750
GO TO 5	BVEC0760
12 CONTINUE	BVEC0770
DO 19 J=1,2	BVEC0780
PBV(J,2)=(BD(J)-BV(J))/10.	BVEC0790
19 CONTINUE	BVEC0800
XP(2)=XP(2)-10.	BVEC0810
XP(3)=XP(3)+10.	BVEC0820
GO TO 5	BVEC0830
13 CONTINUE	BVEC0840
DO 20 J=1,2	BVEC0850
PBV(J,3)=(BD(J)-BV(J))/10.	BVEC0860
20 CONTINUE	BVEC0870
XP(3)=XP(3)-10.	BVEC0880
VP(1)=VP(1)+.01	BVEC0890
GO TO 5	BVEC0900
14 CONTINUE	BVEC0910
DO 21 J=1,2	BVEC0920
PBV(J,4)=(BD(J)-BV(J))*100.	BVEC0930
21 CONTINUE	BVEC0940
VP(1)=VP(1)-.01	BVEC0950
VP(2)=VP(2)+.01	BVEC0960
GO TO 5	BVEC0970
15 CONTINUE	BVEC0980

DO 22 J=1,2	BVEC0990
PBV(J,5)=(BD(J)-BV(J))*100.	BVEC1000
22 CONTINUE	BVEC1010
VP(2)=VP(2)+.01	BVEC1020
VP(3)=VP(3)+.01	BVEC1030
GO TO 5	BVEC1040
16 CONTINUE	BVEC1050
DO 23 J=1,2	BVEC1060
PBV(J,6)=(BD(J)-BV(J))*100.	BVEC1070
23 CONTINUE	BVEC1080
VP(3)=VP(3)+.01	BVEC1090
5 CONTINUE	BVEC1100
VIN=SQRTF(C3)	BVEC1110
UR2=1.*U/R**3	BVEC1120
UR3=UR2/VIN	BVEC1130
DO 24 I=1,3	BVEC1140
J=I+3	BVEC1150
PBV(3,J)=VP(I)/VIN	BVEC1160
PBV(3,I)=UR3*XP(I)	BVEC1170
24 CONTINUE	BVEC1180
25 CONTINUE	BVEC1190
RETURN	BVEC1200
END	BVEC

Subroutine: CHNGP

Purpose: To choose the appropriate body center as a function of distance from the present central body.

Calling Sequence:

CALL CHNGP (NOR, IOR, RAD)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	NOR	1			New body center
I	IOR	1			Present body center
I	RAD	6		Km.	RAD(I) = distance from body I to vehicle

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

Method of Selecting Body Center

<u>Present Central Body</u>	<u>New Central Body</u>	
1) Earth	Sun	$R_1 \geq 25 \times 10^5$
	Earth	$R_2 \geq 3 \times 10^4$
	Moon	$R_2 \leq 3 \times 10^4$
2) Moon	Moon	$R_2 < 3 \times 10^4$
	Earth	$R_2 \geq 3 \times 10^4$
3) Sun	Earth	$R_1 \leq 25 \times 10^5$
	Venus	$R_4 < 25 \times 10^5$
	Mars	$R_5 < 25 \times 10^5$
	Jupiter	$R_6 < 25 \times 10^5$
	Sun	(if none of above)
4) Venus	Venus	$R_4 < 25 \times 10^5$
	Sun	$R_4 \geq 25 \times 10^5$
5) Mars	Mars	$R_5 < 25 \times 10^5$
	Sun	$R_5 \geq 25 \times 10^5$
6) Jupiter	Jupiter	$R_6 \geq 25 \times 10^5$
	Sun	$R_6 < 25 \times 10^5$

where $R_i = \text{RAD}(I) = \text{distance from body (i) to the vehicle.}$


```

      LABEL
      SYMBOL TABLE:
C2002
      SUBROUTINE CHNGP(NOR,IOR,RAD)
      DIMENSION RAD(6)
      IO = IOR
      NOR = IOR
      GO TO (1,2,3,4,4,4), IO
1  IF (RAD(1)-2500000.) 11,12,12
11 IF (RAD(2)-30000.) 13,14,14
12 NOR = 3
   GO TO 14
13 NOR = 2
14 RETURN
   2 IF (RAD(2)-30000.) 14,21,21
21 NOR = 1
   GO TO 14
   3 IF (RAD(1)-2500000.) 31,31,32
31 NOR = 1
   GO TO 14
32 DO 34 I=4,6
   IF (RAD(I)-2500000.) 33,34,34
33 NOR = I
   GO TO 14
34 CONTINUE
   GO TO 14
   4 IF (RAD(IO)-2500000.) 14,41,41
41 NOR = 3
   GO TO 14
      END

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CHNG
CHNG
CHNG
CHNG0000
CHNG0010
CHNG0020
CHNG0025
CHNG0030
CHNG0040
CHNG0050
CHNG0060
CHNG0070
CHNG0080
CHNG0090
CHNG0100
CHNG0110
CHNG0120
CHNG0130
CHNG0140
CHNG0150
CHNG0160
CHNG0170
CHNG0180
CHNG0190
CHNG0200
CHNG0210
CHNG0220
CHNG0230
CHNG0240
CHNG

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Subroutine: COMPHQ

Purpose: To compute the H matrix of measurement partials with respect to the vehicle state and the variance of the measurements. The subroutine is called by ONBTR, on-board tracking subroutine, and MONBTR, the moon beacon tracking subroutine. The types of measurements which are evaluated are range, right ascension, declination, and range rate. After computation of the H matrix and the measurement error, subroutine CORRTP is called to perform the filtering of the measurement and updating of the state covariance matrix, P.

Calling Sequence:

CALL COMPHQ (JJJ, KK, NN)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	JJJ	1			Type of measurement
I	KK	1			On-board or moon beacon
I	NN	1			Key for locating constants in
					storage

Common storages used or required:

T, S, C, IC

Subroutines required:

CORRTP, DOT

Functions required:

SQRT

Approximate number of storages required:

388 DEC

Calling Sequence Elaboration

The calling sequence of COMPHQ consists of CALL COMPHQ (JJJ, KK, NN) where:

JJJ is a key which indicates the type of measurement being performed.

1. Range
2. Right ascension
3. Declination
4. Range rate

KK is a key which indicates if the measurements being made are:
(1) on-board measurements or (2) moon beacons.

NN is a key which is used to obtain constants out of the common S array.

COMPHQ Partial Derivatives

To perform the covariance matrix updating for on-board observations and moon based beacons, a number of partial derivatives are required. The partials are derived in the following paragraphs.

The following quantities and relationships are used in the derivations. The vehicle's position, \vec{X} , and velocity, $\dot{\vec{X}}$, relative to the celestial body or moon beacon are obtained from common. These vectors may be written as:

$$\vec{X} = \begin{pmatrix} X_1 \\ X_2 \\ X_3 \end{pmatrix} = -\vec{X}_V + \vec{X}_B = \begin{pmatrix} -X_V + X_B \\ -Y_V + Y_B \\ -Z_V + Z_B \end{pmatrix}$$

$$\dot{\vec{X}} = \begin{pmatrix} \dot{X}_1 \\ \dot{X}_2 \\ \dot{X}_3 \end{pmatrix} = -\dot{\vec{X}}_V + \dot{\vec{X}}_B$$

Two relationships which will be used in the derivation are:

$$\frac{\partial \text{PAR}}{\partial \vec{X}} = - \frac{\partial \text{PAR}}{\partial \vec{X}_V}$$

$$\frac{\partial \text{PAR}}{\partial \vec{X}} = - \frac{\partial \text{PAR}}{\partial \dot{\vec{X}}_V}$$

The FORTRAN program names for the above vector are as follows:

<u>FORTTRAN</u> <u>NAME</u>	<u>DIMENSION</u>	<u>DERIVATION</u> <u>NAME</u>	<u>DIMENSION</u>
XREL	(3)	\vec{X}	(3)
VREL	(3)	$\dot{\vec{X}}$	(3)

The quantities being measured are the following:

$$R = \text{RANGE} = |\vec{X}| = (\vec{X} \cdot \vec{X})^{1/2}$$

$$R = \text{Range Rate} = \frac{d}{dt} |\vec{X}| = \frac{\vec{X} \cdot \dot{\vec{X}}}{R}$$

$$RA = \tan^{-1} \left\{ \frac{X_2}{X_1} \right\}$$

$$DEC = \sin^{-1} \left\{ \frac{X_3}{R} \right\}$$

- A. The following is a derivation of the partials relating the types of measurements and the vehicle state. In the program, these partials are used as a row vector. The FORTRAN name of the vector is H. H may be written as follows:

$$H = \left(\frac{\partial \text{MEAS}}{\partial X_V}, \frac{\partial \text{MEAS}}{\partial Y_V}, \frac{\partial \text{MEAS}}{\partial Z_V}, \frac{\partial \text{MEAS}}{\partial \dot{X}_V}, \frac{\partial \text{MEAS}}{\partial \dot{Y}_V}, \frac{\partial \text{MEAS}}{\partial \dot{Z}_V} \right)$$

(1) Derivation of partials for range measurement.

$$R = (\vec{X} \cdot \vec{X})^{1/2}$$

$$H_R = \left(\frac{\partial R}{\partial \vec{X}_V}; \frac{\partial R}{\partial \vec{X}_V} \right) = \left(-\frac{X_1}{R}; -\frac{X_2}{R}; -\frac{X_3}{R}; 0; 0; 0 \right)$$

(2) Derivation of partials for range rate measurement.

$$\dot{R} = \frac{\vec{X} \cdot \dot{\vec{X}}}{R}$$

$$H_{RR} = \left(\frac{\partial \dot{R}}{\partial \vec{X}_V}; \frac{\partial \dot{R}}{\partial \vec{X}_V} \right) = \left(-\frac{\dot{X}_1}{R} + \frac{\dot{R}}{R^2} X_1; -\frac{\dot{X}_2}{R} + \frac{\dot{R}}{R^2} X_2; -\frac{\dot{X}_3}{R} + \frac{\dot{R}}{R^2} X_3; \right. \\ \left. \frac{X_1}{R}; \frac{X_2}{R}; \frac{X_3}{R} \right)$$

(3) Derivation of partials for right ascension measurement.

$$RA = \tan^{-1} \left(\frac{X_2}{X_1} \right) \equiv \tan^{-1} \gamma$$

$$\frac{\partial RA}{\partial PAR} = (1 + \gamma^2)^{-1} \frac{\partial \gamma}{\partial PAR}$$

$$(1 + \gamma^2)^{-1} = \frac{X_1^2}{X_1^2 + X_2^2}$$

$$H_{RA} = \left(\frac{\partial RA}{\partial \vec{X}_V}; \frac{\partial RA}{\partial \vec{X}_V} \right) = \left(\frac{X_2}{X_1^2 + X_2^2}; \frac{X_1}{X_1^2 + X_2^2}; 0; 0; 0; 0 \right)$$

(4) Derivation of partials for declination measurement.

$$\text{DEC} = \sin^{-1} \left(\frac{X_3}{R} \right) \equiv \sin^{-1} \gamma$$

$$\frac{\partial \text{DEC}}{\partial \text{PAR}} = [1 - \gamma^2]^{-1/2} \frac{\partial \gamma}{\partial \text{PAR}}$$

$$[1 - \gamma^2]^{-1/2} = \frac{R}{\sqrt{X_1^2 + X_2^2}}$$

$$H_{\text{DEC}} = \left(\frac{\partial \text{DEC}}{\partial \vec{X}_V}; \frac{\partial \text{DEC}}{\partial \vec{X}_V} \right) = \left(\frac{X_1 X_3}{\sqrt{X_1^2 + X_2^2} R^2}; \frac{X_2 X_3}{R^2 \sqrt{X_1^2 + X_2^2}}; \frac{\sqrt{X_1^2 + X_2^2}}{R^2}; \right. \\ \left. 0; 0; 0 \right)$$

B. In order to include errors in the measurements being made due to station location errors and time bias, the partials of the measurements with respect to latitude, longitude, altitude, and time are required. In the program, the station location errors are used as a row vector with FORTRAN name DUM. DUM may be written as follows:

$$\text{DUM} = \left(\frac{\partial \text{MEAS}}{\partial \text{LAT}}; \frac{\partial \text{MEAS}}{\partial \text{LON}}; \frac{\partial \text{MEAS}}{\partial \text{ALT}} \right)$$

The following matrices are obtained from MONBTR and used in the computation of DUM.

$$\text{STPARS} = \begin{pmatrix} \frac{\partial X_1}{\partial \text{LAT}} & \frac{\partial X_1}{\partial \text{LON}} & \frac{\partial X_1}{\partial \text{ALT}} \\ \frac{\partial X_2}{\partial \text{LAT}} & \frac{\partial X_2}{\partial \text{LON}} & \frac{\partial X_2}{\partial \text{ALT}} \\ \frac{\partial X_3}{\partial \text{LAT}} & \frac{\partial X_3}{\partial \text{LON}} & \frac{\partial X_3}{\partial \text{ALT}} \end{pmatrix}$$

$$\text{STPARD} = \begin{pmatrix} \frac{\partial \dot{X}_1}{\partial \text{LAT}} & \frac{\partial \dot{X}_1}{\partial \text{LON}} & \frac{\partial \dot{X}_1}{\partial \text{ALT}} \\ \frac{\partial \dot{X}_2}{\partial \text{LAT}} & \frac{\partial \dot{X}_2}{\partial \text{LON}} & \frac{\partial \dot{X}_2}{\partial \text{ALT}} \\ \frac{\partial \dot{X}_3}{\partial \text{LAT}} & \frac{\partial \dot{X}_3}{\partial \text{LON}} & \frac{\partial \dot{X}_3}{\partial \text{ALT}} \end{pmatrix}$$

(1) Derivation of range measurement error partials.

$$\frac{\partial R}{\partial LAT} = \sum_{i=1}^3 \frac{\partial R}{\partial X_i} \frac{\partial X_i}{\partial LAT}$$

$$\frac{\partial R}{\partial LAT} = \sum_{i=1}^3 -H_R(1,i) \text{ STPARS}(i,1)$$

Similarly

$$\frac{\partial R}{\partial LON} = \sum_{i=1}^3 -H_R(1,i) \text{ STPARS}(i,2)$$

$$\frac{\partial R}{\partial ALT} = \sum_{i=1}^3 -H_R(1,i) \text{ STPARS}(i,3)$$

(2) Derivation of range rate measurement error partials.

$$\frac{\partial \dot{R}}{\partial LAT} = \sum_{i=1}^3 \frac{\partial \dot{R}}{\partial X_i} \frac{\partial X_i}{\partial LAT} + \frac{\partial \dot{R}}{\partial \dot{X}_i} \frac{\partial \dot{X}_i}{\partial LAT}$$

$$\frac{\partial \dot{R}}{\partial LAT} = \sum_{i=1}^3 -H_{RR}(1,i) \text{ STPARS}(i,1) - H_{RR}(1,i+3) \text{ STPARD}(i,1)$$

Similarly

$$\frac{\partial \dot{R}}{\partial LON} = \sum_{i=1}^3 -H_{RR}(1,i) \text{ STPARS}(i,2) - H_{RR}(1,i+3) \text{ STPARD}(i,2)$$

$$\frac{\partial \dot{R}}{\partial \text{ALT}} = \sum_{i=1}^3 -H_{RR}(1,i) \text{ STPARS}(i,3) - H_{RR}(1,i+3) \text{ STPARD}(i,3)$$

(3) Derivation of right ascension measurement error partials.

$$\frac{\partial \text{RA}}{\partial \text{LAT}} = \sum_{i=1}^3 \frac{\partial \text{RA}}{\partial x_i} \frac{\partial x_i}{\partial \text{LAT}}$$

$$\frac{\partial \text{RA}}{\partial \text{LAT}} = \sum_{i=1}^3 -H_{RA}(1,i) \text{ STPARS}(i,1)$$

Similarly

$$\frac{\partial \text{RA}}{\partial \text{LON}} = \sum_{i=1}^3 -H_{RA}(1,i) \text{ STPARS}(i,2)$$

$$\frac{\partial \text{RA}}{\partial \text{ALT}} = \sum_{i=1}^3 -H_{RA}(1,i) \text{ STPARS}(i,3)$$

(4) Derivation of declination measurement error partials.

$$\frac{\partial \text{DEC}}{\partial \text{LAT}} = \sum_{i=1}^3 \frac{\partial \text{DEC}}{\partial x_i} \frac{\partial x_i}{\partial \text{LAT}}$$

$$\frac{\partial \text{DEC}}{\partial \text{LAT}} = \sum_{i=1}^3 -H_{DEC}(1,i) \text{ STPARS}(i,1)$$

Similarly

$$\frac{\partial \text{DEC}}{\partial \text{LON}} = \sum_{i=1}^3 -H_{DEC}(1,i) \text{ STPARS}(i,2)$$

$$\frac{\partial \text{DEC}}{\partial \text{ALT}} = \sum_{i=1}^3 -H_{\text{DEC}}(1,i) \text{STPARS}(i,3)$$

- (5) Derivation of time derivatives of measurement quantities to permit inclusion of time bias errors.

$$\frac{\partial R}{\partial t} = \dot{R} = \frac{\vec{X} \cdot \dot{\vec{X}}}{R}$$

$$\frac{\partial R_A}{\partial t} = \sum_{i=1}^3 \frac{\partial R_A}{\partial X_i} \frac{\partial X_i}{\partial t}$$

$$\frac{\partial R_A}{\partial t} = \sum_{i=1}^3 -H_{RA}(1,i) \dot{X}_i$$

Similarly

$$\frac{\partial \text{DEC}}{\partial t} = \sum_{i=1}^3 -H_{\text{DEC}}(1,i) \dot{X}_i$$

The errors in the measurements are computed in the following manner for station location errors and time bias.

$$\text{QQSTAT} = \left(\text{DUM}_{\text{MEAS}} \right)^2 \begin{pmatrix} \sigma^2_{\text{LAT}} \\ \sigma^2_{\text{LON}} \\ \sigma^2_{\text{ALT}} \end{pmatrix}$$

Station
Location
Error

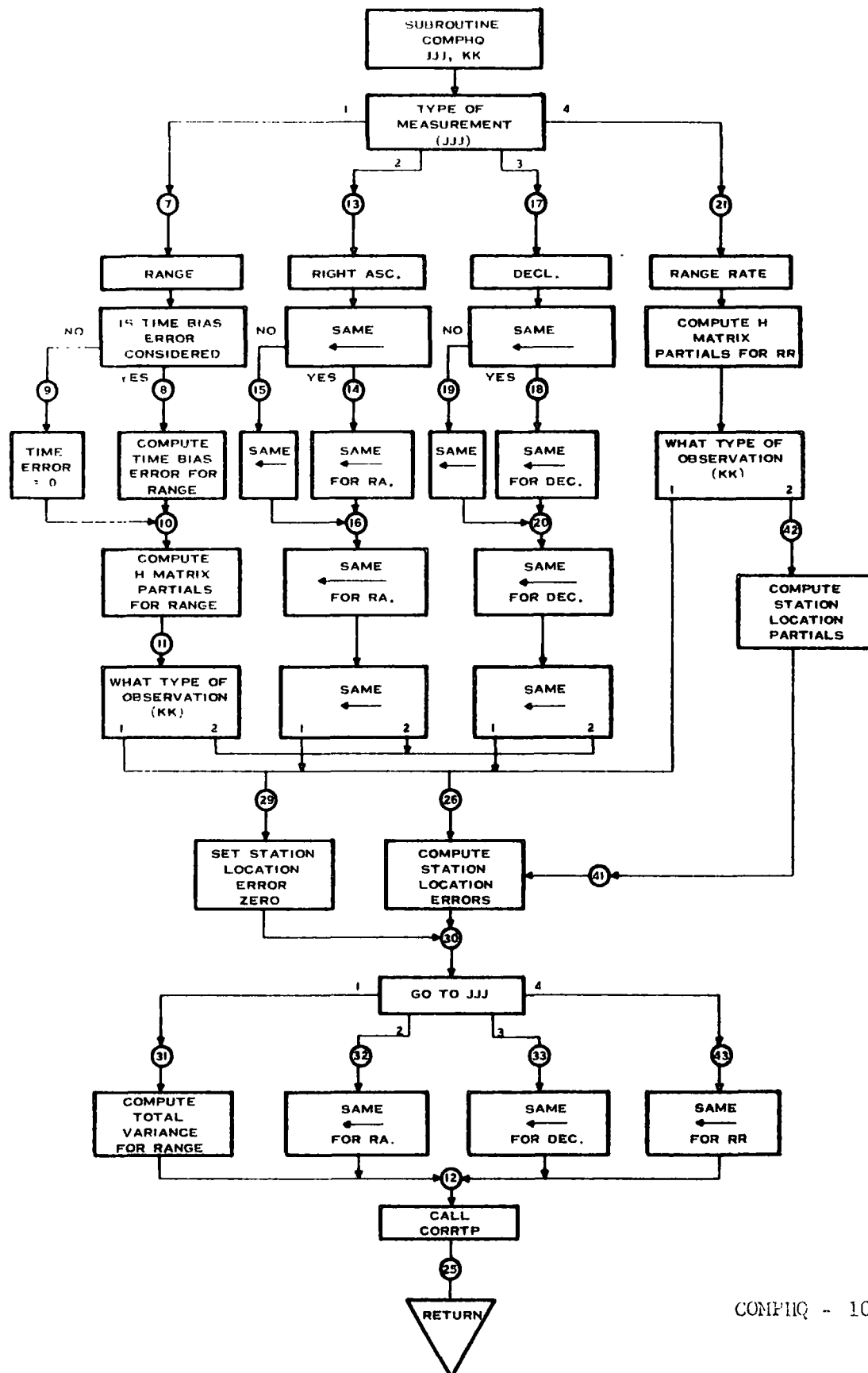
1x1

1x3

3x1

$$QQDOT = \left(\frac{\partial MEAS}{\partial t} \cdot \sigma_{TIME} \right)^2 \quad \text{Time Bias Error}$$

The computation of the H matrices and the measurement errors are the primary computations in COMPHQ. COMPHQ calls CORRTP which uses quantities to update the state covariance matrix.



COMPHQ - 10

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* LABEL
* SYMBOL TABLE
CEC2008 SUBROUTINE COMPHQ
SUBROUTINE COMPHQ(JJJ, KK, NN)
COMMON T, S, C, IC
DIMENSION T(1360), S(1000), C(1000), IC(1)
1, XREL(3), VREL(3), H(6), P(6,6), STPARS(3,3), DUM(3), OUTPUT(6)
DIMENSION STPARD(3,3)
EQUIVALENCE (T, TDUM), (S, SDUM), (C, CDUM), (IC, ICDUM)
1, (C(895), XREL), (C(898), VREL), (C(894), OBNO), (C(893), XMAG),
2(C(892), DEX), (C(891), DEN1), (C(890), DEN2), (C(788), STPARS)
3, (C(889), DEX2), (C(888), DEX3), (C(652), P), (C(973), OUTPUT)
4, (S(73), RTD)
EQUIVALENCE (C(800), STPARD)
C KK 1=ONBOARD MEASUREMENTS 2=MOON BEACONS
JJJ 1=RANGE 2=RIGHT ASC. 3=DECL. 4=RANGE RATE
NN=NN
JJJ=JJJ
KK=KK
NNN=NN/5+657
GO TO (7,13,17,21), JJJ
7 CONTINUE
IF(S(NN+8))9,9,8
8 CONTINUE
GET HERE TO COMPUTE ERROR IN RANGE OBS. DUE TO TIME BIAS.
RDOT=DOT(XREL, VREL)*DEX3
RDOT=RANGE RATE
OUTPUT(2)=RDOT
RDOT2=RDOT*RDOT
QQRDOT=RDOT2*S(NN+8)
QQRDOT=RANGE VARIANCE DUE TO TIME BIAS
GO TO 10
9 CONTINUE
QQRDOT=0.
10 CONTINUE
THE FOLLOWING ARE H MATRIX CALCULATIONS FOR RANGE
DO 11 I=1,3
K=I+3
H(I)=-XREL(I)*DEX3
H(K)=0.
11 CONTINUE
GO TO (29,26), KK
31 CONTINUE
QQ=S(NN)/OBNO+S(NN+4)+QQRDOT+S(425)*XMAG**2+QQSTAT
QQ=TOTAL RANGE VARIANCE=INSTR.*BIAS+TIME BIAS ERROR+SPEED LIGHT
+STATION LOCATION ERRORS
12 CONTINUE
CALL CORRTP (QQ, H, P)
CORRTP UPDATES COVARIANCE MATRIX FOR MEASUREMENT
GO TO 25
13 CONTINUE

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COMP
COMP
COMP
COMP0000
COMP0010
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COMP0025
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COMP0240
COMP0250
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COMP0270
COMP0280
COMP0290
COMP0300
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COMP0320
COMP0330
COMP0340
COMP0350
COMP0360
COMP0370
COMP0380
COMP0390
COMP0400
COMP0410
COMP0420
COMP0430

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	IF(S(NN+8))15,15,14	COMP0440
14	CONTINUE	COMP0450
C	GET HERE TO COMPUTE ERROR IN RA MEASUREMENT DUE TO CLOCK BIAS	COMP0460
	RADOT=(VREL(2)*XREL(1)-VREL(1)*XREL(2))*DEN2	COMP0470
	CUTPUT(4)=RADOT*RTD	COMP0475
C	RADOT=RIGHT ASCENSION RATE	COMP0480
	RADOT2=RADOT*RADOT	COMP0490
	QQRADT=RADOT2*S(NN+8)	COMP0500
C	QQRADT=RIGHT ASCENSION VARIANCE DUE TO TIME BIAS	COMP0510
	GO TO 16	COMP0520
15	CONTINUE	COMP0530
	QQRADT=0.	COMP0540
16	CONTINUE	COMP0550
C	THE FOLLOWING ARE H MATRIX CALCULATIONS FOR RA	COMP0560
	H(6)=0.	COMP0570
	H(5)=0.	COMP0580
	H(4)=0.	COMP0590
	H(3)=0.	COMP0600
	H(1)= XREL(2)*DEN2	COMP0610
	H(2)=-XREL(1)*DEN2	COMP0620
	GO TO (29,26),KK	COMP0630
32	CONTINUE	COMP0640
	QQ=S(NN+1)/OBNO+S(NN+5)+QQRADT+QQSTAT	COMP0650
C	QQ=TOTAL RIGHT ASCENSION VARIANCE	COMP0660
	GO TO 12	COMP0670
17	CONTINUE	COMP0680
	IF(S(NN+8))19,19,18	COMP0690
18	CONTINUE	COMP0700
C	GET HERE TO COMPUTE ERROR IN DEC. MEAS. DUE TO CLOCK BIAS	COMP0710
	CRUD=XREL(1)*VREL(1)+XREL(2)*VREL(2)	COMP0720
	CRUD2=VREL(3)*DEX-XREL(3)*CRUD	COMP0730
	DEDOT=CRUD2/(SQRTF(DEX)*DEX2)	COMP0740
	OUTPUT(6)=DEDOT*RTD	COMP0745
	DEDOT2=DEDOT*DEDOT	COMP0750
	QQDEDT=DEDOT2*S(NN+8)	COMP0760
C	QQDEDT=DECLINATION VARIANCE DUE TO TIME BIAS	COMP0770
	GO TO 20	COMP0780
19	CONTINUE	COMP0790
	QQDEDT=0.	COMP0800
20	CONTINUE	COMP0810
C	THE FOLLOWING ARE H MATRIX COMP. FOR DECLINATION	COMP0820
	H(4)=0.	COMP0830
	H(5)=0.	COMP0840
	H(6)=0.	COMP0850
	H(1)= XREL(1)*XREL(3)*DEN1	COMP0860
	H(2)= XREL(2)*XREL(3)*DEN1	COMP0870
	H(3)=-DEX*DEN1	COMP0880
	GO TO (29,26),KK	COMP0890
33	CONTINUE	COMP0900
	QQ=S(NN+2)/OBNO+S(NN+6)+QQDEDT+QQSTAT	COMP0910
C	QQ=TOTAL DECLINATION VARIANCE	COMP0920

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GO TO 12
21 CONTINUE
THE FOLLOWING ARE H MATRIX COMP. FOR RANGE RATE
RDOT=DOT(XREL,VREL)*DEX3
OUTPUT(2)=RDOT
DO 22 J=1,3
K=J+3
H(K)=XREL(J)*DEX3
H(J)=DEX3*(VREL(J)+H(K)*RDOT)
22 CONTINUE
GO TO (29,42),KK
42 CONTINUE
DO 40 I=1,3
DUM(I)=0.
DO 40 J=1,3
JJ=J+3
40 DUM(I)=DUM(I)+H(J)*STPARS(J,I)+H(JJ)*STPARD(J,I)
GO TO 41
43 CONTINUE
QQ=S(NN+3)/OBNO+S(NN+7)*QQSTAT
QQ=RANGE RATE VARIANCE
GO TO 12
26 CONTINUE
THE FOLLOWING COMPUTATIONS ARE FOR STATION LOCATION ERRORS
DO 27 I=1,3
DUM(I)=0.
DO 27 J=1,3
DUM(I)=DUM(I)+H(J)*STPARS(J,I)
27 CONTINUE
41 CONTINUE
QQSTAT=0.
DO 28 I=1,3
L=NNN+I
QQSTAT=QQSTAT+(DUM(I)**2)*S(L)
28 CONTINUE
GO TO 30
29 CONTINUE
QQSTAT=0.
30 CONTINUE
GO TO(31,32,33,43),JJJ
25 CONTINUE
RETURN
END

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COMP093
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Subroutine: CONST1

Purpose: To read permanent or semipermanent constants into the common S array.

Calling Sequence:

CALL CONST1

Input and Output

Common storages used or required:	<u>T, S</u>
Subroutines required:	<u>None</u>
Functions required:	<u>None</u>
Approximate number of storages required:	<u>669 DEC</u>

* LABEL	CONS
* SYMBOL TABLE	CONS
CEC2026 SUBROUTINE CONST1	CONS
SUBROUTINE CONST1	CONS0000
COMMON T,S	CONS0010
DIMENSION T(1360),S(1000)	CONS0020
EQUIVALENCE (T,TDUM),(S,SDUM)	CONS0030
C PLANETARY MASSES 1-6,	CONS0040
C PLANETARY MASSES 1-6 ,ORDER EARTH,MOON,SUN,VENUS,MARS,JUPITER	CONS0050
C -KM**3/SEC2	CONS0060
S(1)=398603.2	CONS0070
S(2)=4900.7588	CONS0080
S(3)=.13271545E12	CONS0090
S(4)=324769.50	CONS0100
S(5)=42915.515	CONS0110
S(6)=.12671059E9	CONS0120
C 6-9 ARE SPARES	CONS0130
C 10-19 ARE EARTH CONSTANTS,RATE,J,H,D,EQUAT RAD,POLAR RAD	CONS0140
C RAD/SEC	CONS0150
S(10)=7.2921152E-5	CONS0160
S(11)=.162345E-2	CONS0170
S(12)=-.575E-5	CONS0180
S(13)=.7875E-5	CONS0190
S(14)=6378.2064	CONS0200
S(15)=6356.5838	CONS0210
C 20-29 ARE MOON CONSTANTS ,G,A,B,C,RAD	CONS0220
S(20)=.6671E-19	CONS0230
S(21)=.88746E29	CONS0240
S(22)=.88764E29	CONS0250
S(23)=.88801E29	CONS0260
S(24)=1738.	CONS0270
C 30-59 SUN CONSTANTS	CONS0280
C 40-49 VENUS CONSTANTS	CONS0290
C 50-59 MARS CONSTANTS	CONS0300
C 60-69 JUPITER CONSTANTS	CONS0310
C CONVERSION FACTOR DAYS TO SECONDS	CONS0320
S(70)=86400.	CONS0330
C CONVERSION FACTOR SECONDS TO DAYS	CONS0340
S(71)=1./S(70)	CONS0350
C CONVERSION FACTOR FOR DEGREES TO RADIANS	CONS0360
S(72)=.017453296	CONS0370
C CONVERSION FACTOR FOR RADIANS TO DEGREES	CONS0380
S(73)=57.29578	CONS0390
S(80)=28.48713	CONS0400
S(81)=279.42315	CONS0410
S(82)=.00257	CONS0420
S(84)=90.	CONS0430
C 111 IS TYPE OF INPUT(1)EQUATOR 1950 (2)EQUATOR OF DATE(3)	CONS0440
C EARTH=FIXED	CONS0450
C (4),(5),(6) ARE SPHERICAL INPUT IN, RESPECTIVELY, (1),(2),(3)	CONS0460
C 112 AND 113 ARE(YEAR MONTH.DAY)(HOUR MIN.SEC) OF INJECTION DATE	CONS0470

```

C 114 IS CENTRAL BODY NUMBER,(1)EARTH,(2)MOON(3)SUN(4)VENUS(5)
C MARS(6)JUPITER
C 115-120 ARE INPUT STATE CORRESPONDING TO S(111) THRU 114,
C 121 TARGET BODY
C 122 TYPE OF OUTPUT;KOUT
C S(121)=2,
C 123 TSECO
C N GOES FROM 0 TO 19
C(125)+N*15 VARIANCE OF RANGE KM**2
C(126)+N*15 VARIANCE OF AZIMUTH RAD**2
C(127)+N*15 VARIANCE OF ELEVATION RAD**2
C(128)+N*15 VARIANCE OF RANGE RATE KM**2/SEC**2
C(129)+N*15 VARIANCE OF LATITUDE RAD**2
C(130)+N*15 VARIANCE OF LONGITUDE RAD**2
C(131)+N*15 VARIANCE OF ALTITUDE KM**2
C(132)+N*15 VARIANCE OF AZIMUTH BIASES RAD**2
C(133)+N*15 VARIANCE OF ELEVATION BIASES RAD**2
C(134)+N*15 LATITUDE OF STATION DEG
C(135)+N*15 LONGITUDE OF STATION DEG
C(136)+N*15 ALTITUDE OF STATION KM
C(137)+N*15 STATION NAME
C(138)+N*15 PERIOD OF OBSERVATION SEC
C(139)+N*15 VARIANCE OF TIME BIAS SEC**2
C STATION 1 ANTIGUA RADAR 91.1
C S(125)=.000225
C S(126)=.000004
C S(127)=.000004
C S(128)=.00000001
C S(129)=.0000000001
C S(130)=.0000000001
C S(131)=.0001
C S(134)=17.0267
C S(135)=298.2247
C S(136)=0.
C S(137)=6HANTIG
C S(138)=1.
C STATION 2 ASCENSION RADAR 12.16
C S(140)=.000225
C S(141)=.000004
C S(142)=.000004
C S(143)=.00000001
C S(144)=.0000000001
C S(145)=.0000000001
C S(146)=.0001
C S(149)=7.898
C S(150)=345.587393
C S(151)=0.
C S(152)=6HASCENS
C S(153)=1.
C STATION 3 MILLSTONE HILL RADAR
C S(155)=.000225

```

S(156)=.000004
S(157)=.000004
S(158)=.00000001
S(159)=.0000000001
S(160)=.0000000001
S(161)=.0001
S(164)=42.4232
S(165)=288.5080
S(166)=0.
S(167)=6HMLHIL
S(168)=1.

C STATION 4 MOBILE STATION MTS

S(170)= 2500.E-6
S(171)= .04 E-6
S(172)= .04 E-6
S(173)= .04 E-6
S(174)= 1. E-10
S(175)= 1. E-10
S(176)= 9. E-6
S(177)= .0016E-6
S(178)= .0016E-6
S(179)=-25.88472
S(180)= 27.70528
S(181)= 1.54302
S(182)=6HMOBMTS
S(183)= 30.

C STATION 5 AMR TRACKER GE

S(184)= 9.E-6
S(185)=.000225
S(186)=.000004
S(187)=.000004
S(188)=.00000001
S(189)=.0000000001
S(190)=.0000000001
S(191)=.0001
S(194)=28.278103
S(195)=279.418297
S(196)=0.
S(197)=6HGEAMR
S(198)=1.

C STATION 6 BERMUDA

S(200)=.000225
S(201)=.000004
S(202)=.000004
S(203)=.00000001
S(204)=.0000000001
S(205)=.0000000001
S(206)=.0001
S(209)=32.160973
S(210)=295.299179
S(211)=0.

CONS0990
CONS1000
CONS1010
CONS1020
CONS1030
CONS1040
CONS1050
CONS1060
CONS1070
CONS1080
CONS1090
CONS1100
CONS1110
CONS1120
CONS1130
CONS1140
CONS1150
CONS1160
CONS1170
CONS1180
CONS1190
CONS1200
CONS1210
CONS1220
CONS1230
CONS1240
CONS1250
CONS1260
CONS1270
CONS1280
CONS1290
CONS1300
CONS1310
CONS1320
CONS1330
CONS1340
CONS1350
CONS1360
CONS1370
CONS1380
CONS1390
CONS1400
CONS1410
CONS1420
CONS1430
CONS1440
CONS1450
CONS1460
CONS1470
CONS1480
CONS1490

S(257)=6HGBIRAD
S(258)=1.0
C STATION 10 JOHANNESBURG
C 50M SIG
S(260) =2500.E-6
C .2MIL
S(261) =.04 E-6
C .2MIL
S(262) =.04 E-6
C .2M/SEC
S(263) =.04 E-6
C 63.78M
S(264) =1.E-10
C 63.78M
S(265) =1.E-10
C 3M SIG
S(266) = 9.E-6
C .04MR
S(267) = .0016E-6
C .04MR
S(268) = .0016E-6
C DEG
S(269) =-25.88735
C DEG
S(270) = 27.68478
C KM
S(271) = 1.38192
S(272)=6HJOHABG
C SEC
S(273) = 30.
C 3MS SIG
S(274) = 9.E-6
C STATION IN HAWAII
S(275)=.000225
S(276)=.000004
S(277)=.000004
S(278)=.00000001
S(279)=.0000000001
S(280)=.0000000001
S(281)=.0001
S(284)=18.823066
S(285)=204.314722
S(286)=0.
S(287)=6HHAWAII
S(288)=1.0
C STATION 12 JODRELL BANK
S(290)=.000225
S(291)=.000004
S(292)=.000004
S(293)=.00000001
S(294)=.0000000001

CONS2010
CONS2020
CONS2030
CONS2040
CONS2050
CONS2060
CONS2070
CONS2080
CONS2090
CONS2100
CONS2110
CONS2120
CONS2130
CONS2140
CONS2150
CONS2160
CONS2170
CONS2180
CONS2190
CONS2200
CONS2210
CONS2220
CONS2230
CONS2240
CONS2250
CONS2260
CONS2270
CONS2280
CONS2290
CONS2300
CONS2310
CONS2320
CONS2330
CONS2340
CONS2350
CONS2360
CONS2370
CONS2380
CONS2390
CONS2400
CONS2410
CONS2420
CONS2430
CONS2440
CONS2450
CONS2460
CONS2470
CONS2480
CONS2490
CONS2500
CONS2510

S(295)=.0000000001
S(296)=.0001
S(299)=53.049636
S(300)=357.693889
S(301)=0.
S(302)=6HJQDBNK
S(303)=1.0
STATION 13 PUERTO RICO RADAR 9.1
S(305)=.000225
S(306)=.000004
S(307)=.000004
S(308)=.00000001
S(309)=.0000000001
S(310)=.0000000001
S(311)=.0001
S(314)=18.060396
S(315)=292.911805
S(316)=0.
S(317)=6HPURICO
S(318)=1.0
STATION 14 SAN SALVADORE
S(320)=.000225
S(321)=.000004
S(322)=.000004
S(323)=.00000001
S(324)=.0000000001
S(325)=.0000000001
S(326)=.0001
S(329)=23.173566
S(330)=285.4956
S(331)=0.
S(332)=6HSANSAL
S(333)=1.0
STATION 15 WOOMERA
50W SIG
S(335) = 2500.E=6
.2MIL
S(336) = .04E=6
.2MIL
S(337) = .04E=6
.2M/SEC
S(338) = .04E=6
63.78M
S(339) = 1.E=10
63.78M
S(340) = 1.E=10
3M
S(341) = .9.E=6
.04MR
S(342) = .0016E=6
.04MR

[illegible]

C

C

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C

S(343) = .0016E-6
S(344) = -31,38287
S(345) = 136,88502
S(346) = .15079
S(347) = 6HWOMERA
SEC
S(348) = 30.
3MS
S(349) = 9.E-6
STATION 16 JPL CAPE CANAUERAL
S(350) = .000225
S(351) = .000004
S(352) = .000004
S(353) = .00000001
S(354) = .0000000001
S(355) = .0000000001
S(356) = .0001
DEG
S(359) = 28,48713
DEG
S(360) = 279.42315
KM
S(361) = .00257
S(362) = 6HCAPJET
S(363) = 1.0
425 = SPEED OF LIGHT ACCURACY
STATION 17 MAJUNGA
S(369) = .0000000001
S(370) = .0000000001
S(371) = .0001
S(374) = -15,216666
S(375) = 46.38333
S(377) = 6HMAJUNG
S(378) = 30.
STATION 18 CARNARVCN
S(384) = .0000000001
S(385) = .0000000001
S(386) = .0001
S(389) = -24,8666
S(390) = 113.63333
S(392) = 6HCAHNVN
S(393) = 30.
STATION 19 ROSMAN
S(399) = .0000000001
S(400) = .0000000001
S(401) = .0001
S(404) = 35.20000
S(405) = 277.1333
S(407) = 6HROSMAN
S(408) = 30.
S(425) = 1.E-12

CONS3030
CONS3040
CONS3050
CONS3060
CONS3070
CONS3080
CONS3090
CONS3100
CONS3110
CONS3120
CONS3130
CONS3140
CONS3150
CONS3160
CONS3170
CONS3180
CONS3190
CONS3200
CONS3210
CONS3220
CONS3230
CONS3240
CONS3250
CONS3260
CONS3265
CONS3270
CONS3271
CONS3272
CONS3273
CONS3274
CONS3275
CONS3276
CONS3277
CONS3278
CONS3279
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CONS3285
CONS3286
CONS3287
CONS3288
CONS3289
CONS3290
CONS3291
CONS3292
CONS3293
CONS3294
CONS3295

C FROM S(426) TO S(470) IS ONBOARD ERROR DATA

S(475)=1.0
S(476)=100.
S(477)=200.
S(478)=300.
S(479)=400.
S(480)=500.
S(481)=600.
S(485)=.03

C N GOES FROM 0 TO 9 LUNAR BASED BEACONS

C (500)+N*15	VARIANCE OF RANGE	KM2
C (501)+N*15	VARIANCE OF AZIMUTH	RAD2
C (502)+N*15	VARIANCE OF ELEVATION	RAD2
C (503)+N*15	VARIANCE OF RANGE RATE	KM2/SEC2
C (504)+N*15	VARIANCE OF LATITUDE	RAD2
C (505)+N*15	VARIANCE OF LONGITUDE	RAD2
C (506)+N*15	VARIANCE OF ALTITUDE	KM2
C (507)+N*15	VARIANCE OF AZIMUTH BIAS	RAD2
C (508)+N*15	VARIANCE OF ELEVATION BIAS	RAD2
C (509)+N*15	LATITUDE OF STATION	DEG
C (510)+N*15	LONGITUDE OF STATION	DEG
C (511)+N*15	ALTITUDE OF STATION	KM
C (512)+N*15	STATION NAME	
C (513)+N*15	PERIOD OF OBSERVATION	SEC
C (514)+N*15	SPARE	
C (650) TO (685)	IS INITIAL P MATRIX	
C (686) TO (721)	INITIAL RAR MATRIX	
C (722) TO (739)	TRANSITION MATRIX FTA GUIDANCE	
S(900)=6378,165		
S(901)=1738,		
RETURN		
END		

CONS330
CONS331
CONS332
CONS333
CONS334
CONS335
CONS336
CONS337
CONS338
CONS339
CONS340
CONS341
CONS342
CONS343
CONS344
CONS345
CONS346
CONS347
CONS348
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CONS355
CONS356
CONS357
CONS358
CONS359
CONS

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Subroutine: CONVPI

Purpose: Subroutine CONVPI transforms the input covariance matrices to the mean equinox of 1950 coordinate system. The input covariance matrices may be input in four coordinate systems:

1. Instantaneous launch pad tangent plane
2. Instantaneous injection tangent plane
3. True equinox of date
4. Mean equinox of 1950.

Calling Sequence:

CALL CONVPI (ITYPE, PIN, POUT)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	ITYPE	1			Logic key which indicates the type of input coordinate frame
I	PIN	21		Km ² , (Km/Sec) ²	Upper half of input covariance matrix in vector form
O	POUT	6, 6	$E(\vec{X}_{50} \vec{X}_{50}^T)$	Km ² , (Km/sec) ²	Output covariance matrix (1950)

Common storages used or required:

T, S, C, IC

Subroutines required:

CROSS, GHA, MULT, NUTAIT, PTRAN,
ROTEQ, TIMED, TRAC

Functions required:

COS SIN
FNORM

Approximate number of storages required:

476 DEC

Calling Sequence Elaboration

The calling sequence consists of CALL CONVPI (INTYPE, PIN, POUT)
where:

INTYPE is a logic key which indicates the type of coordinate system in which the input covariance matrix is expressed. The range of the key is one to five. One through four indicate the four coordinate systems described above. A five in the call sequence indicates that the input matrix is in the same coordinate frame as the input matrix of the preceding call of the subroutine.

PIN is in the input covariance matrix. The matrix must be in the form of a column matrix with dimension (21). The (21) elements represent the upper half of the input covariance matrix.

$$\text{PIN} = \begin{bmatrix} 1 & 2 & 3 & 4 & 5 & 6 \\ & 7 & 8 & 9 & 10 & 11 \\ & & 12 & 13 & 14 & 15 \\ & & & 16 & 17 & 18 \\ & & & & 19 & 20 \\ & & & & & 21 \end{bmatrix}$$

Input Elements

The required order of the input covariance matrix is the following:
For INTYPE = 1 or 2

$$\text{PIN} = \text{E} \begin{bmatrix} \text{AV} \\ \text{NOR} \\ \text{ALT} \\ \dot{\text{AV}} \\ \dot{\text{NOR}} \\ \dot{\text{ALT}} \end{bmatrix} \begin{bmatrix} \text{AV} \\ \text{NOR} \\ \text{ALT} \\ \dot{\text{AV}} \\ \dot{\text{NOR}} \\ \dot{\text{ALT}} \end{bmatrix}^T$$

6×1
 1×6

where

$$\hat{\text{AV}} \equiv \frac{\vec{\text{R}} \times \vec{\text{v}}}{|\vec{\text{R}} \times \vec{\text{v}}|} \times \frac{\vec{\text{R}}}{|\vec{\text{R}}|} = \text{coordinate along velocity}$$

$$\hat{\text{NOR}} \equiv \frac{\vec{\text{R}} \times \vec{\text{v}}}{|\vec{\text{R}} \times \vec{\text{v}}|} = \text{coordinate normal to orbit plane}$$

$$\hat{\text{ALT}} = \frac{\vec{\text{R}}}{|\vec{\text{R}}|} = \text{coordinate in direction of altitude}$$

Dots represent corresponding rates.

For INTYPE = 3 or 4

$$\text{PIN} = \text{E} \begin{bmatrix} \text{X} \\ \text{Y} \\ \text{Z} \\ \dot{\text{X}} \\ \dot{\text{Y}} \\ \dot{\text{Z}} \end{bmatrix} \begin{bmatrix} \text{X} \\ \text{Y} \\ \text{Z} \\ \dot{\text{X}} \\ \dot{\text{Y}} \\ \dot{\text{Z}} \end{bmatrix}^T$$

6×1
 1×6

POUT is the output covariance matrix in cartesian coordinates mean equator 1950.

CONVPI Transformations

INTYPE = 1 Transformation from launch pad tangent plane to 1950.

Required input constants for operation:

LAUNCH PAD COORDINATES

S(80) Altitude (KM)
 S(81) Longitude (DEG)
 S(82) Latitude (DEG)

LAUNCH AZIMUTH

S(84) Azimuth (DEG)

TIME FROM LAUNCH TO INJECTION

S(83) Time DAYS HOURS. MIN SEC

The transformation from launch pad azimuth coordinates, (AV, NOR, ALT) to mean equinox of 1950 (X_{50} , Y_{50} , Z_{50}) is obtained as follows. Subroutine TRAC is called with launch time and launch pad coordinates to obtain a set of orthogonal unit vectors. The unit vectors, in equator of date, are: \hat{U}_D , unit up vector through the launch pad, \hat{E}_D , unit east vector, and \hat{N}_D , unit north vector. These unit vectors written in matrix form represent the transformation from equator of date coordinates to launch pad coordinates of date

$$\begin{matrix} \vec{X}_{LP} \\ 3 \times 1 \end{matrix} = \begin{bmatrix} \hat{N}_D^T \\ \hat{E}_D^T \\ \hat{U}_D^T \end{bmatrix} \begin{matrix} \vec{X}_{DATE} \\ 3 \times 1 \end{matrix} \quad (1)$$

3x3

The transformation from launch pad coordinates, (N, E, U), to the desired launch azimuth coordinates, (AV, NOR, ALT), is a rotation about the \hat{U} vector by an angle equal to the launch azimuth.

$$\begin{matrix} \vec{x}_{LAZ} & = & \begin{bmatrix} \cos LAZ & \sin LAZ & 0 \\ -\sin LAZ & \cos LAZ & 0 \\ 0 & 0 & 1 \end{bmatrix} & \vec{x}_{LP} = (ROT) \vec{x}_{LP} & (2) \\ 3 \times 1 & & 3 \times 3 & 3 \times 1 & 3 \times 3 & 3 \times 1 \end{matrix}$$

substituting for \vec{x}_{LP} from equation (1) yields

$$\begin{matrix} \vec{x}_{LAZ} & = & (ROT) & \begin{bmatrix} \hat{N}_D^T \\ \hat{E}_D^T \\ \hat{U}_D^T \end{bmatrix} & \vec{x}_{DATE} & (3) \\ 3 \times 1 & & 3 \times 3 & 3 \times 3 & 3 \times 1 \end{matrix}$$

Subroutines ROTEQ and NUTAIT are called to obtain transformation matrix (AN) which is the transformation from mean equinox of 1950 to true equator of date.

$$\begin{matrix} \vec{x}_{DATE} & = & (AN) & \vec{x}_{1950} & (4) \\ 3 \times 1 & & 3 \times 3 & 3 \times 1 \end{matrix}$$

Substituting equation (4) into (3) yields

$$\begin{matrix} \vec{x}_{LAZ} & = & (ROT) & \begin{bmatrix} \hat{N}_D^T \\ \hat{E}_D^T \\ \hat{U}_D^T \end{bmatrix} & (AN) & \vec{x}_{1950} & (5) \\ 3 \times 1 & & 3 \times 3 & 3 \times 3 & 3 \times 3 & 3 \times 1 \end{matrix}$$

or

$$\begin{array}{ccccccc} \vec{x}_{1950} & = & \left\{ \begin{array}{c} (AN)^T \\ \left[\begin{array}{c} \hat{N}_D^T \\ \hat{E}_D^T \\ \hat{U}_D^T \end{array} \right]^T \\ (ROT)^T \end{array} \right\} \vec{x}_{LAZ} & = & (TRANS) \vec{x}_{LAZ} & (6) \\ 3 \times 1 & & 3 \times 3 & 3 \times 3 & 3 \times 1 & 3 \times 3 & 3 \times 1 \end{array}$$

The corresponding velocity transformation is the following:

$$\dot{\vec{x}}_{1950} = (TRANS) \dot{\vec{x}}_{LAZ} \quad (7)$$

under the assumption that $(\dot{AN}) = 0$ which implies $(TRANS) = 0$.

The 3x3 matrix, (TRANS), is the desired transformation from launch azimuth coordinates to mean equator of 1950. Subroutine PTRAN is called with a 2 in the call list to perform the desired covariance matrix transformation.

$$\begin{array}{ccccccc} E \left\{ \begin{array}{c} \vec{x}_{1950} \vec{x}_{1950}^T \end{array} \right\} & = & \left\{ \begin{array}{cc} (TRANS) & 0 \\ 3 \times 3 & 3 \times 3 \end{array} \right\} & E \left\{ \begin{array}{c} \vec{x}_{LAZ} \vec{x}_{LAZ}^T \end{array} \right\} & \left\{ \begin{array}{cc} (TRANS) & 0 \\ 0 & (TRANS) \end{array} \right\}^T & (8) \\ 6 \times 6 & & 6 \times 6 & 6 \times 6 & 6 \times 6 \end{array}$$

where \vec{x}_{1950} and \vec{x}_{LAZ} now represent the total state vector (position and velocity).

INTYPE = 2 Transformation from injection tangent plane to 1950.

The transformation from injection tangent plane coordinates, (AV, NOR, ALT), to mean equinox 1950 is obtained as follows. The unit vectors for the injection tangent plane coordinates are obtained in equator of 1950.

$$AV_{50} = \frac{\vec{R} \times \vec{v}}{|\vec{R} \times \vec{v}|} \times \frac{\vec{R}}{|\vec{R}|}$$

$$\text{NOR}_{50} = \frac{\vec{R} \times \vec{v}}{|\vec{R} \times \vec{v}|} \quad (9)$$

$$\text{ALT}_{50} = \frac{\vec{R}}{|\vec{R}|}$$

These vectors written in matrix form represent the transformation from mean equinox of 1950 to injection tangent plane

$$\begin{array}{ccc} \vec{X}_{\text{ITP}} & = & \begin{bmatrix} \hat{A}V_{50}^T \\ \hat{N}OR_{50}^T \\ \hat{A}LT_{50}^T \end{bmatrix} \vec{X}_{1950} \\ 3 \times 1 & & 3 \times 3 \quad 3 \times 1 \end{array} \quad (10)$$

or

$$\begin{array}{ccc} \vec{X}_{1950} & = & \begin{bmatrix} \hat{A}V_{50}^T \\ \hat{N}OR_{50}^T \\ \hat{A}LT_{50}^T \end{bmatrix}^T \vec{X}_{\text{ITP}} \\ 3 \times 1 & & 3 \times 3 \quad 3 \times 1 \end{array} \quad \vec{X}_{\text{ITP}} = (\text{TRANS}) \vec{X}_{\text{ITP}} \quad (11)$$

The corresponding velocity transformation is

$$\begin{array}{ccc} \dot{\vec{X}}_{1950} & = & (\text{TRANS}) \dot{\vec{X}}_{\text{ITP}} \\ 3 \times 1 & & 3 \times 3 \quad 3 \times 1 \end{array} \quad (12)$$

Subroutine PTRAN is called with a 2 in the call list and the operation presented in equation (8) is performed with the 3x3 matrix, (TRANS), defined in equation (11).

INTYPE = 3 Transformation from equator of date to equator of 1950.

The transformation from equator of date to equator of 1950 is obtained as follows. Subroutines ROTEQ and NUTAIT are called to obtain (AN), the required transformation matrix.

$$\begin{array}{ccccc} \vec{X}_{\text{DATE}} & = & (\text{AN}) & \vec{X}_{1950} & (13) \\ 3 \times 1 & & 3 \times 3 & & 3 \times 1 \end{array}$$

or

$$\begin{array}{ccccccc} \vec{X}_{1950} & = & (\text{AN})^T & \vec{X}_{\text{DATE}} & = & (\text{TRANS}) & \vec{X}_{\text{DATE}} & (14) \\ 3 \times 1 & & 3 \times 3 & & 3 \times 1 & & 3 \times 3 & & 3 \times 1 \end{array}$$

The corresponding velocity transformation is

$$\begin{array}{ccc} \dot{\vec{X}}_{1950} & = & (\text{TRANS}) \dot{\vec{X}}_{\text{DATE}} & (15) \end{array}$$

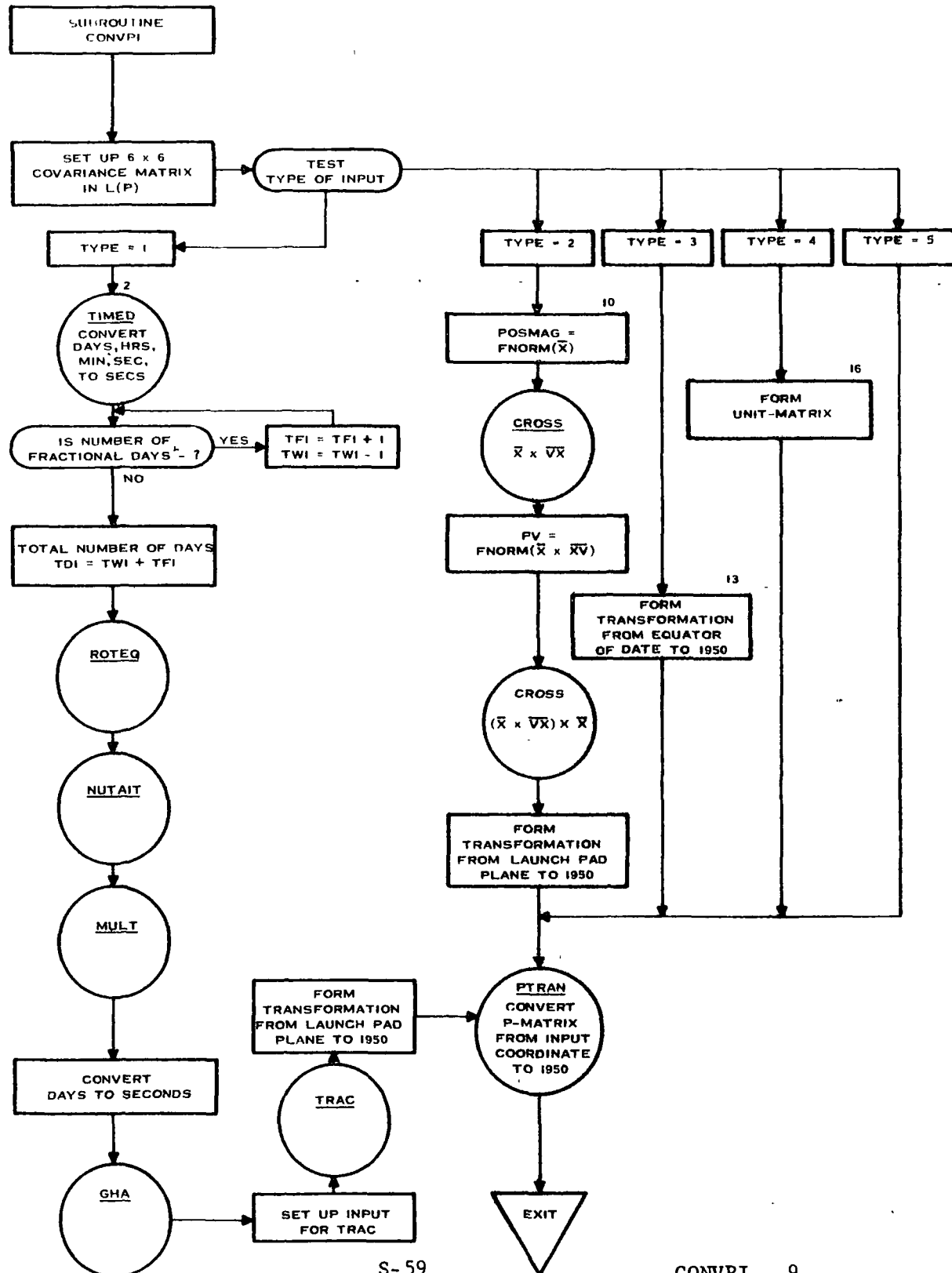
Subroutine PTRAN is called with a 2 in the call list and the operation presented in equation (8) is performed with the 3x3 matrix, (TRANS), defined in equation (14).

INTYPE = 4 Transformation from equator of 1950 to equator of 1950.

The transformation is the unit matrix.

$$\begin{array}{ccccc} \vec{X}_{1950} & = & (\text{I}) & \vec{X}_{1950} & = & (\text{TRANS}) & \vec{X}_{1950} & (16) \\ 3 \times 1 & & 3 \times 3 & & 3 \times 1 \end{array}$$

INTYPE = 5 The subroutine calls PTRAN to perform the operation presented in equation (8) with the transformation matrix, (TRANS), which is in storage from the previous call of CONVPI.



```
* LABEL
* SYMBOL TABLE
SEC2010 SUBROUTINE CONVPI
SUBROUTINE CONVPI(INPUTP,PI,PS)
COMMON T,S,C,IC
DIMENSION T(1360),S(1000),C(1000),IC(1)
1,PI(21),P(6,6),A(3,3),EM(3,3),AN(3,3),U(3)
2,E(3),EN(3),PDUMP(3,3),DUM(3,3),PS(6,6)
3,X(3),VX(3),ORORB(3),ALV(3),RT(3)
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),(IC,ICDUM)
1,(S(70),DTS),(S(72),DR),(S(83),TLTI)
2,(C(138),AN),(S(115),X),(S(118),VX),(C(10),TW)
3,(C(11),TF),(C(129),A),(C(120),EM)
INPUTP DETERMINES TYPE OF INPUT 1.LAUNCH PAD TANGENT PLANE
2.INJECTION TANGENT PLANE 3.EQUATOR DATE 4.EQ1950 5.USE MATRIX
THE REQUIRED ORDER OF INPUT VECTOR OF WHICH PI IS THE COVARIANCE
MATRIX FOR TANGENT PLANE CASES IS FOLLOWING:
1.ALONG VELOCITY,2.NORMAL TO ORBIT,3.ALTITUDE,4,5,6 CORRES.RATES
K=0
DO 1 I=1,6
I=I
DO 1 J=I,6
K=K+1
P(I,J)=PI(K)
P(J,I)=P(I,J)
1 CONTINUE
INPUTP=INPUTP
GO TO (2,10,13,16,8),INPUTP
2 CONTINUE
CALL TIMED(TLTI,TT)
TFI=TF-(TT/86400.)
TWI=TW
3 CONTINUE
IF(TFI)4,5,5
4 CONTINUE
TFI=TFI+1.
TWI=TWI-1.
GO TO 3
5 CONTINUE
TDI=TWI+TFI
CALL ROTEQ(TDI,A)
CALL NUTAIT(TDI,OM,CR,DDC,EM,EPSIL)
CALL MULT(EM,A,AN,N)
FSEC=DTS*TFI
CALL GHA(FSEC,TWI,GH,EM(2,1),OMEGA)
GH=GH*DR
AT=S(80)*DR
ON=S(81)*DR
AL=S(82)
CALL TRAC(ON,AT,AL,GH,U,E,EN,RT,AC,SL,CL,ST,CT)
FAZ=S(84)*DR
```

CONV
CONV
CONV
CONV0030
CONV0040
CONV0050
CONV0060
CONV0070
CONV0080
CONV0090
CONV0100
CONV0110
CONV0120
CONV0130
CONV0140
CONV0150
CONV0160
CONV0170
CONV0180
CONV0190
CONV0200
CONV0210
CONV0220
CONV0230
CONV0240
CONV0250
CONV0260
CONV0270
CONV0280
CONV0290
CONV0300
CONV0310
CONV0320
CONV0330
CONV0340
CONV0350
CONV0360
CONV0370
CONV0380
CONV0390
CONV0400
CONV0410
CONV0420
CONV0430
CONV0440
CONV0450
CONV0460
CONV0470
CONV0480
CONV0490
CONV0500

[illegible]

CONVPI

WDL-TR2184

17 CONTINUE
GO TO 8
15 CONTINUE
RETURN
END

CONV1020
CONV1030
CONV1040
CONV1050
CONV

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CONVPI - 12

Subroutine: CORRTP

Purpose: To perform the filtering or weighting of the observation being made and updating of the state covariance matrix for the inclusion of the observation.

Calling Sequence:

CALL CORRTP (QQ, H, P)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	QQ	1	σ_{MEAS}^2		Measurement variance
I	H	(1,6)	$\frac{\partial \text{MEAS}}{\partial \text{STATE}}$		Measurement partials
I,O	P	(6,6)	$E(\hat{x} \hat{x}^T)$		State covariance matrix

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

124 DEC

Equation Being Solved

The updating of the state covariance matrix for an observation assuming the Schmidt-Kahlman optimum filter is used on the data is the following:

$$P_{NEW} = P_{OLD} - P_o H^T (H P_o H^T + QQ)^{-1} H P_o$$

CORR
CORR
CORR
CORR00
CORR00
CORR00
CORR00
CORR00
CORR00
CORR00
CORR00
CORR00
CORR00
CORR01
CORR01
CORR01
CORR01
CORR01
CORR01
CORR01
CORR01
CORR

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Subroutine: CROSS

Purpose: To find the cross product of two 3-dimensional vectors.

Calling Sequence:

CALL CROSS (A, B, C)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	A	3			First input vector
I	B	3			Second input vector
O	C	3			Result = AXB

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

CROSS

WDL-TR2184

* LABEL
* SYMBOL TABLE
SUBROUTINE CROSS(A,B,C)
DIMENSION A(3),B(3),C(3)
C(1)=A(2)*B(3)-A(3)*B(2)
C(2)=A(3)*B(1)-A(1)*B(3)
C(3)=A(1)*B(2)-A(2)*B(1)
RETURN
END

CROS
CROS
CROS0000
CROS0010
CROS0020
CROS0030
CROS0040
CROS0050
CROS

Subroutine: (CSH)S

Purpose: This is the standard Fortran II card image input subroutine modified to output the card image, accept logical input and output tape numbers from SETN, and call subroutine HOUR to read the clock if desired.

Calling Sequence:

CALL (CSH)S (BUFF)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
0	BUFF	12			Buffer for contents of card read.

Common storages used or required:

None.

Subroutines required:

SETN, HOUR, System read routines.

Functions required:

None.

Approximate number of storages required:

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Subroutine: DE6FN

Identification

RW DE6FN
704 - FORTRAN SAP Language Subroutine
STL

Purpose

This FORTRAN subprogram integrates a set of N simultaneous second-order ordinary differential equations in which first derivatives may or may not appear. It is the FORTRAN version of the standard subroutine RW DE6F.

Restrictions

Same as explained in the write-up for RW DE6F.

Method

A fourth-order Runge-Kutta method (RW DE5F) is used to start the integration and to change the step-size during integration. A Cowell "second-sum" method based on sixth differences is used to continue the integration. While input to this routine is single precision, double precision is used internally to control round-off errors. Truncation error can be controlled by choosing an appropriate step-size, or by using the variable step-size mode of operation. The set-up entry uses the auxiliary subroutine to evaluate the second-order derivatives. The values of the variables and derivatives are consistent at all times. A detailed description of the method used is available in Appendix A.

Usage

- a. Calling LIST for set-up entry (performed prior to initiating the integration).

CALL DE6FN(10,11,T(1),N,V,J,K,A3,A4,A5,A6)

IO is the same as PO of RW DE6F write-up.

- +1 1st derivatives are present in the evaluation of the second derivatives.
- 1 1st derivatives are missing in the evaluation of the second derivatives.

I1 is the same as P1 of RW DE6F write-up.

- +1 Variable step-size mode of operation is used.
- 1 Fixed step-size mode of operation is used.

T is the name of the floating point array which is of dimension $30N+3$ and is reserved by the user. This region should be located in COMMON, since it must be referred to by the main program and by the subroutine V. T(1) need not be set equal to N; however, all other requirements that concern the usage of area T apply. The value of N is not available to the programmer in T(1) and if it is required by the auxiliary subroutine, it should appear in COMMON also.

N is the number of equations (an integer).

V is the name of a FORTRAN subroutine for evaluating the derivatives y_i . This subroutine must be named in the main program by the use of an "F" card.

J equates to B in RW DE6F write-up (an integer).

K equates to R in RW DE6F write-up (an integer).

A3 equates to $\alpha+3$ in RW DE6F write-up (floating point).

A4 equates to $\alpha+4$ in RW DE6F write-up (floating point).

A5 equates to $\alpha+5$ in RW DE6F write-up (floating point).

A6 equates to $\alpha+6$ in RW DE6F write-up (floating point).

For meaning of N, V, J, K, A3, A4, A5, A6 refer to RW DE6F write-up.

Region T contains the following information prior to Set-up Entry.

T(2)	x	value of independent variable
T(3)	h	value of step-size
T(4) thru	y_i thru	values of the independent variables y_i
T(N+3)	y_N	
T(N+4) thru	y_i' thru	values of the first derivatives y_i'
T(2N+3)	y_N'	
T(2N+4) thru	y_i'' thru	values of the second derivatives y_i''
T(3N+3)	y_N''	
T(3N+4) - T(30N+4)		temporary storage

More detailed description of this storage may be found in the RW DE6F write-up.

b. RW DE6FN entry to integrate one step.

CALL DE6FPI (ACCUM)

Upon return ACCUM will have the results which formerly appeared in the accumulator.

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DE6FN-2

- c. RW DE6FN entry for a running start.

CALL DE6FP2

- d. RW DE6FN entry for a change of step-size in Cowell/Runge-Kutta System.

CALL DE6FP3(H)

H is the new value of h which was formerly placed in the accumulator prior to entry.

- e. RW DE6FN entry for a change of step-size for a final integration.

CALL DE6FP4

T(3) must be set to the correct value before the CALL.

- f. RW DE6FN entry to initiate a running change in coordinates and to set a list call to a non-zero value.

CALL DE6FNZ (VALUE)

- g. RW DE6FN entry to change from variable mode to fixed mode.

CALL DE6FNG

- h. RW DE6FN entry to change from fixed mode to variable mode.

CALL DE6FPS

- i. RW DE6FN entry to change the value of h_{\min} .

CALL DE6FMN (VALUE)

VALUE is the new h_{\min} in floating point.

- j. RW DE6FN entry to change the value of h_{\max} .

CALL DE6FMA (VALUE)

VALUE is the new h_{\max} value in floating point.

- k. RW DE6FN entry to change the value of y_{\min} .

CALL DE6FCM (VALUE)

VALUE is the new y_{\min} value in floating point.

- l. RW DE6FN entry to change the value of R after a Cowell integration step.

CALL DE6FCH(NR,R)

NR is the integer value of R.

R is the value in floating point.

Identification

RWDE6F Floating Point Cowell (Second Sum), Runge-Kutta
 Integration of Second-Order Equations
 704 - SAP
 STL

Purpose

To solve a set of N simultaneous second-order ordinary differential equations in which first derivatives may or may not appear.

Restrictions

No internal checks are made for overflow or underflow. The user must provide an auxiliary subroutine which evaluates the second-order derivatives. The initial conditions must be set up prior to the first set up entry.

Method

A fourth-order Runge-Kutta method* (RWDE5F) is used to start the integration and to change the step-size during integration. A Cowell "second-sum" method based on sixth differences is used to continue the integration. While input to this routine is single precision, double precision is used internally to control round-off errors. Truncation error can be controlled by choosing an appropriate step-size, or by using the variable step-size mode of operation. The set-up entry uses the auxiliary subroutine to evaluate the second-order derivatives. The values of the variables and derivatives are consistent at all times. A detailed description of the method used is available in Appendix A of this Subroutine.

Usage

Calling sequence to set up a problem:

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
Y	TSX DE6F,4	Set up entry.
$\alpha+1$	PO T,O,V	Option, addresses of storage and auxiliary subroutines.
$\alpha+2$	PI B,O,R	Option and Parameters
$\alpha+3$	DEC 1E-S	S is the number of significant figures desired.
$\alpha+4$	DEC h _{min}	Minimum step-size. Floating point.

* Scarborough, T.B., Numerical Mathematical Analysis, Third Edition, John Hopkins Press, Baltimore, 1955 (pp. 301-302)

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
$\alpha+5$	DEC h_{\max}	Maximum step-size. Floating point.
$\alpha+6$	DEC y_{\min}	Minimum y_i value allowed for testing. Floating point. (See Appendix A for details of y_{\min} .)

Calling sequence to integrate all variables one step:

α	TSX DE6F+1,4	Integration entry.
$\alpha+1$	Return	Sign of AC will be plus if the integration was Runge-Kutta and minus if Cowell.

The address T is the first of $30N+3$ calls arranged as follows:

T	PZE N,0,0	N is the number of equations. Fixed point.
T+1	x	Value of independent variable. Floating point.
T+2	h	Value of step-size. Floating point.
T+23 thru y_i thru y_N		Values of the dependent variables y_i . Floating point
T+N+2 y_N		
T+N+3 thru y'_i thru y'_N		Values of the first derivatives y'_i . Floating point
T+2.N+2 y'_N		
T+3N+3 thru y''_i thru y''_N		Locations where the user's auxiliary subroutine must store the second derivatives y''_i .
T+3N+3 y''_N		
T+3N+3 thru T+30N+2		27N cells of temporary storage.

T+3N+3 thru T+9N+2 (6N) are used by the Runge-Kutta subroutine (RWDE5F).
T+4N+3 thru T+5N+2 and T+8N+3 thru T+9N+2 contain the least significant parts (except when a change of coordinates is in progress) of y'_i and y_i respectively, and must be preserved throughout the entire integration procedure. The final 21N cells of the T storage are used by the Cowell subroutine and must also be preserved. (See Appendix E of this subroutine for a detailed description of these 27N cells.)

The address V is the entry point of the auxiliary subroutine which evaluates the derivatives y''_i and is entered by the calling sequence:

α	TSX V,4	Index registers need not be saved in V.
$\alpha+1$	Return	Return must be made via a TRA 1,4.

The first B ($\leq N$) equations are tested to determine whether it is necessary to halve or possibly to double the step-size or to proceed with a Cowell integration step.

For a given step-size h , the Cowell integration step is h and the Runge-Kutta integration step is h/R .

Options

- PO - PZE 1st derivatives are present in the evaluation of the second derivatives
 - MZE 1st derivatives are missing in the evaluation of the second derivatives.
 Pl = PZE Variable step-size mode of operation is used.
 = MZE Fixed step-size mode of operation is used.

If $1E-S$, h_{\min} , h_{\max} , and y_{\min} are not specified (0 in first calling sequence), the subroutine will set them to $1E-9$, 0, $1E18$, and 1., respectively.

Special Usage (See Appendices A and B for complete details.)

The following special usages are possible:

1. Running change of coordinates.
2. Running start.
3. Change of step-size by user in the Cowell/Runge-Kutta system.
4. Change of step-size for a final integration or at some prescribed value of x .

Space Required (In addition to T and V).

955 calls of program and constants. (Includes DE5F.)

44 calls of COMMON thru COMMON + 43.

Timing

Set-up time. (V=time for 1 entry to the auxiliary subroutine.)

.012 $[12N + 512]$ ms. + 1V.

To integrate one step:

1. Runge-Kutta (AC=+ after an integration return.)

A. With 1st derivatives.

.012 $[476N + (8N+18)/R + 240]$ ms. + 4V.

B. Without 1st derivatives.

.012 $[383N + (8N + 18)/R + 240]$ ms. + 3V.

Timing (Continued)

2. Cowell (AC= - after an integration return.)

A. With 1st derivatives.

$$.012 \left[2901N + 92B + 194 \right] \quad \text{ms.} + 2V.$$

$$+ .012 \left[2124N + 34 \right] \quad \text{ms. if previous integration was Runge-Kutta.}$$

B. Without 1st derivatives.

$$.012 \quad 2334N + 92B + 194 \quad \text{ms.} + 2V.$$

$$+ .012 \quad 2124N + 38B + 34 \quad \text{ms. if previous integration was Runge-Kutta.}$$

3. Change of Coordinates. (In addition to first part of 2A or 2B.)

$$.012 \left[2286N \right] \quad \text{ms.} + 8V.$$

METHOD

This routine is prepared to solve the following system:

$$\left. \begin{aligned} 1) \quad y_i'' &= f_i(x, y_i, \dots, y_N, y_i', \dots, y_N') \\ y_i(x_0) &= y_{i0}, \quad y_i'(x_0) = y_{i0}' \end{aligned} \right\} \quad i = 1, 2, \dots, N$$

In case none of the f_i involve the first derivatives y_i' , time is saved by indicating this in the set-up. The Runge-Kutta routine RWDE5F is used to start the integration and also to change the step-size h . The user must ask for each integration step, and the routine will follow this sequence:

1. R Runge-Kutta steps of size $\frac{h \text{ start}}{R}$ are taken to obtain y_{i1} , y_{i1}' , y_{i1}'' . This is continued until we reach y_{i6} , y_{i6}' , y_{i6}'' , after a total of $6R$ Runge-Kutta steps. The integer R ($=4$ if unspecified) simply allows Runge-Kutta to operate at a smaller step than the main program.
2. For each of the N equations, that part of the difference table above the diagonal line is constructed in three steps:

$$\begin{aligned}
 3) \quad 'F_{i4} = & \frac{y'_{i3}}{h} - D_0 y''_{i3} - D_1 \Delta^I_{i3} - D_2 \Delta^{II}_{i2} - D_3 \Delta^{III}_{i2} \\
 & - D_4 \Delta^{IV}_{i1} - D_5 \Delta^V_{i1} - D_6 \Delta^{VI}_{i0}
 \end{aligned}$$

The table is then completed down to the diagonal line, by requiring the difference between any entry and the entry above to equal the entry to the right. The constants used in equations (2) - (7) are given in the description of the Livermore Cowell routine.

3. Before going to a Cowell step, the step-size h is tested. The tests are omitted, however, if the user so indicates in the initial calling sequence, in which case h is fixed. Only the first B equations are used to test, where $1 \leq B \leq N$ and $B = N$ if unspecified. We determine--

$$V = \frac{\max_{1 \leq i \leq B}}{\left| \frac{\Delta^V_{i1}}{\max(y_{i6}, y_{\min})} \right|}. \quad \text{If } V \geq \frac{10^{3-S}}{h^2}, \text{ then the}$$

ratio of 5th difference to function is too large -- if S decimal places are to be retained at that step. Therefore, h is reduced to $h/2$ and Runge-Kutta re-entered for another sequence of $6R$ steps. These begin with the latest calculated values (y_{i6}, y'_{i6}) and no ground is retraced. The constant y_{\min} ($=1$ if unspecified) prevents division by y near a zero; for example, in sine calculation $y_{\min}=.1$ avoids difficulty near 180° . The integer S , taken as 9 if unspecified, allows a large h if chosen smaller, say $S = 7$.

$$\text{If } \frac{10^{-1-S}}{h^2} < V < \frac{10^{3-S}}{h^2}, \text{ we proceed to a Cowell step.}$$

If $V \leq \frac{10^{-1-S}}{h^2}$, we may be able to double h . We test further

to see that

$$W = \frac{\max_{1 \leq i \leq B}}{\left| \frac{\Delta_{i0}^{VI}}{\max(y_{i6}, y_{\min})} \right|} \leq \frac{10^{-1-S}}{h^2},$$

and if so, we re-enter Runge-Kutta after replacing h by $2h$, since the step-size h has led to needlessly small difference to function ratios. Of course, h is not halved or doubled if this would violate h_{\min} or h_{\max} , which are 0 and 10^{18} if unspecified.

4. The Cowell integration begins with predictions:

$$4) \quad y_{i7} = h^{2^*} ({}^*F_{i8} + N_0 y''_{i6} + N_1 \Delta_{i5}^I + \dots + N_6 \Delta_{i0}^{VI})$$

$$5) \quad y'_{i7} = h ({}^*F_{i7} + \dot{N}_0 y''_{i6} + \dot{N}_1 \Delta_{i5}^I + \dots + \dot{N}_6 \Delta_{i0}^{VI})$$

These use the row of the difference table above the diagonal line; only this row is needed for a Cowell step and is kept up to date as the integration proceeds. (We mention that the above prediction for y'_{i7} is omitted in the missing first derivative option.) Now from y_{i7} and y'_{i7} , we obtain y''_{i7} and then complete the row of differences out to Δ_{i1}^{VI} under the diagonal line in the table. With this row, we calculate final corrected values --

$$6) \quad y_{i7} = h^2 ({}^*F_{i8} + B_0 y''_{i7} + \dots + B_6 \Delta_{i1}^{VI})$$

$$7) \quad y'_{i7} = h ({}^*F_{i7} + \dot{B}_0 y''_{i7} + \dots + \dot{B}_6 \Delta_{i1}^{VI})$$

From these we get corrected values for y''_{i7} , and recalculate the entire row under the diagonal line. This completes the integration step. Using the new row of differences, the next step begins by testing the step-size (i.e., at 3.).

Further Properties of the Program

In some problems, information about the first derivative (velocity) may be less reliable than information about the function (position). The user may then choose a "running change of coordinates" or a "running start;" these depend on the fact that with 8 consecutive values of the y_i (and the y'_i in case first derivatives are present in the f_i) the Cowell part of the program can be self-starting. The mathematics is simple: step No. 1 is omitted, and No. 2 modified to calculate " F_{i4} " and " F_{i5} " from Eq. (2) (instead of " F_{i4} " and " F_{i4} "). The difference table may again be completed, and Cowell integration begins. The user, having tested the AC to establish that the previous step was a Cowell step, begins a running change of coordinates by setting cell DE6F + 500 to non-zero. He then sets up a counter and begins immediately to store 8 consecutive values of the y_i starting at $T+3+11N$ (and y'_i starting at $T+3+3N$, if they appear in the f_i). After changing the coordinates the 8th time, the user may change the second derivative evaluation routines; if x and h are to be in new units this should also be done. When another step is asked for, the routine will form a difference table in the new coordinates and proceed to a Cowell step.

The mechanics of a running start are similar; after going through the set-up routine, the user loads his values of y_{i0} through y_{i7} (and the y'_i if needed in the f_i) into the same locations as above and makes the required transfer.

There may also be occasions on which the user will wish to modify h himself; e.g., if he wishes to produce the numerical solution at some prescribed value of x , or if he wishes to approach a running change of coordinates at a step-size smaller than that being used by the routine.

The technique of modifying h is described in Appendix B.

APPENDIX B

USAGE AND CODING INFORMATION

There are essentially two entries to the subroutine. The first entry must be made once at the beginning to set up the addresses, options, parameters, etc., of the routine for integration of N simultaneous second-order, ordinary differential equations, in which first derivatives may or may not appear. The first entry utilizes the auxiliary subroutine to evaluate the second-order derivatives at the initial conditions. Thus, the initial conditions must be set up prior to the first entry. The second entry may be used any number of times after the first to integrate all y_i from x to $x+h$ by a Cowell step; or x to $x+h/R$ by a Runge-Kutta step.

The first entry has the following calling sequence:

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
α	TSX DE6F,4	Set-up entry.
$\alpha+1$	PO T,O,V	Option, addresses of storage and auxiliary subroutine.
$\alpha+2$	Pl B,O,R	Option and parameters.
$\alpha+3$	DEC lE-S	S is the number of significant figures desired.
$\alpha+4$	DEC h_{\min}	Minimum step-size. Floating point.
$\alpha+5$	DEC h_{\max}	Maximum step-size. Floating point.
$\alpha+6$	DEC y_{\min}	Minimum y_i value allowed for testing. Floating point.
$\alpha+7$	Return	

($\alpha+1$): T is the address of the first word of a block of $30N+3$ cells of temporary storage arranged as follows:

<u>Loc.</u>	<u>Contents</u>	<u>Comments</u>
T	PZE N,0,0	N is the number of equations. Fixed point.
T+1	x	Value of independent variable. Floating point.
T+2	h	Value of step-size. Floating point.
T+3 thru T+N+2	y_i thru y_N }	Values of the dependent variables y_i . Floating point.
T+N+3 thru T+2N+2	y'_i thru y'_N }	Values of the first derivatives y'_i . Floating point.
T+2N+3 thru T+3N+2	y''_i thru y''_N }	Locations where the user's auxiliary subroutine must store the second derivatives y''_i . Floating point.
T+3N+3 thru T+30N+2		27N cells of temporary storage.

The next 27N storages of T are temporary storages. The Runge-Kutta subroutine uses the first 6N cells (T+3N+2 thru T+9N+3) and the Cowell routine uses the final 21N cells (T+9N+3 thru T+30N+2). However, if a change of coordinates (see Special Usage) is made, the Cowell routine will also use the first 6N cells. The attached T Storage Chart shows the set-up of the entire T region. The N cells starting at T+5N+3 and the N cells starting at T+6N+3 are used by the Runge-Kutta subroutine to compute $\Delta'y_{iN}$ and Δy_{iN} . However, $\Delta'y_{iN}$ and Δy_{iN} are destroyed before final exit, and these cells contain intermediate values of no significance to the user. The left side of the chart shows the storage for the normal case where 6R Runge-Kutta steps are taken (using the first 9N cells of T for each integration) before an attempt is made to proceed to a Cowell step. At the beginning of each set of R steps, the Cowell subroutine saves the values of the second derivatives (7 sets starting at T+11N+3). In addition, the values of y_{i3} and y'_{i3} are saved, starting at T+9N+3 and T+10N+3 respectively, for use in the central difference equations where F_{i4} and F'_{i4} are calculated. Care must be exercised in using certain values in the temporary region.

For instance, after a Runge-Kutta integration step, the most significant values of y_i and y'_i , starting at $T+7N+3$ and $T+3N+3$ respectively, will be the values of the previous integration; while the least significant values of y_i and y'_i , starting at $T+8N+3$ and $T+4N+3$, respectively, will be the values of the present integration. The Cowell routine also saves the least significant values of y_i and y'_i (unless a change of coordinates is in progress) in these same storages at the end of each integration. The $11N$ storages starting at $T+19N+3$ contain the right half of the N difference tables, an example of which is shown in Appendix A. The right side of the chart shows other values which are stored in the T region during a change of coordinates and will be explained later under Special Usage. Even though only one symbol is given (y'_{10} , etc.), it should be understood that N values are stored as in the left side of the chart. Thus, y'_{10} signifies $y'_{10}, y'_{20}, y'_{30}, \dots, y'_{N0}$.

The address V is the entry point of an auxiliary subroutine which the user must provide to evaluate the second derivatives y''_i . This subroutine must store y''_i in $T+2N+3$ through $T+3N+2$ as shown above. The subroutine is entered by the calling sequence:

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
α	TSX V,4	Index registers need not be saved.
$\alpha+1$	Return	Return via a TRA 1,4.

The derivatives y''_i are evaluated during the set-up and at the end of each integration step. Thus, the values of the variables and the derivatives are consistent at all times. Extra precision is recommended for the evaluation of the second derivatives y''_i .

PO should be set to PZE if the first derivatives are present in the evaluation of the second derivatives. If first derivatives are not present, PO should be set to MZE.

($\alpha+2$): P1 should be set to PZE if a variable step-size is wanted. For a fixed step-size; P1 should be set to MZE. The former allows doubling and halving while the latter restricts the routine to a fixed r . The user may change the mode of operation externally at any time by setting cell DE6F+501 to plus for a variable step-size and minus for a fixed step-size.

Only the first B ($1 \leq B \leq N$) equations are tested to determine doubling or halving of h . Thus, the user should arrange the N equations in descending order of importance, and specify B accordingly. If $B = 0$ in the calling sequence, it will be set to N.

R is the ratio of the Cowell step-size to the Runge-Kutta step-size. Thus, smaller integration steps can be taken in the Runge-Kutta subroutine by setting R greater than 1. If $R = 0$ in the calling sequence, it will be set to 4. R is saved in the decrement of cell DE6F+516 and in floating point in cell DE6F+517. After any Cowell integration step (AC = -), the user should change R by changing both of these cells.

($\alpha+3$): $1E-S$ is a floating point number where S is the number of significant figures of accuracy desired at each step. The user should experiment with S to fit his own particular problem. The 1 of $1E-S$ may also be varied from 1 to 9 ($1E-S$ thru $9E-S$) for a final degree of control over the accuracy testing. If $1E-S=0$ in the calling sequence, it will be set to $1E-9$.

($\alpha+4$): h_{\min} is a floating point number giving a lower bound for h . h_{\min} is saved in cell DE6F+509 and can be changed at any time.

($\alpha+5$): h_{\max} is a floating point number giving an upper bound for h . If $h_{\max}=0$ in the calling sequence, the upper bound will be set to $1E18$. h_{\max} is saved in cell DE6F+510 and can be changed at any time.

($\alpha+6$): y_{\min} is a positive floating point number which is used in testing the step-size. If $y_{\min}=0$ in the calling sequence, it will be set to 1. y_{\min} is saved in cell DE6F+511 and can be changed at any time.

If the fixed step-size mode of operation is selected ($P1=MZE$), then B , $1E-S$, h_{\min} , h_{\max} , and y_{\min} are all ignored by the subroutine. (If $P1=MZE$, set $B = 1$ for maximum efficiency.)

The integration entry has the following calling sequence:

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
α	TSX DE6F+1,4	Integrates all variables one step.
$\alpha+1$	Return	

Upon return from the integration entry, the accumulator will be plus if the integration was a Runge-Kutta step and minus if the integration was a Cowell step. Ordinarily, x will have been advanced to $x + h/R$ for a Runge-Kutta step and $x + h$ for a Cowell step. However, in the variable h mode, it is possible that the value of h in $T+2$ prior to the integration entry has been changed to $h/2$ or $2h$. In this case, the integration step will be a Runge-Kutta step, and the value of x will be either $x + h/2R$ or $x + 2h/R$. All values of y_i , y'_i , and y''_i will be consistent with the new value of x . The user must never change the value of the step-size h except as described under Special Usage.

Special Usage (See Appendix A. Further Properties of the Program.)

1. Running Change of Coordinates. (Normal Entries.)

After any Cowell integration step (AC= -), the user may initialize the beginning of a change of coordinates by setting cell DE6F+500 to non-zero. Starting with the present values, he begins to save eight consecutive sets of y_i starting at $T+11N+3$ (and y'_i starting at $T+3N+3$ if they appear in the y''_i). He continues to use the integration entry above. The routine will

detect the non-zero value stored in cell DE6F+500 and will begin a count-down in cell DE6F+502 from 8 (-1) 0. The next seven integrations will be Cowell steps and all testing will be discontinued during this period. After the eighth set of y_i (y_{i7}), and y'_i (y'_{i7}) if necessary, have been stored (DE6F+502 will have a fixed point 1 in the address), the user may change the second derivative evaluation routine V and the units of x and h . The units of the eight sets of y_i and y'_i may be changed while storing each set, or after all eight sets have been stored. When another integration step is asked for, the routine will perform the change of coordinates and proceed to a Cowell integration step. Cell DE6F+500 will be restored to zero, and an 8 will be restored to the address of cell DE6F+502. Thus, the routine will be ready for another change of coordinates and will operate under standard conditions.

2. Running Start. (Special Entry.)

A running start is similar to a running change of coordinates except that the user must supply all eight sets of y_i (and y'_i if necessary) at one time. The following sequence of operations must be followed:

- A. Set up the initial conditions in the T storage. Only N , x , and h are needed, although the eight sets of y_i (but not y'_i) can also be stored at this time. x must correspond to y_{i7} and h must be the interval at which the y_i have been obtained. Thus, $x = x_0 + 7h$ where x_0 corresponds to y_0 (and y'_0).
- B. Use the first entry calling sequence to set up all parameters and options. The V subroutine will be used but will have no effect on the problem. Also, cells $T+4N+3$ thru $T+5N+2$ and $T+8N+3$ thru $T+9N+2$ will be set to zero. Thus, the eight sets of y'_i must be stored after the setup entry.
- c. Store eight consecutive sets (equal intervals) of y_i starting at cell $T+11N+3$ (and eight consecutive sets of y'_i starting at cell $T+3N+3$, if needed).

D. Execute the following calling sequence one time:

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
α	TSX DE6F+16,4	Enter only once.
$\alpha+1$	Return	Integrates 1 step.

E. Continue with the regular integration entry (TSX DE6F+1,4) to integrate further. Step D integrates all variables one Cowell step, and $x(x_0 + 7h)$ is advanced to $x + h(x_0 + 8h)$. From this point, the routine will operate under normal conditions.

3. Change of Step-Size in the Cowell/Runge-Kutta System. (Special Entry.)

During the integration procedure, the user may wish to output for a specific value of x without interrupting the Cowell/Runge-Kutta integration procedure. Or, he may wish to change the value of the step size h prior to a running change of coordinates. He can do this after any integration entry with the following procedure:

<u>Loc.</u>	<u>Instruction</u>	<u>Comments</u>
α	TSX DE6F+22,4	Changes h and starts new series of 6R Runge-Kutta steps.
$\alpha+1$	Return	

Thus, the integration step will be h/R . Continue with the regular integration entry (TSX DE6F+1,4) to integrate further.

If the above procedure is being used to reduce the step-size prior to a change of coordinates, the user must prevent the routine from doubling again until after the change of coordinates. Doubling can be prevented either by storing zero in cell DE6F+510 (h_{\max}), or by setting cell DE6F+501 (fixed step size) negative prior to the above entry. After the change of coordinates, the user may restore the above cells.

4. Change of Step Size for a Final Integration. (Special Entry.)

This is simply a direct transfer to the Runge-Kutta integration subroutine and should be used to end exactly at a specific value of x .

After changing the value of h in T+2,

<u>Loc.</u>	<u>Instruction</u>	<u>Comment</u>
α	TSX DE6F+588,4	Integrates one step with the Runge-Kutta subroutine.
$\alpha+1$	Return	

The integration step will be the value of h in T+2. This procedure could be used in the middle of the integration procedure if 3. above (TSX DE6F+22,4) is used immediately afterwards to restart in the Cowell/Runge-Kutta system.

In addition to the user's auxiliary subroutine and the 30N+3 cells for the T storage, the storage requirements are 955 words for RWDE6F plus 44 words of COMMON.

The value of the independent variable x is accumulated in double precision when incremented by h . The least significant part of x is saved in cell DE6F+718.

APPENDIX B - T STORAGE CHART

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* FAP
  TTL DE6FN COWELL INTEGRATION ROUTINE CORRECTED 6/63
  LBL DE6FN
  COUNT 1100
  ENTRY DE6FN
  ENTRY DE6FP1
  ENTRY DE6FP2
  ENTRY DE6FP3
  ENTRY DE6FNZ
  ENTRY DE6FPS
  ENTRY DE6FNG
  ENTRY DE6FCH
  ENTRY DE6FCM
  ENTRY DE6FP4
  ENTRY DE6FMN
  ENTRY DE6FMA
  PZE 0
  PZE 0
  PZE 0
DE6FN SXD DE6FN-1,1      SAVE 1R
      SXD DE6FN-2,2
      SXD DE6FN-3,4
      CLA 5,4
      STA DUX1
      CLA 6,4
      STA BCOM          LOC B
      CLA 7,4
      STA RCOM          LOC R
BCOM  CLA *
      STA CALL+1
      ARS 18
      STO CELM1
RCOM  CLA *
      ADD CELM1
      STO CALL+2        2ND WORD
      CLA 8,4
      STA **+1
      CLA *
      STO CALL+3        3RD WORD
      CLA 9,4
      STA **+1
      CLA *
      STO CALL+4        4TH WORD
      CLA 10,4
      STA **+1
      CLA *
      STO CALL+5        5TH WORD
      CLA 11,4
      STA **+1
      CLA *
      STO CALL+6        6TH WORD

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DE6FN
DE6FN0000
DE6FN0010
DE6FN0020
DE6FN0030
DE6FN0040
DE6FN0050
DE6FN0060
DE6FN0070
DE6FN0080
DE6FN0090
DE6FN0100
DE6FN0110
DE6FN0120
DE6FN0130
DE6FN0140
DE6FN0150
DE6FN0160
DE6FN0170
DE6FN0180
DE6FN0190
DE6FN0200
DE6FN0210
DE6FN0220
DE6FN0230
DE6FN0240
DE6FN0250
DE6FN0260
DE6FN0270
DE6FN0280
DE6FN0290
DE6FN0300
DE6FN0310
DE6FN0320
DE6FN0330
DE6FN0340
DE6FN0350
DE6FN0360
DE6FN0370
DE6FN0380
DE6FN0390
DE6FN0400
DE6FN0410
DE6FN0420
DE6FN0430
DE6FN0440
DE6FN0450
DE6FN0460
DE6FN0470
DE6FN0480
DE6FN0490

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CLA 2,4	SET SIGN	DE6FN050
STA ++1		DE6FN051
CLA *		DE6FN052
TPL ++3	2ND WORD	DE6FN053
CLS CALL+2		DE6FN054
STO CALL+2		DE6FN055
CLA 4,4	LOC ENDT	DE6FN056
STA NTOTA		DE6FN057
CLA 3,4		DE6FN058
STA REVER+3		DE6FN059
STA REVER+5		DE6FN060
STA NTOT		DE6FN061
STA COMN		DE6FN062
STA COMCEL		DE6FN063
STA SVTD		DE6FN064
NTOTA CLA *		DE6FN065
ARS 18		DE6FN066
NTOT STO *		DE6FN067
COMCEL LDQ *	FIND TOP T	DE6FN068
MPY TRTY		DE6FN069
STQ CELM1		DE6FN070
CLA SVTD		DE6FN071
SUB CELM1		DE6FN072
SUB TWO		DE6FN073
ADM CALL+1		DE6FN074
STA START	SAP T	DE6FN075
STO CALL+1		DE6FN076
CLA 1,4		DE6FN077
STA ++1		DE6FN078
CLA *		DE6FN079
TPL ++3	SET SIGN PO	DE6FN080
CLS CALL+1		DE6FN081
STO CALL+1		DE6FN082
COMN LDQ *	COMPUTE	DE6FN083
MPY FIFTN	MID POINT	DE6FN084
STQ CELM1		DE6FN085
CLA CELM1		DE6FN086
ADD ONE		DE6FN087
STO HN		DE6FN088
CLA START		DE6FN089
ADD HN		DE6FN090
STA REVER+2		DE6FN091
STA REVER+4		DE6FN092
TSX REVER,4		DE6FN093
CALL TSX DE6F,4	ENTER	DE6FN094
PZE , , DUX		DE6FN095
PZE *		DE6FN096
PZE *		DE6FN097
PZE *		DE6FN098
PZE *		DE6FN099
PZE *		DE6FN100

TSX REVER, 4
 LXD DE6FN-1, 1
 LXD DE6FN-2, 2
 LXD DE6FN-3, 4
 TRA 12, 4
 REVER LXA HN, 1
 LXD ZERO, 2
 IN LDQ *, 1
 CLA *, 2
 STO *, 1
 STO *, 2
 TXI **1, 2, 1
 TIX IN, 1, 1
 TRA 1, 4
 DE6FP1 SXD DE6FN-1, 1
 SXD DE6FN-2, 2
 SXD DE6FN-3, 4
 TSX REVER, 4
 TSX DE6F+1, 4
 STO CELM1
 TSX REVER, 4
 LXD DE6FN-1, 1
 LXD DE6FN-2, 2
 LXD DE6FN-3, 4
 CLA 1, 4
 STA **2
 CLA CELM1
 STO *
 TRA 2, 4
 DE6FP2 SXD DE6FN-1, 1
 SXD DE6FN-2, 2
 SXD DE6FN-3, 4
 TSX REVER, 4
 TSX DE6F+16, 4
 TSX REVER, 4
 LXD DE6FN-1, 1
 LXD DE6FN-2, 2
 LXD DE6FN-3, 4
 TRA 1, 4
 DE6FP3 SXD DE6FN-1, 1
 SXD DE6FN-2, 2
 SXD DE6FN-3, 4
 TSX REVER, 4
 LXD DE6FN-3, 4
 CLA 1, 4
 STA **1
 CLA *
 TSX DE6F+22, 4
 TSX REVER, 4
 LXD DE6FN-1, 1
 LXD DE6FN-2, 2

REVERSE T BLOCK

DE6FN1010
 DE6FN1020
 DE6FN1030
 DE6FN1040
 DE6FN1050
 DE6FN1060
 DE6FN1070
 DE6FN1080
 DE6FN1090
 DE6FN1100
 DE6FN1110
 DE6FN1120
 DE6FN1130
 DE6FN1140
 DE6FN1150
 DE6FN1160
 DE6FN1170
 DE6FN1180
 DE6FN1190
 DE6FN1200
 DE6FN1210
 DE6FN1220
 DE6FN1230
 DE6FN1240
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 DE6FN1260
 DE6FN1270
 DE6FN1280
 DE6FN1290
 DE6FN1300
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 DE6FN1350
 DE6FN1360
 DE6FN1370
 DE6FN1380
 DE6FN1390
 DE6FN1400
 DE6FN1410
 DE6FN1420
 DE6FN1430
 DE6FN1440
 DE6FN1450
 DE6FN1460
 DE6FN1470
 DE6FN1480
 DE6FN1490
 DE6FN1500
 DE6FN1510

LXD DE6FN-3,4

TRA 2,4

DE6FP4 SXD DE6FN-1,1

SXD DE6FN-2,2

SXD DE6FN-3,4

TSX REVER,4

TSX DE6F+588,4

TSX REVER,4

LXD DE6FN-1,1

LXD DE6FN-2,2

LXD DE6FN-3,4

TRA 1,4

DE6FNZ CLA 1,4

STA **1

CLA *

STO DE6F+500

TRA 2,4

DE6FPS CLA DE6F+501

SSP

STO DE6F+501

TRA 1,4

DE6FNG CLA DE6F+501

SSM

STO DE6F+501

TRA 1,4

DE6FMN CLA 1,4

STA **1

CLA *

STO DE6F+509

TRA 2,4

DE6FMA CLA 1,4

STA **1

CLA *

STO DE6F+510

TRA 2,4

DUX SXD DUX2,4

TSX REVER,4

DUX1 TSX 0,4

TSX REVER,4

LXD DUX2,4

TRA 1,4

DUX2 PZE

DE6FCM CLA 1,4

STA **1

CLA *

STO DE6F+511

TRA 2,4

DE6FCH CLA 1,4

STA LINKA

CLA 2,4

STA LINKB

DE6FN150

DE6FN150

DE6FN150

DE6FN150

DE6FN150

DE6FN150

DE6FN150

DE6FN150

DE6FN150

DE6FN160

DE6FN160

DE6FN160

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DE6FN190

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DE6FN190

DE6FN190

DE6FN190

DE6FN190

DE6FN200

DE6FN200

DE6FN200

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LINKA CLA *
      STO DE6F+516
LINKB CLA *
      STO DE6F+517
      TRA 3,4
ZERO PZE 0
ONE DEC 1
TWO DEC 2
FIFTH DEC 15
HN PZE 0
SVTD PZE 0
COMMON BSS 44
DE6F TRA DE6F+0799      COWELL METHOD INTEGRATION SUB (TR SETUP)
      SXD DE6F+0504,1      2ND ENTRY, BEGIN
      SXD DE6F+0505,2      INTEGRATION
      SXD DE6F+0506,4
      CLA DE6F+0500      TEST SWITCH FOR COORD. CHANGE
      TZE DE6F+0011      0=NORMAL CASE
      CLA DE6F+0502      8(-1)0
      SUB DE6F+0531      1
      STO DE6F+0502
      TNZ DE6F+0011      CONTINUE IF NOT ZERO
      TRA DE6F+0091      TR FOR COORD. CHANGE
      CLA DE6F+0503      TEST R.K. OR COWELL
      TMI DE6F+0185      --COWELL
      CLA DE6F+0709      TEST 1ST TIME FOR R.K.==+
      TMI DE6F+0043      =2N=3RD, ..., RTH R.K. INTEGR.
      TRA DE6F+0030      TR TO BEGIN RUNGE KUTTA SERIES (R)
      SXD DE6F+0504,1      PROGRAMMER MAY ENTER HERE FOR
      SXD DE6F+0505,2      SPECIAL COORD. CHANGE, 8 SETS
      SXD DE6F+0506,4      OF Y,S MUST BE IN T+11N+3
      STZ DE6F+0502      AND T MUST BE AT 8TH Y.
      SXD DE6F+0500,4      8 SETS OF Y PRIME MUST BE
      TRA DE6F+0091      AT T+3N+3 IF F(X,Y,Y PRIME) USED.
      SXD DE6F+0504,1      PROGRAMMER MAY ENTER HERE WITH H IN AC
      SXD DE6F+0505,2      AND START NEW RUNGE KUTTA SERIES
      SXD DE6F+0506,4      H/R WILL BE INTEGRATION STEP.
      STO COMMON+000      NEW H
      CLA DE6F+0500      CANNOT CHANGE H IF COORD.
      TNZ DE6F+0006      CHANGE IS IN PROGRESS
      LDQ COMMON+000      NEW H
      TSX DE6F+0077,2      CHANGE VMIN, VMAX, WMAX FOR H2
      CLA DE6F+0519      H/R=R.K. H FOR EACH STEP
      FDP DE6F+0517      R=TOTAL R.K. STEPS
      STQ 0      (T+2)
      LDQ DE6F+0519      DELTA (T) = H
      FMP DE6F+0519
      STO DE6F+0520      DELTA (T) SQUARED
      STZ DE6F+0518      SET K=0, (K=0(1)6)
      SSM
      STO DE6F+0709      FIX SWITCH FOR 2ND, ETC ENTRIES

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DE6FN2030
DE6FN2040
DE6FN2050
DE6FN2060
DE6FN2070
DE6FN2080
DE6FN2090
DE6FN2100
DE6FN2110
DE6FN2140
DE6FN2160
DE6FN2170
DE6FN2180
DE6FN2190
DE6FN2200
DE6FN2210
DE6FN2220
DE6FN2230
DE6FN2240
DE6FN2250
DE6FN2260
DE6FN2270
DE6FN2280
DE6FN2290
DE6FN2300
DE6FN2310
DE6FN2320
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DE6FN2390
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DE6FN2420
DE6FN2430
DE6FN2440
DE6FN2450
DE6FN2460
DE6FN2470
DE6FN2480
DE6FN2490
DE6FN2500
DE6FN2510
DE6FN2520
DE6FN2530
DE6FN2540
DE6FN2550
DE6FN2560

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LXA DE6F+0527,1      7N(=N)N TO SAVE 2ND DERIV.)
SXD DE6F+0527,1      7N(=N)N
CLA DE6F+0516         R=R,K. STEPS PER DELTA(T)
STO DE6F+0515         R IN DECR.
LXD DE6F+0515,1      R(=1)1
CLA DE6F+0516         R=TOTAL R,K. STEPS PER D(T)
SUB DE6F+0515         R(I)=CURRENT RI=R(=1)1 IN DECR.
TNZ DE6F+0054         TR IF NOT 1ST R
LXA DE6F+0710,4      N
LXD DE6F+0527,2      7N(=N)N
CLA 0,4              T+3N+3(2ND DERIV.)
STO 0,2              T+11N+3+(7N), (7N 2ND DERIVS)
TXI DE6F+0052,2,-1
TIX DE6F+0049,4,1
SXD DE6F+0527,2      7N(=N)N
LXA DE6F+0518,2
TXH DE6F+0122,2,5    IF K=6, TR TO COWELL
TSX DE6F+0588,4      TR TO RUNGE KUTTA INTEGRATION
TIX DE6F+0070,1,1    REDUCE R TIL R=RN
LXD DE6F+0516,1      R=RN (RESTORE R FOR NEXT CYCLE)
CLA DE6F+0518         K=0(1)6
ADD DE6F+0531         1-
STO DE6F+0518
SUB DE6F+0533         3
TNZ DE6F+0070         SAVE Y(3) AND Y(3) PRIME IF 0
LXA DE6F+0710,2      N
CLA 0,2              T+N+3=Y(I)=DEPENDENT VAR. (YI)
STO 0,2              T+10N+3=Y(3)
CLA 0,2              T+2N+3=Y(I) PRIME=1ST DERIV.
STO 0,2              T+11N+3=Y(3)PRIME
TIX DE6F+0065,2,1
SXD DE6F+0515,1
SSP
STO DE6F+0503         SAVE R
                      * = RUNGE KUTTA
                      * = COWELL METHOD
LXD DE6F+0506,4
LXD DE6F+0504,1      1 R,K. STEP COMPLETED
LXD DE6F+0505,2
TRA 1,4              RETURN TO PROGRAMMER
CLA DE6F+0519         OLD H (SUB. FOR NEW VMIN, VMAX, WMAX)
STO COMMON+001        H1=OLD H (SAVE FOR CHANGE OF HMAX)
CLA DE6F+0520         OLD H SQ.=H1 SQ.
STO COMMON+000        H1 SQ.
STQ DE6F+0519         NEW H=H2
FMP DE6F+0519
STO DE6F+0520         NEW H SQ.=H2 SQ.
LXA DE6F+0533,5      3 IN IR1, IR4
CLA COMMON+000        H1 SQ.
FDP DE6F+0520         H2 SQ.
FMP DE6F+0515,4      CHANGE VMIN, VMAX, VMAX
STO DE6F+0515,4      (V/H1 SQ.)X(H1 SQ.)/(H2 SQ.)
TIX DE6F+0085,4,1

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TRA 1,2
LDQ 0
FMP DE6F+0544
FAD 0
STO 0
LXA DE6F+0528,1
SXD DE6F+0528,1
CLA 0
FAD 0
STO 0
LXA DE6F+0710,2
CLA 0,1
STO 0,2
CLA 0,1
STO 0,2
TXI DE6F+0106,1,-1
TIX DE6F+0101,2,1
TSX 0,4
LXD DE6F+0528,1
LXA DE6F+0710,2
CLA 0,2
STO 0,1
TXI DE6F+0113,1,-1
TIX DE6F+0110,2,1
TXH DE6F+0096,1,0
LDQ 0
TSX DE6F+0077,2
CLA DE6F+0519
FDP COMMON+001
FMP DE6F+0512,1
STO DE6F+0512,1
TIX DE6F+0117,1,1
STZ DE6F+0521
STZ DE6F+0522
LXA DE6F+0529,4
SXD DE6F+0529,4
LXA DE6F+0710,4
LXA DE6F+0527,2
SXD DE6F+0527,2
CLA 0,4
STO DE6F+0711
CLA DE6F+0502
TNZ DE6F+0316
TSX DE6F+0380,2
PZE 0
CLA DE6F+0520
TSX DE6F+0344,2
PZE DE6F+0552,0,COMMON+21
CLA 0,4
TSX DE6F+0482,2
TSX DE6F+0373,2

T+2=H (COORD. CHANGE BEGINS)
-8.
T+1=T
T+1
8N
8N(-N)0
T+1=(T)
T+2=H
T+1=(T+H)
N
T+11N+3+(8N)=(Y0,Y1,...,Y7)
T+N+3
T+3N+3*(8N)=1ST DERIV.
T+2N+3(IF SAVED)
MOVE DEPENDENT VAR. TO T+3 THRU T+N+2
V (FORM2ND DERIV.)
8N
N
T+3N+3 (2ND DERIV.)
T+3N+3*(8N)
STORE 2ND DERIV. (8 SETS)
LOOP FOR 8 SETS OF Y
(T+2)=H=DELTA(T)
CHANGE VMIN, VMAX, WMAX
H2=NEW H
H1=OLD H
CHANGE UNITS OF HMIN,HMAX,
AND XMIN
CLEAR W, W=MAX (DELTA VII)/Y
CLEAR V, V=MAX (DELTA VI)/Y
11N
N
7N
7N(-1)6N
T+N+3=Y
SEE V AND W CALC.
NORMALLY=8 (NO CHANGE IN COORD.)
O=COORD. CHANGE
FORM DIFF.
T+3N+3*(7N)
H.SQ.
FORM SUM OF PRODUCTS
C(I)XDELTAS
T+15N+3(Y3,COORD. CHANGE)
ADD Y3 TO C+3,C+4
F4(II) IN A1 AND A2

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DE6FN3080
DE6FN3090
DE6FN3100
DE6FN3110
DE6FN3120
DE6FN3130
DE6FN3140
DE6FN3150
DE6FN3160
DE6FN3170
DE6FN3180
DE6FN3190
DE6FN3200
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DE6FN3570
DE6FN3580

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CLS DE6F+0507
STO DE6F+0714      -F4(II)
CLS DE6F+0508
STO DE6F+0715
TSX DE6F+0380,2    FORM DIFF.
PZE 0              T+4N+3+(7N)
TSX DE6F+0345,2    H SQ. STILL IN COM+2
PZE DE6F+0552,0,COMMON+21
CLA 0,4            T+16N+3,(Y4, COORD. CHANGE)
TSX DE6F+0482,2    ADD Y4 TO C+3,C+4
TSX DE6F+0373,2    F5(II) IN A1 AND A2
CLA DE6F+0714
STO COMMON+003     -F4(II)
CLA DE6F+0715
STO COMMON+004
TSX DE6F+0491,2    F4(I)=F5(II)-F4(II)
STO COMMON+003     -F4(I)
STQ COMMON+004
CLA COMMON+008     Y4 (2ND DERIV.)
TSX DE6F+0482,2    F5(I) IN COMMON+3,4
LXA DE6F+0533,1    3
TSX DE6F+0491,2    F5(II) OR F6(II) IF COORD. CHG.
STO DE6F+0507
STQ DE6F+0508
CLA COMMON+012,1   Y(4),Y(5),Y(6) 2ND DERIV.
TSX DE6F+0482,2    OR Y(5),Y(6),Y(7) IF COORD. CHANGE
TSX DE6F+0491,2    FORM F5(II),F6(II),F7(II),F8(II)
TIX DE6F+0163,1,1  OR F6(II),F7(II),F8(II),F9(II)

STO COMMON+027     F8(II) OR F9(II)
STQ COMMON+028
CLA COMMON+003     F7(I) OR F8(I)
STO COMMON+029
CLA COMMON+004
STO COMMON+030
LXD DE6F+0529,1    11N(=11)11
LXA DE6F+0541,2    11
CLA COMMON+031,2   SAVE DIFF. AND F8(II),F7(I)
STO 0,1            T+19N+3+(11N)
TXI DE6F+0180,1,-1
TIX DE6F+0177,2,1
SXD DE6F+0529,1    SAVE FOR NEXT SET
LXD DE6F+0527,2
TXI DE6F+0184,2,-1
TIX DE6F+0128,4,1
TSX DE6F+0414,4    COMPLETE N EQNS.
CLA DE6F+0502      8(=1)0    TEST H (MAY TR R.K. AGAIN)
TNZ DE6F+0191      IF NOT=0, STILL IN COORD. CHG. OR NORMAL
CLA DE6F+0538      8 RESTORE COUNTER FOR
STO DE6F+0502      NEXT CHANGE IN COORD.
STZ DE6F+0500      RESTORE SWCH TO NORMAL

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DE6FN359
 DE6FN360
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 DE6FN407
 DE6FN408
 DE6FN409

DE6FN (Cont'd)

CLA DE6F+0519 H
 STO T+2=(H) RESTORE AFTER R.K.
 FAD T+1=T=INDEPENDENT VAR.
 STO COMMON+000 T+H/2 (MOST SIG.)
 STQ COMMON+001 LST, SIG.
 CLA COMMON+001
 FAD DE6F+0718 CUM, LST, SIG.
 FAD COMMON+000
 STQ DE6F+0718 SAVE LST, SIG. FOR NEXT INTEGRATION
 STO T+1=(T+H)
 LX A DE6F+0710,4 N
 LX A DE6F+0529,1 11N
 CLA DE6F+0530 T+19N+3+(7)
 STA DE6F+0208
 STA DE6F+0218 T+19N+3+(7)
 CLA DE6F+0520
 TSX DE6F+0344,2
 PZE 0,0,DE6F+0566 N+3+(7) STORED ABOVE (+11N)
 LDQ DE6F+0520 H SQ
 FMP 0,1 T+19N+3+(11N+7)=F8(II)
 TSX DE6F+0473,2
 FAD COMMON+003
 STO 0,4 T+N+3=NEW Y
 CLA DE6F+0717 TEST MISSING 1ST DERIV. IN F
 TMI DE6F+0224 =F(X,Y),+=F(X,Y,Y PRIME)
 CLA DE6F+0519 H
 TSX DE6F+0344,2
 PZE 0,0,DE6F+0587 N+3+(7) (+11N) INCR. BY 11
 LDQ DE6F+0519 H
 FMP 0,1 T+19N+3+(11N+9)=F7(I)
 TSX DE6F+0473,2
 FAD COMMON+003
 STO 0,4 T+2N+3=NEW Y PRIME
 CAL DE6F+0208 T+19N+3+(7)
 ADM DE6F+0541 11
 STA DE6F+0208
 STA DE6F+0218
 TXI DE6F+0229,1,-11 SET UP NEXT F8(II),F7(I)
 TIX DE6F+0206,4,1 LOOP FOR N EQNS.
 TSX 0,4 V (TR TO FORM 2ND DERIV.)
 LX A DE6F+0529,1 11N
 LX A DE6F+0710,4 N
 LX A DE6F+0541,2 11
 CLA 0,1 T+19N+3+(11N)
 STO COMMON+031,2 READ DIFF. TO COM+20
 TXI DE6F+0237,1,-1
 TIX DE6F+0234,2,1
 SXD DE6F+0529,1
 CLA 0,4 T+3N+3=Y(7) 2ND DERIV.
 STO COMMON+039 Y(7) 2ND DERIV.
 LX A DE6F+0536,1 6

DE6FN4100
 DE6FN4110
 DE6FN4120
 DE6FN4130
 DE6FN4140
 DE6FN4150
 DE6FN4160
 DE6FN4170
 DE6FN4180
 DE6FN4190
 DE6FN4200
 DE6FN4210
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 DE6FN4230
 DE6FN4240
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 DE6FN4270
 DE6FN4280
 DE6FN4290
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 DE6FN4370
 DE6FN4380
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 DE6FN4560
 DE6FN4570
 DE6FN4580
 DE6FN4590
 DE6FN4600

DE6FN (Cont'd)

LXA DE6F+0571,2 ZERO TO IR2
 FSB COMMON+026,2 Y(6) 2ND DERIV. D5(I)...D0(VI)
 STO COMMON+038,2 D6(I),D5(II),D4(III),...D1(VI)
 TXI DE6F+0246,2,1 WE ARE GOING BACKWARDS HERE
 TIX DE6F+0243,1,1
 CLA DE6F+0520 H SQ.
 TSX DE6F+0344,2 B(I) X DELTAS
 PZE DE6F+0573,0,COMMON+40
 LDQ DE6F+0520 H SQ.
 FMP COMMON+027 F8(II)
 TSX DE6F+0473,2
 FAD COMMON+003
 STO 0,4 T+N+3=NEW Y
 CLA DE6F+0500 TEST COORD. CHANGE
 TNZ DE6F+0258 CANNOT SAVE IF COORD. CHANGE
 STQ 0,4 T+9N+3=LST. SIG. (FOR R.K.)
 CLA DE6F+0519 H
 TSX DE6F+0344,2 B(I) DOT Y DELTAS
 PZE DE6F+0580,0,COMMON+40
 LDQ DE6F+0519 H
 FMP COMMON+029 F7(I)
 TSX DE6F+0473,2
 FAD COMMON+003
 STO 0,4 T+2N+3=NEW Y PRIME
 CLA DE6F+0500
 TNZ DE6F+0269
 STQ 0,4 T+5N+3=LST. SIG. (FOR R.K.)
 LXD DE6F+0529,1
 TIX DE6F+0233,4,1 COMPLETE N SETS
 TSX 0,4 V (FORM Y(7) 2ND DERIV.
 STZ DE6F+0522 CLEAR V
 STZ DE6F+0521 CLEAR W
 LXA DE6F+0529,4 11N
 LXA DE6F+0710,1 N
 SXD DE6F+0529,4 11N(-11)11
 LXA DE6F+0541,2 11
 CLA 0,4 T+19N+3+(11N)
 STO COMMON+031,2 READ DIFF. TO COM+20
 TXI DE6F+0281,4,-1
 TIX DE6F+0278,2,1
 CLA 0,1 T+3N+3=Y(7) 2ND DERIV.
 STO COMMON+039 Y(7) 2ND DERIV.
 CLA COMMON+029 F7(I) MOST SIG.
 STO COMMON+003
 CLA COMMON+030 F7(I) LST. SIG.
 STO COMMON+004
 CLA COMMON+039 Y(7) 2ND DERIV.
 TSX DE6F+0482,2
 STO COMMON+042 F8(I) MOST SIG.
 STQ COMMON+043 F8(I) LST. SIG.
 CLA COMMON+027 F8(II) MOST. SIG.

DE6FN461
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 DE6FN480
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 DE6FN482
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 DE6FN502
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 DE6FN507
 DE6FN508
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 DE6FN510
 DE6FN511

DE6FN (Cont'd)

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STO DE6F+0507
CLA COMMON+028      F8(II) LST. SIG.
STO DE6F+0508
TSX DE6F+0491,2      DOUBLE PREC. FAD
STO COMMON+040      F9(II) MOST. SIG.
STQ COMMON+041      F9(II) LST. SIG.
LXA DE6F+0536,4      .6
LXA DE6F+0571,2
CLA COMMON+039,2      Y(7) 2ND DERIV., D6(I),...,D1(VI)
FSB COMMON+026,2      Y(6) 2ND DERIV., D5(I),...,D0(VI)
STO COMMON+038,2      D6(I), D5(II),...,D1(VI)
TXI DE6F+0305,2,1      WE ARE GOING BACKWARDS HERE
TIX DE6F+0301,4,1
LXD DE6F+0529,4      11N(-11)11
LXA DE6F+0541,2      11
CLA COMMON+044,2      SAVE FOR NEXT INTEGRATION
STO 0,4      T+19N+3+(11N)
TXI DE6F+0311,4,-1
TIX DE6F+0308,2,1
TXH DE6F+0340,1,*      N=B IN DECR.
TIX DE6F+0276,1,1      COMPLETE N SETS
SSM      ==COWELL STEP
TRA DE6F+0072      RETURN TO PROGRAMMER
TSX DE6F+0380,2      NORMAL CASE (NO COORD. CHANGE)
PZE 0      T+11N+3+(7N) (FORM DIFF.)
CLA DE6F+0519      H
TSX DE6F+0344,2      FORM SUM OF PRODUCTS
PZE DE6F+0559,0,COMMON+21      D(I)XDELTAS
CLA 0,4      T+11N+3 (Y3 DOT)
TSX DE6F+0482,2      ADD Y3 DOT TO C+3,C+4
TSX DE6F+0373,2      F4(I) IN A1 AND A2
CLA DE6F+0507
STO DE6F+0714      F4(I)
CLA DE6F+0508
STO DE6F+0715
CLA DE6F+0520      H SQ.
TSX DE6F+0344,2      FORM SUM OF PRODUCTS
PZE DE6F+0552,0,COMMON+21      D(I) X DELTAS
CLA 0,4      T+10N+3 (Y3)
TSX DE6F+0482,2      ADD Y3 TO C+3,C+4
TSX DE6F+0373,2      F4(II) IN A1 AND A2
CLA DE6F+0714      F4(I)
STO COMMON+003
CLA DE6F+0715
STO COMMON+004
TXH DE6F+0453,4,*      N=B IN DECR. (TEST 1ST B EQNS)
TRA DE6F+0161
CLA 0,1      T+N+3=Y
STO DE6F+0711      Y
TSX DE6F+0455,2      FORM MAX V. W.
TRA DE6F+0313      FOR THIS Y

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DE6FN5120
DE6FN5130
DE6FN5140
DE6FN5150
DE6FN5160
DE6FN5170
DE6FN5180
DE6FN5190
DE6FN5200
DE6FN5210
DE6FN5220
DE6FN5230
DE6FN5240
DE6FN5250
DE6FN5260
DE6FN5270
DE6FN5280
DE6FN5290
DE6FN5300
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DE6FN5370
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DE6FN5580
DE6FN5590
DE6FN5600
DE6FN5610
DE6FN5620

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DE6FN (Cont'd)

STO COMMON+002
 SXD DE6F+0707,1
 SXD DE6F+0708,2
 CAL 1,2
 STA DE6F+0356
 ARS 18
 STA DE6F+0357
 CLA COMMON+008
 STO COMMON+014
 STZ COMMON+003
 STZ COMMON+004
 LXA DE6F+0537,1
 LDQ 0,1
 FMP 0,1
 TSX DE6F+0473,2
 TIX DE6F+0356,1,1
 LDQ COMMON+002
 FMP COMMON+003
 STO COMMON+003
 STQ COMMON+000
 LDQ COMMON+002
 FMP COMMON+004
 FAD COMMON+000
 FAD COMMON+003
 STO COMMON+003
 STQ COMMON+004
 LXD DE6F+0707,1
 LXD DE6F+0708,2
 TRA 2,2
 CLA COMMON+003
 FDP COMMON+002
 STQ DE6F+0507
 FAD COMMON+004
 FDP COMMON+002
 STQ DE6F+0508
 TRA 1,2
 SXD DE6F+0716,2
 CAL 1,2
 STA DE6F+0385
 LXD DE6F+0527,2
 LXA DE6F+0571,1
 CLA 0,2
 STO COMMON+005,1
 STO COMMON+020,1
 TXI DE6F+0389,1,~1
 TIX DE6F+0385,2,+
 LXA DE6F+0536,2
 SXD COMMON+000,2
 LXA DE6F+0571,1
 CLA COMMON+021,1
 FSB COMMON+020,1

H SQ, OR H IN AC
 SUB, TO FORM (CONSTANTS X DIFF.)
 A,0,B (A=CONSTANTS, B=DIFF.)
 CONSTANT ADDR, +7
 DIFF, ADDR, +7
 Y3, 2ND DERIV.
 (OR Y4 IF COORD, CHANGE)
 7
 CO+7, OR DO+7, OR N6+7, ETC.
 COMMON+21, OR COM+27, ETC.
 ACCUM. PRODUCT IN C+3,C+4.
 H SQ, OR H
 MOST SIG.
 H SQ, OR H
 MOST SIG, IN COMMON+3
 LST, SIG, IN COMMON+4
 DIVIDES C+3,C+4 BY C+2
 H SQ OR H
 MOST SIG, IN A1
 REMAINDER + LST, SIG.
 H SQ, OR H
 LST, SIG, IN A2
 MOVE 2ND DERIV. AND FORM DIFF.
 STARTING ADDR. OF 2ND DERIV.
 7N(-1)6N
 START ADDR. (T+11N+3+(7N), ETC.)
 MOVE 2ND DERIV. TO COM+5
 AND COM+20
 N IN DECR.
 6 (FORM DIFFERENCES)
 ZERO (2ND DERIV. STORED AT
 AT COMMON+5, AGAIN AT COM +20
 FORM DIFFERENCES IN

DE6FN560
 DE6FN564
 DE6FN565
 DE6FN566
 DE6FN567
 DE6FN568
 DE6FN569
 DE6FN570
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 DE6FN613

DE6FN (Cont'd)

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STO COMMON+020,1      COM+20 THRU COM+25
TXI DE6F+0397,1,-1
TIX DE6F+0393,2,1      LOOP 6,5,....,1 TIMES
LXD COMMON+000,2
TXH DE6F+0405,2,5      TR IF 1ST DIFF.
TXH DE6F+0408,2,3      TR IF 2ND OR 3RD DIFF.
TXH DE6F+0411,2,1      TR IF 4TH OR 5TH DIFF.
TIX DE6F+0391,2,1
LXD DE6F+0716,2
TRA 2,2
CLA COMMON+023         DELTA (I)3
STO COMMON+015         IN COM+15
TRA DE6F+0402
CLA COMMON+022         DELTA (II)2 OR DELTA (III)2
STO COMMON+021,2      IN COM+16 OR COM+17
TRA DE6F+0402
CLA COMMON+021         DELTA(IV)1 OR DELTA(V)1
STO COMMON+021,2      IN COM+18 OR COM+19
TRA DE6F+0402
CLA DE6F+0500          SWITCH (0=NORMAL CASE)
TNZ 1,4                - STOP TEST IF NON/ZERO
CLA DE6F+0501          TEST FIXED H
TMI 1,4                -=FIXED H INTERGRATION
CLA DE6F+0519          H=DELTA(T) COWELL TEST
FDP DE6F+0719          2.
STQ COMMON+000         H/2
CLA DE6F+0523          002.0 (WILL MULT BY 2 SQUARED
STO COMMON+001         WILL MULT VMAX,VMIN, AND WMAX
CLA DE6F+0509          MINIMUM H ALLOWED (CAN=0)
LRS 0                  SET SIGNS PLUS
TLQ DE6F+0438          H/2 LESS THAN H MIN.
CLA DE6F+0513          10 TO (3=S)/(H SQUARED) =MAX V
LDQ DE6F+0522          V=MAX (DELTA VI)/Y
TLQ DE6F+0438          V LESS THAN MAX. V
CLA COMMON+000         H/2 OR 2H
STO DE6F+0519          SET H=H/2 (OR 2H) AND
LXA DE6F+0533,4        3 (SCALE VMIN, VMAX, AND WMAX)
CLA DE6F+0515,4        VMIN, VMAX, AND WMAX
TZE DE6F+0436          SKIP IF ZERO
ADD COMMON+001         + OR - 002.0
STO DE6F+0515,4        NEW VALUES DUE TO CHANGE IN H
TIX DE6F+0432,4,1
TRA DE6F+0030          RETURN TO RUNGE KUTTA
CLA DE6F+0519          H=DELTA(T)
FAD DE6F+0519
STO COMMON+000         2H
SSP
LDQ DE6F+0510          MAXIMUM H ALLOWED
TLQ DE6F+0452          2H GREATER THAN H MAX.
LDQ DE6F+0512          10 TO (-1=S)/(H SQUARED)= VMIN
CLA DE6F+0522          V=MAX(DELTA VII)/Y

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DE6FN6140
DE6FN6150
DE6FN6160
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DE6FN6630
DE6FN6640

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TLQ DE6F+0452 V GR. THAN V MIN
CLS DE6F+0523 002.0 DIVIDES BY 2 SQUARED
STO COMMON+001 DECREASES VMIN, WMAX, VMAX
CLA DE6F+0514 10 TO  $(-1+S)/(H \text{ SQUARED}) = HMAX$ 
LDQ DE6F+0521 W=MAX (DELTA VII)/Y
TLQ DE6F+0429 W LESS THAN W MAX. (SET H=2H)
TRA 1,4 RETURN TO PROGRAM
TSX DE6F+0455,2 FORM LARGEST V AND W
TRA DE6F+0339
CLA DE6F+0501 SUB TO FORM MAX V AND W FOR 1ST N-B EQNS.
TMI 1,2 --=FIXED H INTEGRATION
CLA DE6F+0711 Y
SSP SET Y PLUS
LDQ DE6F+0511 A=MIN. Y ALLOWED
TLQ DE6F+0462 TR IF Y GREATER THAN Y MIN.
STQ DE6F+0711 OTHERWISE, SET Y=Y MIN.=A
SXD COMMON+002,1
LXA DE6F+0532,1
CLA COMMON+022,1
FDP DE6F+0711
CLA DE6F+0523,1
LRS 0
TLQ DE6F+0470
STQ DE6F+0523,1
TIX DE6F+0464,1,1
LXD COMMON+002,1
TRA 1,2
STQ COMMON+000
FAD COMMON+003
STQ COMMON+003
STQ COMMON+001
CLA COMMON+000
FAD COMMON+001
FAD COMMON+004
STQ COMMON+004
TRA 1,2
LST SIG. (PREC. AND 1/2)
MOST SIG.
STQ COMMON+000
FAD COMMON+003
STQ COMMON+003
STQ COMMON+000
CLA COMMON+000
UFA COMMON+004
FAD COMMON+003
STQ COMMON+003
STQ COMMON+004
TRA 1,2
LST. SIG.
UFA COMMON+003
STQ COMMON+003
STQ COMMON+000
CLA COMMON+000
UFA COMMON+004
FAD COMMON+003
STQ COMMON+003
STQ COMMON+004
TRA 1,2
ADDS AC TO COM+3, COM+4
AND STORES ANSWER IN C+3,C+4.
UFA COMMON+003
STQ COMMON+001
STQ COMMON+000
CLA COMMON+000
UFA DE6F+0508
MOST SIG. IN COMMON+3
LST. SIG. IN COMMON+4
DOUBLE PRECISION FAD
UFA COMMON+003
STQ COMMON+001
STQ COMMON+000
CLA COMMON+000
UFA DE6F+0508

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DE6FN-3

WDL DIVISION

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DEC 0 C3=0
DEC -5,125661376E-4 C4
DEC 0 C5=0
DEC +7,964065256E-5 C6
DEC +0,5 (SIGNS HAVE BEEN REVERSED) (D0)
DEC +8,333333333E-2 D1
DEC -4,166666667E-2 D2
DEC -1,527777778E-2 D3
DEC +7,638888889E-3 D4
DEC +3,1580688E-3 D5
DEC -1,5790344E-3 D6
DEC +6,549575617E-2 (NO CHANGE IN SIGNS) (N6)
DEC +6,820436508E-2 N5
DEC +7,134589948E-2 N4
DEC +0,075 N3
DEC +7,916666667E-2 N2
DEC +8,333333333E-2 N1
DEC +8,333333333E-2 N0
DEC -2,708608907E-3 B6
DEC -3,141534392E-3 B5
DEC -3,654100529E-3 B4
DEC -4,166666667E-3 B3
DEC -4,166666667E-3 B2
DEC 0 B1=0
DEC +8,333333333E-2 B0
DEC -1,136739418E-2 B6 DOT
DEC -1,426917989E-2 B5 DOT
DEC -1,875E-2 B4 DOT
DEC -2,638888889E-2 B3 DOT
DEC -4,166666667E-2 B2 DOT
DEC -8,333333333E-2 B1 DOT
DEC +0,5 B0 DOT
DEC .304224537 (NO CHANGE IN SIGNS) (N6 DOT)
DEC .315591931 N5 DOT
DEC .329861111 N4 DOT
DEC .348611111 N3 DOT
DEC .375000000 N2 DOT
DEC .416666666 N1 DOT
DEC .500000000 N0 DOT
TRA DE6F+0725 TO SET UP ROUTINE (RUNGE KUTTA SUB)
SXD DE6F+0707,1 SAVE INDEX REG.
SXD DE6F+0708,2 FROM
SXD DE6F+0709,4 MAIN PROGRAM (NEW R.K. STARTS)
CLA 0 (T+2)=H
STO DE6F+0713 H
FDP DE6F+0719 2,
STQ DE6F+0714 H/2
STQ DE6F+0715 H/2
FMP DE6F+0713 H
STO DE6F+0711 (H SQ)/2
FDP DE6F+0720 4,

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[illegible]

DE6FN (Cont'd)

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STQ DE6F+0712.      (H SQ)/8
CLA DE6F+0713      H
FDP DE6F+0722      6,
STQ DE6F+0716      H/6
LXA DE6F+0710,1    N
CLA 0,1            SAVE YI (T+N+3)=YI (M.S.)
STO 0,1            (T+8N+3)=YI MOST SIG.
CLA 0,1            SAVE YI PRIME (T+2N+3)
STO 0,1            (T+4N+3)=YI PRIME MOST SIG.
TIX DE6F+0604,1,1
LXA DE6F+0723,1    1
SXD DE6F+0724,1    K=1(+1)4
LXA DE6F+0710,6    N TO IR2 AND IR4
TXL DE6F+0629,1,1  TR IF K=1
TXL DE6F+0649,1,2  TR IF K=2
TXL DE6F+0629,1,3  TR IF K=3
LXA DE6F+0710,2    K=4 (N TO IR4)
CLA 0,2            T+3N+3=F(X,Y,Y PRIME)
FAD 0,2            T+6N+3=CUM. D(YN) PRIME
STO 0,2            T+6N+3=NEW D(YN) PRIME
TIX DE6F+0616,2,1
TXH DE6F+0669,1,3  OUT IF K=4
TIX DE6F+0615,1,1  ADD 2F(X,Y,PRIME) IF K=2,3
LXD DE6F+0724,1    K
TXH DE6F+0626,1,2  TR IF K=3
CLA DE6F+0717      TEST MISSING 1ST DERIV. IN F
TMI DE6F+0628      +=F(X,Y,Y PRIME)
TSX 0,4            V (TR OUT FOR F(X,Y,Y PRIME)
LXD DE6F+0724,1
TXI DE6F+0610,1,1  INCREASE K BY 1
CLA 0              T+1=(T)
FAD DE6F+0714      H/2
STO COMMON+000     T+H/2 (MOST SIG.)
STQ COMMON+001     LST. SIG.
CLA COMMON+001
FAD DE6F+0718      CUM. LST. SIG.
FAD COMMON+000
STQ DE6F+0718      SAVE LST. SIG. FOR NEXT INTEGRATION
STO 0              T+1=(T+H/2)
TIX DE6F+0639,1,1  IR1=1 IF K=1, IR1=2 IF K=3
LDQ DE6F+0713,1    (H SQ)/8 OR (H SQ)/2 (K=1,3)
FMP 0,2            T+3N+3=F(X,Y,Y PRIME)
STO COMMON+000
LDQ DE6F+0715,1    (H/2) OR (H) K=1 OR 3
FMP 0,2            T+4N+3=YN PRIME (M.S.)
FAD COMMON+000     (H SQ)/8 X F(X,Y,YP)
FAD 0,2            T+8N+3=YN (M.S.)
STO 0,2            T+N+3=YN AT (T+H/2) OR (T+H)
TIX DE6F+0639,2,1  N WAS IN IR2
LXD DE6F+0724,1    RESTORE K TO 1 OR 3
CLA DE6F+0717      TEST MISSING 1ST DERIV. IN F

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DE6FN8180
DE6FN8190
DE6FN8200
DE6FN8210
DE6FN8220
DE6FN8230
DE6FN8240
DE6FN8250
DE6FN8260
DE6FN8270
DE6FN8280
DE6FN8290
DE6FN8300
DE6FN8310
DE6FN8320
DE6FN8330
DE6FN8340
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DE6FN8370
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DE6FN8670
DE6FN8680

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DEOFN (Cont'd)

TMI DE6F+0656	=F(X,Y), +=F(X,Y,Y PRIME)	DE6FN86
LDQ DE6F+0716,1	H/2 OR H	DE6FN87
FMP 0,4	T+3N+3=F(X,Y,Y PRIME)	DE6FN87
FAD 0,4	T+4N+3=YN PRIME (M.S.)	DE6FN87
STO 0,4	T+2N+3=NEW Y PRIME	DE6FN87
TIX DE6F+0651,4,1		DE6FN87
LXA DE6F+0710,2	N	DE6FN87
TXL DE6F+0664,1,1	TR TO STORE IF K=1	DE6FN87
CLA 0,2	T+3N+3=F(X,Y,Y PRIME)	DE6FN87
FAD 0,2	T+7N+3=CUM.DELTA(YN)	DE6FN87
STO 0,2	T+7N+3	DE6FN87
TIX DE6F+0658,2,1		DE6FN88
TXL DE6F+0615,1,2	TR IF K=2 (CONNOT=1)	DE6FN88
TXI DE6F+0615,1,-1	REDUCE K FROM 3 TO 2	DE6FN88
CLA 0,2	T+3N+3=F(X,Y,Y PRIME)	DE6FN88
STO 0,2	T+6N+3=STORE FOR D(YN)PRIME	DE6FN88
STO 0,2	T+7N+3=STORE FOR D(YN)	DE6FN88
TIX DE6F+0664,2,1	N WAS IN IR2	DE6FN88
TRA DE6F+0626	TR FOR K=2	DE6FN88
LXA DE6F+0717,4	2N	DE6FN88
LXA DE6F+0710,2	N	DE6FN88
LDQ DE6F+0716	H/6	DE6FN89
FMP 0,4	T+7N+3=D(YN)P AND D(YN)	DE6FN89
STQ COMMON+002		DE6FN89
UFA 0,2	T+4N+3=YN PRIME (M.S.)	DE6FN89
STO COMMON+000		DE6FN89
STQ COMMON+001		DE6FN89
CLA COMMON+001		DE6FN89
UFA 0,2	T+5N+3=YN PRIME (LST. SIG.)	DE6FN89
UFA COMMON+002		DE6FN89
FAD COMMON+000		DE6FN89
STO 0,4	T+3N+3=(YN)P AND (YN) (M.S.)	DE6FN90
STQ 0,4	T+7N+3=(YN)P AND (YN) (L.S.)	DE6FN90
TNX DE6F+0686,4,1	(YN) DESTROYS F(X,Y,Y PRIME)	DE6FN90
TIX DE6F+0671,2,1	(YN)P AT T+N+3 (COMPLETED)	DE6FN90
TRA DE6F+0670	(YN) AT T+2N+3 (NOT COMPLETED)	DE6FN90
LXA DE6F+0710,2	N	DE6FN90
LDQ DE6F+0713	H	DE6FN90
FMP 0,2	T+3N+3=(YN PRIME + H/6(DY)	DE6FN90
STQ COMMON+002		DE6FN90
UFA 0,2	T+8N+3=YN (M.S.)	DE6FN90
STO COMMON+000		DE6FN91
STQ COMMON+001		DE6FN91
CLA COMMON+001		DE6FN91
UFA 0,2	T+9N+3=YN (L.S.)	DE6FN91
UFA COMMON+002		DE6FN91
FAD COMMON+000		DE6FN91
STO 0,2	T+N+3=Y(N+1) (M.S.)	DE6FN91
STQ 0,2	T+9N+3=Y(N+1) (L.S.)	DE6FN91
CLA 0,2	T+6N+3=Y(N+1)P (L.S.)	DE6FN91
STO 0,2	T+5N+3 (SAVE LST. SIG.)	DE6FN91

DE6FN (Cont'd)

TIX DE6F+0687,2,1

TSX 0,4

LXD DE6F+0709,4

LXD DE6F+0707,1

LXD DE6F+0708,2

TRA 1,4

PZE 2,0,0

BSS 11

DEC 2.

DEC 4.

DEC 8.

DEC 6.

DEC 1

BSS 1

SXD DE6F+0707,1

SXD DE6F+0708,2

SXD DE6F+0709,4

STZ DE6F+0718

CLA 1,4

STA DE6F+0708

STO DE6F+0717

STA DE6F+0737

ARS 18

STA DE6F+0796

STA DE6F+0702

STA DE6F+0626

CLA

STO DE6F+0710

CAL DE6F+0708

ADD DE6F+0723

STA DE6F+0629

STA DE6F+0637

ADD DE6F+0723

STA DE6F+0591

ADD DE6F+0723

ADM DE6F+0710

STA DE6F+0604

STA DE6F+0697

STA DE6F+0646

ADM DE6F+0710

STA DE6F+0606

STA DE6F+0654

ADM DE6F+0710

STA DE6F+0616

STA DE6F+0681

STA DE6F+0640

STA DE6F+0652

STA DE6F+0658

STA DE6F+0664

STA DE6F+0688

V (FORM 2ND DERIV.)

LEAVE SUB. FROM 2ND ENTRY
IR1 SAVED IN DECR.

2.

4.

8.

6.

1

K=1(+1)4

R.K. SET UP ENTRY

CLEAR LST. SIG. OF T

T,0,V

T=ADDRESS

=F(X,Y), +=F(X,Y,Y PRIME)

V TO ADDR.

V

V

(T)=N

N

T

1

T+1

1

T+2

1

N

T+N+3=YI (STARTS AT T+3)

T+N+3=YI

T+N+3

N

T+2N+3=YI PRIME (STARTS T+N+3)

N

T+3N+3=2ND DERIV.

T+3N+3

T+3N+3

T+3N+3

T+3N+3

DE6FN9200

DE6FN9210

DE6FN9220

DE6FN9230

DE6FN9240

DE6FN9250

DE6FN9260

DE6FN9270

DE6FN9280

DE6FN9290

DE6FN9300

DE6FN9310

DE6FN9320

DE6FN9330

DE6FN9340

DE6FN9350

DE6FN9360

DE6FN9370

DE6FN9380

DE6FN9390

DE6FN9400

DE6FN9410

DE6FN9420

DE6FN9430

DE6FN9440

DE6FN9450

DE6FN9460

DE6FN9470

DE6FN9480

DE6FN9490

DE6FN9500

DE6FN9510

DE6FN9520

DE6FN9530

DE6FN9540

DE6FN9550

DE6FN9560

DE6FN9570

DE6FN9580

DE6FN9590

DE6FN9600

DE6FN9610

DE6FN9620

DE6FN9630

DE6FN9640

DE6FN9650

DE6FN9660

DE6FN9670

DE6FN9680

DE6FN9690

DE6FN9700

DE6FN (Cont'd)

ADM DE6F+0710	N	DE6FN9710
STA DE6F+0653	T+4N+3	DE6FN9720
STA DE6F+0607		DE6FN9730
STA DE6F+0643	T+4N+3	DE6FN9740
STA DE6F+0674	T+4N+3	DE6FN9750
ADM DE6F+0710	N	DE6FN9760
STA DE6F+0793	T+5N+3	DE6FN9770
STA DE6F+0700		DE6FN9780
STA DE6F+0678		DE6FN9790
ADM DE6F+0710	N	DE6FN9800
STA DE6F+0617	T+6N+3	DE6FN9810
STA DE6F+0618		DE6FN9820
STA DE6F+0665		DE6FN9830
STA DE6F+0699	T+6N+3	DE6FN9840
ADM DE6F+0710	N	DE6FN9850
STA DE6F+0660	T+7N+3	DE6FN9860
STA DE6F+0672		DE6FN9870
STA DE6F+0659		DE6FN9880
STA DE6F+0666		DE6FN9890
STA DE6F+0682	T+7N+3	DE6FN9900
ADM DE6F+0710	N	DE6FN9910
STA DE6F+0605	T+8N+3	DE6FN9920
STA DE6F+0645		DE6FN9930
STA DE6F+0690		DE6FN9940
ADM DE6F+0710	N	DE6FN9950
STA DE6F+0694	T+9N+3	DE6FN9960
STA DE6F+0698	T+9N+3	DE6FN9970
STA DE6F+0794		DE6FN9980
		DE6FN9990

DE6FN (Cont'd)

```

CAL DE6F*0710      N
PAX 0,1            N TO IR1
ADM DE6F*0710      N
STA DE6F*0717      2N TO ADDR. OF SAVE*10
STZ 0,1            T*5N*3 (CLEAR Y PRIME L.S.)
STZ 0,1            T*9N*3 (CLEAR Y LST. SIG.)
TIX DE6F*0793,1,1
TSX 0,4            V (FORM 2ND DERIV.)
LXD DE6F*0709,4    RESTORE IRC
TXI DE6F*0704,4,-1 TRA 2,4 FROM HERE
SXD DE6F*0504,1    COWELL SETUP
SXD DE6F*0505,2
SXD DE6F*0506,4
CLA 1,4            T,0,V
STO DE6F*0805      FIX RUNGE KUTTA (1ST ENTRY)
TSX DE6F*0587,4    TR TO SET UP RUNGE KUTTA
PZE                T,0,V
LXD DE6F*0506,4    RESTORE IR4 AFTER R,K.
CAL DE6F*0702      V
STA DE6F*0107      V
STA DE6F*0230      V
STA DE6F*0271      V
CAL DE6F*0717      2N
STA DE6F*0526
ADM DE6F*0645      T*8N*3
STA DE6F*0134      T*10N*3=T*3N*3+(7N)
STA DE6F*0066
STA DE6F*0331
ADM DE6F*0710      N
STA DE6F*0103      T*11N*3=T*3N*3+(8N)
STA DE6F*0111      T*3N*3+(8N)
STA DE6F*0146      T*4N*3+(7N)
STA DE6F*0068      T*11N*3
STA DE6F*0321
CAL DE6F*0794      T*9N*3
STA DE6F*0257
CAL DE6F*0700      T*5N*3
STA DE6F*0268
CAL DE6F*0681      T*3N*3
STA DE6F*0049
STA DE6F*0110
STA DE6F*0239
STA DE6F*0282      T*3N*3
CAL DE6F*0606      T*2N*3
STA DE6F*0067
STA DE6F*0104
STA DE6F*0223
STA DE6F*0265      T*2N*3
CAL DE6F*0697      T*N*3
STA DE6F*0065
STA DE6F*0102

```

```

DE6FN10000
DE6FN10010
DE6FN10020
DE6FN10030
DE6FN10040
DE6FN10050
DE6FN10060
DE6FN10070
DE6FN10080
DE6FN10090
DE6FN10100
DE6FN10110
DE6FN10120
DE6FN10130
DE6FN10140
DE6FN10150
DE6FN10160
DE6FN10170
DE6FN10180
DE6FN10190
DE6FN10200
DE6FN10210
DE6FN10220
DE6FN10230
DE6FN10240
DE6FN10250
DE6FN10260
DE6FN10270
DE6FN10280
DE6FN10290
DE6FN10300
DE6FN10310
DE6FN10320
DE6FN10330
DE6FN10340
DE6FN10350
DE6FN10360
DE6FN10370
DE6FN10380
DE6FN10390
DE6FN10400
DE6FN10410
DE6FN10420
DE6FN10430
DE6FN10440
DE6FN10450
DE6FN10460
DE6FN10470
DE6FN10480
DE6FN10490
DE6FN10500

```


DE6FN (Cont'd)

STA DE6F+0129		DE6FN105
STA DE6F+0213		DE6FN105
STA DE6F+0254		DE6FN105
STA DE6F+0340	T+N+3	DE6FN105
CAL DE6F+0629	T+1	DE6FN105
STA DE6F+0093		DE6FN105
STA DE6F+0094		DE6FN105
STA DE6F+0097		DE6FN105
STA DE6F+0099		DE6FN105
STA DE6F+0193		DE6FN106
STA DE6F+0200	T+1	DE6FN106
CAL DE6F+0591	T+2	DE6FN106
STA DE6F+0032		DE6FN106
STA DE6F+0091		DE6FN106
STA DE6F+0923	T+2	DE6FN106
STA DE6F+0098		DE6FN106
STA DE6F+0115		DE6FN106
STA DE6F+0192	T+2	DE6FN106
LDQ DE6F+0538	8	DE6FN106
MPY DE6F+0710	N	DE6FN107
STQ DE6F+0528	8N	DE6FN107
CAL DE6F+0528	8N	DE6FN107
SBM DE6F+0710	N	DE6FN107
STA DE6F+0527	7N	DE6FN107
ADM DE6F+0526	2N	DE6FN107
ADM DE6F+0526	2N	DE6FN107
STA DE6F+0529	11N	DE6FN107
ADM DE6F+0672	T+7N+3	DE6FN107
STA DE6F+0050	T+18N+3=T+11N+3+(7N)	DE6FN107
STA DE6F+0317	T+18N+3=T+11N+3+(7N)	DE6FN108
ADM DE6F+0710	N	DE6FN108
STA DE6F+0101	T+19N+3=T+11N+3+(8N)	DE6FN108
ADM DE6F+0537	7	DE6FN108
STA DE6F+0530	T+19N+10=T+19N+3+(7)	DE6FN108
CAL DE6F+0101	T+19N+3	DE6FN108
ADM DE6F+0529	11N	DE6FN108
STA DE6F+0178	T+30N+3=T+19N+3+(11N)	DE6FN108
STA DE6F+0234		DE6FN108
STA DE6F+0278		DE6FN108
STA DE6F+0309	T+30N+3	DE6FN109
ADM DE6F+0537	7	DE6FN109
STA DE6F+0210	T+30N+10=T+19N+3+(11N+7)	DE6FN109
ADM DE6F+0532	2	DE6FN109
STA DE6F+0220	T+30N+12=T+19N+3+(11N+9)	DE6FN109
CAL DE6F+0317	7+18N+3	DE6FN109
SBM DE6F+0526	2N	DE6FN109
STA DE6F+0149	T+16N+3	DE6FN109
SBM DE6F+0710	N	DE6FN109
STA DE6F+0138	T+15N+3	DE6FN109
LXA DE6F+0710,1	N	DE6FN110
SXD DE6F+0389,1	N TO DECR.	DE6FN110

DE6FN (Cont'd)

```

CLA 2,4          PZE=VAR, STEP SIZE (B,0,R)
STO DE6F+0501    MZE=FIXED STEP SIZE
STZ COMMON+000
STA COMMON+000    B (B LESS THAN OR =N)
STZ DE6F+0516
STD DE6F+0516     R=TOTAL R.K. LOOPS PER D(T)
CLA DE6F+0516
ARS 18
TNZ DE6F+0903
LXA DE6F+0534,1   4
SXD DE6F+0516,1   IF R=0, SET R=4
CLA DE6F+0534     4
ADD DE6F+0524     2330000000000
FAD DE6F+0571     FLOAT FIXED PT. NO.
STO DE6F+0517     R IN FLOATING PT.
CLA COMMON+000    TEST B=0
TNZ DE6F+0910
CLA DE6F+0710     IF B=0, SET B=N
STA COMMON+000    N
CAL DE6F+0710     N
SBM COMMON+000    B (OR N, IF B=0)
TPL DE6F+0914     PROGRAMMER GOOFED, IF MINUS
CLM              SET B=N IF B TOO LARGE (N-B=0)
ALS 18           N-B TO DECR.
STD DE6F+0338    1ST B EQNS. TESTED
STD DE6F+0312    N=B
CLA 3,4          S
TNZ DE6F+0920    IF S=0, SET S=9
CLA DE6F+0954    1E-9
STO COMMON+000   S (SEE VMIN,VMAX,WMAX.
STZ DE6F+0503    +=R.K., +=COWELL
STZ DE6F+0709    +=1ST R.K. INTEGRATION, +=2ND, ETC.
CLA              T+2=DELTA(T)=H
STO DE6F+0519
CLA 6,4          A=MIN. Y ALLOWED
TNZ DE6F+0928
CLA DE6F+0543    1. (IF A=0, SET A=1.)
STO DE6F+0511
CLA 4,4          MINIMUM H ALLOWED (FLOATING PT.)
SSP
STO DE6F+0509
CLA 5,4          MAXIMUM H ALLOWED (FLOATING PT.)
SSP
TNZ DE6F+0936    IF H=0, SET HMAX= 1E18
CLA DE6F+0525    1E18
STO DE6F+0510
LDQ DE6F+0519    DELTA(T)=H
FMP DE6F+0519
STO DE6F+0520    H SQ.
CLA COMMON+000   1E-S
FDP DE6F+0520    H SQ.

```

```

DE6FN11020
DE6FN11030
DE6FN11040
DE6FN11050
DE6FN11060
DE6FN11070
DE6FN11080
DE6FN11090
DE6FN11100
DE6FN11110
DE6FN11120
DE6FN11130
DE6FN11140
DE6FN11150
DE6FN11160
DE6FN11170
DE6FN11180
DE6FN11190
DE6FN11200
DE6FN11210
DE6FN11220
DE6FN11230
DE6FN11240
DE6FN11250
DE6FN11260
DE6FN11270
DE6FN11280
DE6FN11290
DE6FN11300
DE6FN11310
DE6FN11320
DE6FN11330
DE6FN11340
DE6FN11350
DE6FN11360
DE6FN11370
DE6FN11380
DE6FN11390
DE6FN11400
DE6FN11410
DE6FN11420
DE6FN11430
DE6FN11440
DE6FN11450
DE6FN11460
DE6FN11470
DE6FN11480
DE6FN11490
DE6FN11500
DE6FN11510
DE6FN11520

```

DE6FN (Cont'd)

FMP DE6F+0952	.1	DE6FN115
STO DE6F+0512	$VMIN=(10)**(-1-S)/H SQ.$	DE6FN115
STO DE6F+0514	WMAX	DE6FN115
FDP DE6F+0953	$1E-4$	DE6FN115
STQ DE6F+0513	$VMAX=(10)**(3-S)/H SQ.$	DE6FN115
STZ DE6F+0500	SWITCH (PROGRAMMER SETS NON/ZERO)	DE6FN115
CLA DE6F+0538	8 (SET UP COUNTER IN CASE	DE6FN115
STO DE6F+0502	OF CHANGE IN COORD.)	DE6FN115
LXD DE6F+0506,4	RETURN TO PROGRAMMER, (1ST ENTRY)	DE6FN115
TXI DE6F+0074,4,-6	TRA 7,4	DE6FN115
DEC .1	.1	DE6FN115
DEC $1E-4$	$.0001 \pm 1E-4$	DE6FN115
DEC $1E-9$	$1E-9$ (IF $S=0$)	DE6FN115
BREAK EQU *		DE6FN115
END EQU *		DE6FN115

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Function: DOT

Purpose: To find the dot product of two three-dimensional vectors.

Calling Sequence:

Z = DOT (X, Y)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	X	3			First input vector
I	Y	3			Second input vector
O	Z				$Z = X(1)Y(1)+X(2)Y(2)+X(3)Y(3)$

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

DOT

```
* LABEL
* SYMBOL TABLE
FUNCTION DOT(X,Y)
DIMENSION X(3),Y(3)
DOT = X(1)*Y(1) + X(2)*Y(2) + X(3)*Y(3)
RETURN
END
```

```
DOT0
DOT0
DOT0000
DOT0010
DOT0020
DOT0030
DOT0
```

Subroutine: EARTR

Purpose: Subroutine EARTR determines which tracking stations can observe the vehicle at the time EARTR is called. The subroutine then updates the state covariance matrix for the types of observations being performed by the tracking station. The possible types of observations are: range, range rate, azimuth-elevation, and direction cosines. The measurements may be corrupted by the following types of errors: random, bias, time bias, and station location errors. The subroutine input and output quantities are in common storage.

Calling Sequence:

CALL EARTR

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities placed in common

Common storages used or required:

T, S, C, IC

Subroutines required:

CORRTP, DOT, GHA, INTRI, MATRX,
NUTAIT, SETN, TRAC, TRANSH

Functions required:

ARKTNS, ATAN, COS,
FNORM, SQRT, SIN

Approximate number of storages required: 1530

EARTR Partial Derivatives

To perform the covariance matrix updating for earth based tracking observations, a number of partial derivatives are required. The updating of the covariance matrix for observations requires the partial derivatives relating the types of measurements and the vehicle state. The evaluation of the errors in the measurements due to station location errors and time bias requires the partials which relate the measurements and the station latitude, longitude, altitude, and time.

The following quantities and relationships are used in the derivations of the various partials. Four important vectors are obtained by calling subroutine TRAC. Three unit vectors, \hat{U} , \hat{E} , \hat{N} , which form a topocentric orthogonal coordinate system and the vector X_T are obtained from the center of the earth to tracker.

The unit vectors are the up, east, and north vectors. These vectors may be written as follows:

$$U_1 = \cos(\text{LAT}) \cos(\text{LON})$$

$$U_2 = \cos(\text{LAT}) \sin(\text{LON})$$

$$U_3 = \sin(\text{LAT})$$

$$E_1 = -\sin(\text{LON})$$

$$E_2 = \cos(\text{LON})$$

$$E_3 = 0$$

$$N_1 = -\sin(\text{LAT}) \cos(\text{LON})$$

$$N_2 = -\sin(\text{LAT}) \sin(\text{LON})$$

$$N_3 = \cos(\text{LAT})$$

$$\text{LON} = \omega(t + t_0) + \text{LON}'$$

$$\text{LON}' = \text{STATION LONGITUDE}$$

$$\omega = \text{EARTH'S ROTATION RATE}$$

$$\omega t_0 = \text{GREENWICH'S LONGITUDE AT EPOCH}$$

$$x_T = \left(\frac{R_E}{C} + H \right) U_1$$

H = ALTITUDE

$$y_T = \left(\frac{R_E}{C} + H \right) U_2$$

$$C = \left[\cos^2(\text{LAT}) + \frac{R_P^2}{R_E^2} \sin^2(\text{LAT}) \right]^{1/2}$$

$$z_T = \left(\frac{R_P^2}{R_E C} + H \right) U_3$$

 R_E = EQUATORIAL RADIUS R_P = POLAR RADIUS

The vehicle's position, \vec{X}_V , and velocity, \vec{X}_V , are obtained from common storage.

$$\vec{X}_V = \begin{pmatrix} x_v \\ y_v \\ z_v \end{pmatrix}$$

$$\dot{\vec{X}}_V = \begin{pmatrix} \dot{x}_v \\ \dot{y}_v \\ \dot{z}_v \end{pmatrix}$$

The tracking station velocity is obtained by differentiating \vec{X}_T .

$$\frac{d}{dt} (\vec{X}_T) = \dot{\vec{X}}_T = \begin{pmatrix} \dot{x}_T \\ \dot{y}_T \\ \dot{z}_T \end{pmatrix}$$

$$\dot{x}_T = -\omega \left(\frac{R_E}{C} + H \right) \cos(\text{LAT}) \sin(\text{LON})$$

$$\dot{y}_T = \omega \left(\frac{R_E}{C} + H \right) \cos(\text{LAT}) \cos(\text{LON})$$

$$\dot{z}_T = 0$$

The vector from the tracking station to vehicle may then be written as

$$\begin{array}{ccccccc} \vec{X} & = & \begin{pmatrix} X_1 \\ X_2 \\ X_3 \end{pmatrix} & = & \vec{X}_V - \vec{X}_T & = & \begin{pmatrix} X_V - X_T \\ Y_V - Y_T \\ Z_V - Z_T \end{pmatrix} \\ 3 \times 1 & & 3 \times 1 & & 3 \times 1 & & 3 \times 1 \end{array}$$

A relationship which will be used in the derivations is

$$\frac{\partial \text{PAR}}{\partial \vec{X}_V} = \frac{\partial \text{PAR}}{\partial \vec{X}}$$

The FORTRAN program names for the above vectors are as follows:

<u>FORTTRAN</u> <u>NAME</u>	<u>DIMENSION</u>	<u>DERIVATION</u> <u>NAME</u>	<u>DIMENSION</u>
U	(3)	U	(3)
E	(3)	E	(3)
EN	(3)	N	(3)
X	(3)	X_V	(3)
RT	(3)	X_T	(3)
Y	(3)	$X = X_V - X_T$	(3)
A	(1)	R_E	(1)
B	(1)	R_P	(1)
RAT	(1)	$ X $	(1)
XD	(3)	$\dot{X} = \dot{X}_V - \dot{X}_T$	(3)

The quantities being measured are the following:

$$R = \text{RANGE} = |\vec{X}| = (\vec{X} \cdot \vec{X})^{1/2}$$

$$\dot{R} = \text{RANGE RATE} = \frac{d}{dt} |\vec{X}| = \frac{\vec{X} \cdot \dot{\vec{X}}}{R}$$

$$AZ = \tan^{-1} \left\{ \frac{\vec{X} \cdot \hat{E}}{\vec{X} \cdot \hat{N}} \right\}$$

$$EL = \sin^{-1} \frac{(\hat{U} \cdot \vec{X})}{R}$$

Below is a list of partial derivatives which will be used in the application of the chain rule for partial derivatives.

$$\frac{\partial U_1}{\partial LAT} = N_1$$

$$\frac{\partial E_1}{\partial LAT} = 0$$

$$\frac{\partial U_2}{\partial LAT} = N_2$$

$$\frac{\partial E_2}{\partial LAT} = 0$$

$$\frac{\partial U_3}{\partial LAT} = N_3$$

$$\frac{\partial E_e}{\partial LAT} = 0$$

$$\frac{\partial U_1}{\partial LON} = \cos(LAT) \sin(LON)$$

$$\frac{\partial E_1}{\partial LON} = -\cos(LON)$$

$$\frac{\partial U_2}{\partial LON} = \cos(LAT) \cos(LON)$$

$$\frac{\partial E_2}{\partial LON} = -\sin(LON)$$

$$\frac{\partial U_3}{\partial LON} = 0$$

$$\frac{\partial E_3}{\partial LON} = 0$$

$$\frac{\partial U_1}{\partial ALT} = 0$$

$$\frac{\partial E_1}{\partial ALT} = 0$$

$$\frac{\partial U_2}{\partial ALT} = 0$$

$$\frac{\partial E_2}{\partial ALT} = 0$$

$$\frac{\partial U_3}{\partial ALT} = 0$$

$$\frac{\partial E_3}{\partial ALT} = 0$$

$$\frac{\partial N_1}{\partial LAT} = -U_1$$

$$\frac{\partial N_2}{\partial LAT} = -U_2$$

$$\frac{\partial N_3}{\partial LAT} = -U_3$$

$$\frac{\partial N_1}{\partial LON} = \sin(LAT) \sin(LON)$$

$$\frac{\partial N_2}{\partial LON} = -\sin(LAT) \cos(LON)$$

$$\frac{\partial N_3}{\partial LON} = 0$$

$$\frac{\partial N_1}{\partial ALT} = 0$$

$$\frac{\partial N_2}{\partial ALT} = 0$$

$$\frac{\partial N_3}{\partial ALT} = 0$$

$$\frac{\partial U_1}{\partial t} = -\omega \sin(LON) \cos(LAT)$$

$$\frac{\partial U_2}{\partial t} = \omega \cos(LON) \cos(LAT)$$

$$\frac{\partial U_3}{\partial t} = 0$$

$$\frac{\partial E_1}{\partial t} = -\omega \cos(LON)$$

$$\frac{\partial E_2}{\partial t} = -\omega \sin(LON)$$

$$\frac{\partial E_3}{\partial t} = 0$$

$$\frac{\partial N_1}{\partial t} = \omega \sin(LAT) \sin(LON)$$

$$\frac{\partial N_2}{\partial t} = -\omega \sin(LAT) \cos(LON)$$

$$\frac{\partial N_3}{\partial t} = 0$$

FORTTRAN 3x3 matrix called DRT

$$DRT = \begin{pmatrix} \frac{\partial X_1}{\partial LAT} & \frac{\partial X_1}{\partial LON} & \frac{\partial X_1}{\partial ALT} \\ \frac{\partial X_2}{\partial LAT} & \frac{\partial X_2}{\partial LON} & \frac{\partial X_2}{\partial ALT} \\ \frac{\partial X_3}{\partial LAT} & \frac{\partial X_3}{\partial LON} & \frac{\partial X_3}{\partial ALT} \end{pmatrix}$$

3x3 3x3

$$DRT(1,1) = - \frac{\partial \dot{x}_T}{\partial LAT} = \left(\frac{R_E}{C} + H \right) \sin(LAT) \cos(LON) + U_1 \frac{R_E}{C^2} \frac{\partial C}{\partial LAT}$$

$$\frac{\partial C}{\partial LAT} = \frac{\sin(LAT) \cos(LAT)}{C} \left(1 - \frac{R_P^2}{R_E^2} \right)$$

$$DRT(2,1) = - \frac{\partial \dot{y}_T}{\partial LAT} = U_2 \frac{R_E}{C^2} \frac{\partial C}{\partial LAT} + \left(\frac{R_E}{C} + H \right) \sin(LAT) \sin(LON)$$

$$DRT(3,1) = - \frac{\partial \dot{z}_T}{\partial LAT} = - \left(\frac{R_P^2}{R_E C} + H \right) \cos(LAT) + U_3 \frac{R_P^2}{R_E C^2} \frac{\partial C}{\partial LAT}$$

$$DRT(1,2) = - \frac{\partial \dot{x}_T}{\partial LON} = -E_1 \left(\frac{R_E}{C} + H \right) \cos(LAT)$$

$$DRT(2,2) = - \frac{\partial \dot{y}_T}{\partial LON} = -E_2 \left(\frac{R_E}{C} + H \right) \cos(LAT)$$

$$DRT(3,2) = 0$$

$$DRT(1,3) = -U_1$$

$$DRT(2,3) = -U_2$$

$$DRT(3,3) = -U_3$$

$$\frac{\partial \dot{x}_1}{\partial LAT} = - \frac{\partial \dot{x}_T}{\partial LAT} = -\omega \left(\frac{R_E}{C} + H \right) \sin(LAT) \sin(LON)$$

$$\frac{\partial \dot{x}_2}{\partial LAT} = - \frac{\partial \dot{y}_T}{\partial LAT} = \omega \left(\frac{R_E}{C} + H \right) \sin(LAT) \cos(LON)$$

$$\frac{\partial \dot{x}_3}{\partial LAT} = - \frac{\partial \dot{z}_T}{\partial LAT} = 0$$

$$\frac{\partial \dot{x}_1}{\partial \text{LON}} = - \frac{\partial \dot{x}_T}{\partial \text{LON}} = \omega \left(\frac{R_E}{C} + H \right) \cos(\text{LAT}) \cos(\text{LON})$$

$$\frac{\partial \dot{x}_2}{\partial \text{LON}} = - \frac{\partial \dot{y}_T}{\partial \text{LON}} = \omega \left(\frac{R_E}{C} + H \right) \cos(\text{LAT}) \sin(\text{LON})$$

$$\frac{\partial \dot{x}_3}{\partial \text{LON}} = - \frac{\partial \dot{z}_T}{\partial \text{LON}} = 0$$

$$\frac{\partial \dot{x}_1}{\partial \text{ALT}} = - \frac{\partial \dot{x}_T}{\partial \text{ALT}} = \omega \cos(\text{LAT}) \sin(\text{LON})$$

$$\frac{\partial \dot{x}_2}{\partial \text{ALT}} = - \frac{\partial \dot{y}_T}{\partial \text{ALT}} = -\omega \cos(\text{LAT}) \cos(\text{LON})$$

$$\frac{\partial \dot{x}_3}{\partial \text{ALT}} = - \frac{\partial \dot{z}_T}{\partial \text{ALT}} = 0$$

- A. The following is a derivation of the partials relating the types of measurements and the vehicle state. In the program, these partials are used as a row vector. The FORTRAN name of the vector is H. H may be written as follows:

$$H = \left(\frac{\partial \text{MEAS}}{\partial \dot{x}_v}; \frac{\partial \text{MEAS}}{\partial \dot{y}_v}; \frac{\partial \text{MEAS}}{\partial \dot{z}_v}; \frac{\partial \text{MEAS}}{\partial \dot{x}_T}; \frac{\partial \text{MEAS}}{\partial \dot{y}_T}; \frac{\partial \text{MEAS}}{\partial \dot{z}_T} \right)$$

1x6

1x6

- (1) Derivation of partials for range measurement

$$R = (\vec{X} \cdot \vec{X})^{1/2}$$

$$H_R = \left(\frac{\partial R}{\partial \dot{x}_v}; \frac{\partial R}{\partial \dot{x}_T} \right) = \left(\frac{x_1}{R}; \frac{x_2}{R}; \frac{x_3}{R}; 0; 0; 0 \right)$$

1x6

1x6

1x6

(2) Derivation of partials for range rate measurement.

$$\dot{R} = \frac{\vec{X} \cdot \dot{\vec{X}}}{R}$$

$$H_{RR} = \left(\frac{\partial \dot{R}}{\partial \dot{X}_V}; \frac{\partial \dot{R}}{\partial \dot{X}_V} \right) = \left(\frac{\dot{X}_1}{R} - \frac{\dot{R}}{R^2} (X_1); \frac{\dot{X}_2}{R} - \frac{\dot{R}}{R^2} (X_2); \frac{\dot{X}_3}{R} - \frac{\dot{R}}{R^2} (X_3); \frac{X_1}{R}; \frac{X_2}{R}; \frac{X_3}{R} \right)$$

(3) Derivation of partials for azimuth measurement.

$$AZ = \tan^{-1} \left(\frac{\vec{X} \cdot \hat{E}}{\vec{X} \cdot \hat{N}} \right) \equiv \tan^{-1} \gamma$$

$$\frac{\partial AZ}{\partial PAR} = [1 + \gamma^2]^{-1} \frac{\partial \gamma}{\partial PAR}$$

$$[1 + \gamma^2]^{-1} = \frac{(\vec{X} \cdot \hat{N})^2}{S^2} \quad S^2 = (\vec{X} \cdot \hat{E})^2 + (\vec{X} \cdot \hat{N})^2$$

$$H_{AZ} = \left(\frac{\partial AZ}{\partial \dot{X}_V}; \frac{\partial AZ}{\partial \dot{X}_V} \right) = \left(\frac{E_1(\hat{N} \cdot \vec{X})}{S^2} - \frac{\hat{E} \cdot \vec{X}(N_1)}{S^2}; \frac{E_2(\hat{N} \cdot \vec{X})}{S^2} - \frac{\hat{E} \cdot \vec{X}(N_2)}{S^2}; \frac{E_3(\hat{N} \cdot \vec{X})}{S^2} - \frac{\hat{E} \cdot \vec{X}(N_3)}{S^2}; 0; 0; 0 \right)$$

(4) Derivation of partials for elevation measurement.

$$EL = \sin^{-1} \left(\frac{\hat{U} \cdot \vec{X}}{R} \right) \equiv \sin^{-1} \gamma$$

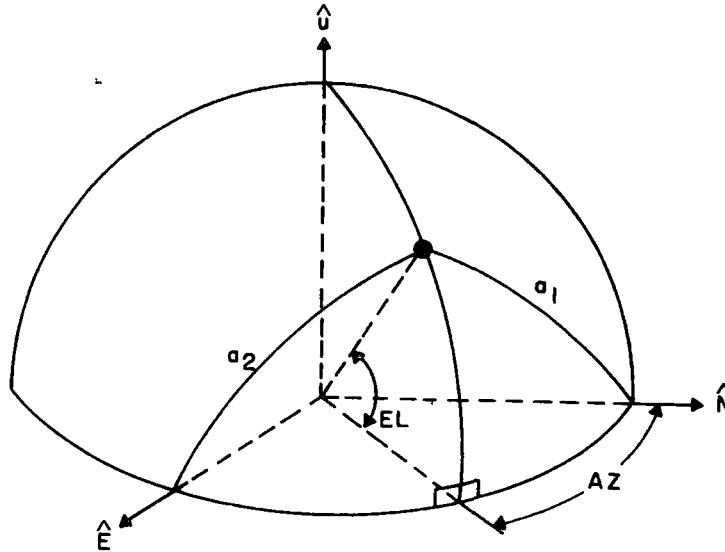
$$\frac{\partial EL}{\partial PAR} = [1 - \gamma^2]^{-1/2} \frac{\partial \gamma}{\partial PAR}$$

$$(1 - \gamma^2)^{-1/2} = \frac{R}{S}$$

$$H_{EL} = \left(\frac{\partial EL}{\partial \vec{X}} ; \frac{\partial EL}{\partial \vec{X}} \right) = \left(\frac{U_1}{S} - \frac{(\hat{U} \cdot \vec{X})}{R^2 S} x_1 ; \frac{U_2}{S} - \frac{(\hat{U} \cdot \vec{X})}{R^2 S} x_2 ; \right.$$

$$\left. \frac{U_3}{S} - \frac{(\hat{U} \cdot \vec{X})}{R^2 S} ; 0 ; 0 ; 0 \right)$$

- (5) Derivation of partials for direction cosines. The partials for the ℓ and m direction cosines are obtained by combining the azimuth and elevation partials as follows:



$$m = \cos(a_1) = \cos AZ \cos EL$$

$$\ell = \cos(a_2) = \sin AZ \cos EL$$

$$\frac{\partial m}{\partial PAR} = - \cos AZ \sin EL \frac{\partial EL}{\partial PAR} - \sin AZ \cos EL \frac{\partial AZ}{\partial PAR}$$

$$\frac{\partial \ell}{\partial PAR} = - \sin AZ \sin EL \frac{\partial EL}{\partial PAR} + \cos AZ \cos EL \frac{\partial AZ}{\partial PAR}$$

$$H_m = \begin{pmatrix} \frac{\partial m}{\partial X} & \frac{\partial m}{\partial Y} \end{pmatrix} = \begin{pmatrix} -\cos AZ & \sin EL & -\sin AZ & \cos EL \end{pmatrix} \begin{pmatrix} H_{AZ} \\ H_{EL} \end{pmatrix}$$

1x6 1x6 1x2 2x6

$$H_\ell = \begin{pmatrix} \frac{\partial \ell}{\partial X} & \frac{\partial \ell}{\partial Y} \end{pmatrix} = \begin{pmatrix} -\sin AZ & \sin EL & \cos AZ & \cos EL \end{pmatrix} \begin{pmatrix} H_{AZ} \\ H_{EL} \end{pmatrix}$$

1x6 1x6 1x2 2x6

- B. In order to include errors in the measurements being made due to station location errors and time bias, the partials of the measurements with respect to latitude, longitude, altitude, and time are required. In the program, the station location partials are used as a row vector with FORTRAN name SPART. SPART may be written as follows:

$$SPART = \left(\frac{\partial MEAS}{\partial LAT} ; \frac{\partial MEAS}{\partial LON} ; \frac{\partial MEAS}{\partial ALT} \right)$$

- (1) Derivations of range measurement error partials.

$$\frac{\partial R}{\partial LAT} = \sum_{i=1}^3 \frac{\partial R}{\partial X_i} \frac{\partial X_i}{\partial LAT}$$

$$\frac{\partial R}{\partial LAT} = \sum_{i=1}^3 H_R(1,i) DRT(i,1)$$

Similarly

$$\frac{\partial R}{\partial LON} = \sum_{i=1}^3 H_R(1,i) DRT(i,2)$$

$$\frac{\partial R}{\partial ALT} = \sum_{i=1}^3 H_R(1,i) DRT(1,3)$$

$$SPART_R = \left(\frac{\partial R}{\partial LAT}; \frac{\partial R}{\partial LON}; \frac{\partial R}{\partial ALT} \right)$$

(2) Derivation of range rate measurement error partials.

$$\frac{\partial \dot{R}}{\partial LAT} = \sum_{i=1}^3 \frac{\partial \dot{R}}{\partial X_i} \frac{\partial X_i}{\partial LAT} + \frac{\partial \dot{R}}{\partial \dot{X}_1} \frac{\partial \dot{X}_1}{\partial LAT}$$

$$\frac{\partial \dot{R}}{\partial LAT} = \sum_{i=1}^3 H_{RR}(1,i) DRT(1,1) + H_{RR}(1,i+3) \frac{\partial \dot{X}_1}{\partial LAT}$$

Similarly

$$\frac{\partial \dot{R}}{\partial LON} = \sum_{i=1}^3 H_{RR}(1,i) DRT(1,2) + H_{RR}(1,i+3) \frac{\partial \dot{X}_1}{\partial LON}$$

$$\frac{\partial \dot{R}}{\partial ALT} = \sum_{i=1}^3 H_{RR}(1,i) DRT(1,3) + H_{RR}(1,i+3) \frac{\partial \dot{X}_1}{\partial ALT}$$

$$SPART_{RR} = \left(\frac{\partial \dot{R}}{\partial LAT}; \frac{\partial \dot{R}}{\partial LON}; \frac{\partial \dot{R}}{\partial ALT} \right)$$

(3) Derivation of azimuth measurement error partials.

$$\frac{\partial AZ}{\partial LAT} = \sum_{i=1}^3 \frac{\partial AZ}{\partial X_i} \frac{\partial X_i}{\partial LAT} + \overset{(<0>)}{\cancel{\frac{\partial AZ}{\partial E_i} \frac{\partial E_i}{\partial LAT}}} + \frac{\partial AZ}{\partial N_1} \frac{\partial N_1}{\partial LAT}$$

$$\frac{\partial AZ}{\partial N_i} = - \frac{X_i (\vec{X} \cdot \hat{E})}{S^2} \quad i = 1, 2, 3$$

$$\frac{\partial AZ}{\partial LAT} = \sum_{i=1}^3 H_{AZ}(1,i) DRT(1,1) - \frac{X_i(\vec{X} \cdot \hat{E})}{S^2} \frac{\partial N_i}{\partial LAT}$$

$$\frac{\partial AZ}{\partial LON} = \sum_{i=1}^3 \frac{\partial AZ}{\partial X_i} \frac{\partial X_i}{\partial LON} + \frac{\partial AZ}{\partial E_i} \frac{\partial E_i}{\partial LON} + \frac{\partial AZ}{\partial N_i} \frac{\partial N_i}{\partial LON}$$

$$\frac{\partial AZ}{\partial E_i} = \frac{X_i(\vec{X} \cdot \hat{N})}{S^2} \quad i = 1, 2, 3$$

$$\frac{\partial AZ}{\partial LON} = \sum_{i=1}^3 H_{AZ}(1,i) DRT(1,2) + \frac{X_i}{S^2} (\vec{X} \cdot \hat{N}) \frac{\partial E_i}{\partial LON} - \frac{X_i}{S^2} (\vec{X} \cdot \hat{E}) \frac{\partial N_i}{\partial LON}$$

$$\frac{\partial AZ}{\partial ALT} = \sum_{i=1}^3 \frac{\partial AZ}{\partial X_i} \frac{\partial X_i}{\partial ALT} + \overset{=0}{\frac{\partial AZ}{\partial E_i} \frac{\partial E_i}{\partial ALT}} + \overset{=0}{\frac{\partial AZ}{\partial N_i} \frac{\partial N_i}{\partial ALT}}$$

$$\frac{\partial AZ}{\partial ALT} = \sum_{i=1}^3 H_{AZ}(1,i) DRT(1,3)$$

$$SPART_{AZ} = \left(\frac{\partial AZ}{\partial LAT} ; \frac{\partial AZ}{\partial LON} ; \frac{\partial AZ}{\partial ALT} \right)$$

(4) Derivation of elevation measurement error partials.

$$\frac{\partial EL}{\partial LAT} = \sum_{i=1}^3 \frac{\partial EL}{\partial X_i} \frac{\partial X_i}{\partial LAT} + \frac{\partial EL}{\partial U_i} \frac{\partial U_i}{\partial LAT}$$

$$\frac{\partial EL}{\partial U_i} = \frac{X_i}{S} \quad i = 1, 2, 3$$

$$\frac{\partial EL}{\partial LAT} = \sum_{i=1}^3 H_{EL}(1,i) DRT(i,1) + \frac{x_1}{s} \frac{\partial u_1}{\partial LAT}$$

$$\frac{\partial EL}{\partial LON} = \sum_{i=1}^3 \frac{\partial EL}{\partial x_i} \frac{\partial x_i}{\partial LON} + \frac{\partial EL}{\partial u_1} \frac{\partial u_1}{\partial LON}$$

$$\frac{\partial EL}{\partial LON} = \sum_{i=1}^3 H_{EL}(1,i) DRT(i,2) + \frac{x_1}{s} \frac{\partial u_1}{\partial LON}$$

$$\frac{\partial EL}{\partial ALT} = \sum_{i=1}^3 \frac{\partial EL}{\partial x_i} \frac{\partial x_i}{\partial ALT} + \frac{\partial EL}{\partial u_1} \frac{\partial u_1}{\partial ALT} \quad (=0)$$

$$\frac{\partial EL}{\partial ALT} = \sum_{i=1}^3 H_{ALT}(1,i) DRT(i,3)$$

$$SPART_{EL} = \left(\frac{\partial EL}{\partial LAT} ; \frac{\partial EL}{\partial LON} ; \frac{\partial EL}{\partial ALT} \right)$$

(5) Derivation of direction cosine measurement error partials.

$$\begin{array}{ccc} SPART_m & = & \begin{pmatrix} -\cos AZ \sin EL & -\sin AZ \cos EL \end{pmatrix} \begin{pmatrix} SPART_{AZ} \\ SPART_{EL} \end{pmatrix} \\ \begin{matrix} 1 \times 3 & & 1 \times 2 \end{matrix} & & \begin{matrix} 2 \times 3 \\ 2 \times 3 \end{matrix} \\ SPART_\ell & = & \begin{pmatrix} -\sin AZ \sin EL & \cos AZ \cos EL \end{pmatrix} \begin{pmatrix} SPART_{AZ} \\ SPART_{EL} \end{pmatrix} \\ \begin{matrix} 1 \times 3 & & 1 \times 2 \end{matrix} & & \begin{matrix} 2 \times 3 \\ 2 \times 3 \end{matrix} \end{array}$$

- (6) Derivations of time derivatives of measurement quantities to permit inclusion of time bias errors.

$$\frac{\partial R}{\partial t} = \dot{R} = \frac{\vec{X} \cdot \dot{\vec{X}}}{R}$$

$$\frac{\partial AZ}{\partial t} = \sum_{i=1}^3 \frac{\partial AZ}{\partial X_i} \frac{\partial X_i}{\partial t} + \frac{\partial AZ}{\partial E_i} \frac{\partial E_i}{\partial t} + \frac{\partial AZ}{\partial N_i} \frac{\partial N_i}{\partial t}$$

$$\frac{\partial AZ}{\partial t} = \sum_{i=1}^3 H_{AZ}(1,i) \dot{X}_i + \frac{\partial AZ}{\partial E_i} \dot{E}_i + \frac{\partial AZ}{\partial N_i} \dot{N}_i$$

$$\frac{\partial EL}{\partial t} = \sum_{i=1}^3 H_{EL}(1,i) \dot{X}_i + \frac{\partial EL}{\partial E_i} \dot{E}_i + \frac{\partial EL}{\partial N_i} \dot{N}_i$$

- (7) The time partials for the ℓ and m direction cosines are obtained by the following combination of azimuth and elevation partials.

$$\frac{\partial m}{\partial t} = \begin{pmatrix} -\cos AZ & \sin EL & -\sin AZ & \cos EL \end{pmatrix} \begin{pmatrix} \frac{\partial AZ}{\partial t} \\ \frac{\partial EL}{\partial t} \end{pmatrix}$$

1x1 1x2 2x1

$$\frac{\partial \ell}{\partial t} = \begin{pmatrix} -\sin AZ & \sin EL & \cos AZ & \cos EL \end{pmatrix} \begin{pmatrix} \frac{\partial AZ}{\partial t} \\ \frac{\partial EL}{\partial t} \end{pmatrix}$$

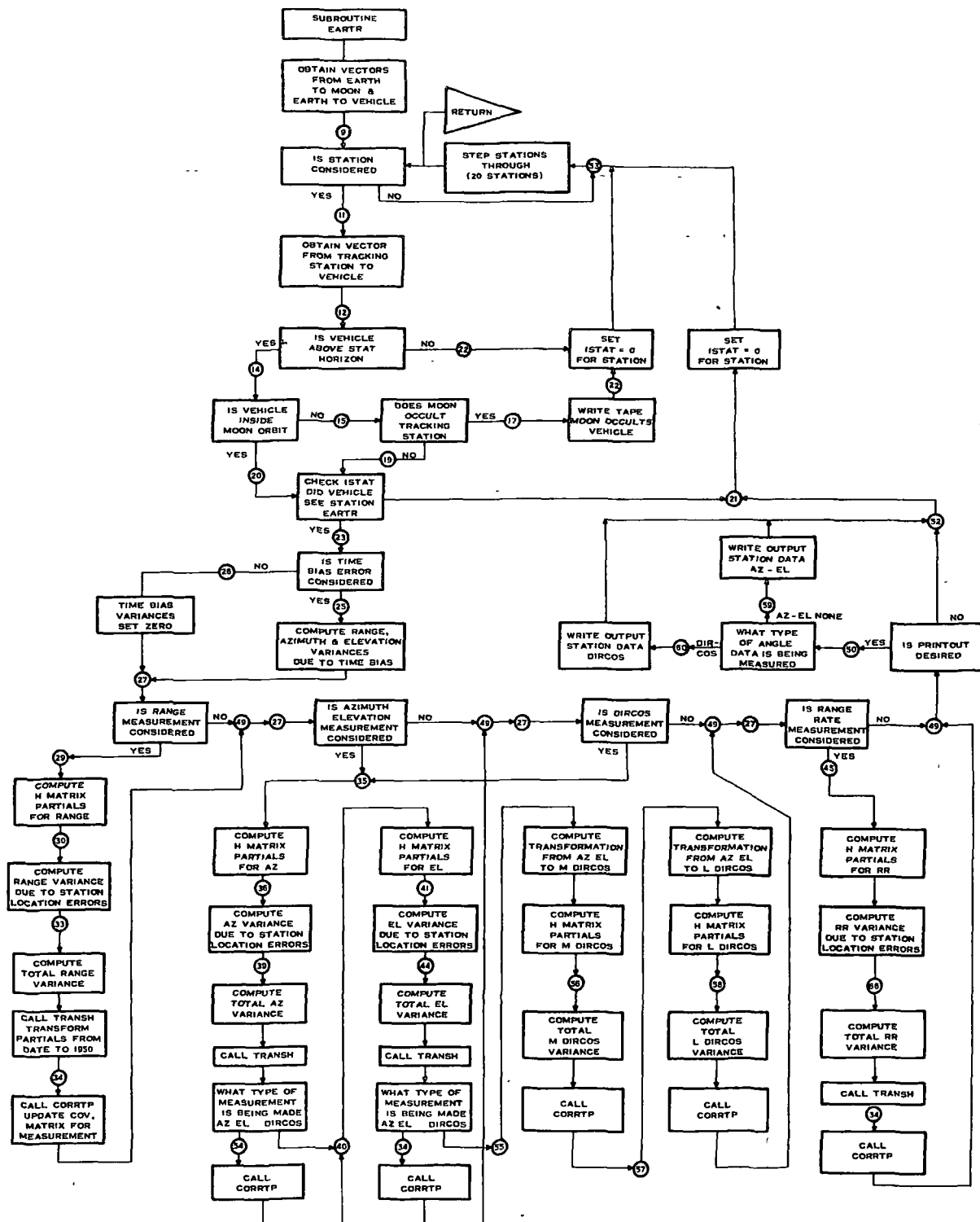
1x1 1x2 2x1

The errors in the measurements are computed in the following manner for station location errors and time bias.

$$\begin{array}{ccc}
 \text{QQS} & = & \left(\text{SPART}_{\text{MEAS}} \right)^2 \begin{pmatrix} \sigma^2_{\text{LAT}} \\ \sigma^2_{\text{LON}} \\ \sigma^2_{\text{ALT}} \end{pmatrix} & \text{Station Location Error} \\
 1 \times 1 & & 1 \times 3 & 3 \times 1
 \end{array}$$

$$\text{QQDOT} = \left\{ \frac{\partial \text{MEAS}}{\partial t} \cdot \sigma_{\text{TIME}} \right\}^2 \quad \text{Time Bias Error}$$

The computation of the H matrices and the measurement errors are the primary computations in EARTR. These quantities are input to subroutine CORRTP which does the weighting of the measurement and updating of the state covariance matrix.



EARTR

<pre> * LABEL * SYMBOL TABLE SUBROUTINE EARTR C SUBROUTINE EARTR UPDATES THE COVARIANCE MATRIX USED C IN EARTH TRACKING COMMON T,S,C,IC DIMENSION PO(22),VE(22),XED(3),VED(3),AN(3,3),RBOP(6),POSM(3), 1VOSM(3),POVRM(3),EM(3,3),EN(3),U(3),E(3),RT(3),Y(3),TD(3), 2ISTAT(20),H(6),X(3),VX(3),T(1360),S(1000),C(1000),IC(1),ISA(20), 3IMSTA(4,20),P(6,6),SPART(3),DRT(3,3),XD(3),SPART2(3),HA(6),HCOS(6) EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM) 1,(IC(3),NOR),(C(13),TW),(C(14),TF),(C(62),PO),(C(84),VE) 2,(C(112),RBOP),(C(138),AN),(C(120),EM),(C(15),X),(C(18),VX), 3(S(70),DTS),(S(71),STD),(S(72),DR),(S(73),RD),(IC(194),ISTAT) 4,(IC(10),ISA),(IC(30),IMSTA),(IC(214),NOUT),(C(652),P) 5,(C(649),TSECP),(C(30),TSEC),(S(10),W),(S(14),A),(S(15),B) CALL SETN(NIN,NUTS) NB=NOR-1 DIS=1.E10 CALL INTR1 (TW,TF,NB,PO,1,VE,DIS) CALL MATRX(AN,X,XED,3,3,1,0) CALL MATRX(AN,VX,VED,3,3,1,0) C XED=VECTOR FROM NB BODY TO VEHICLE, VED=VELOCITY EQUATOR OF DATE MS=1 IF(RBOP(1)-330000.)10,2,2 C RBOP= MAGNITUDE OF VECTOR FROM VEHICLE TO BODY 2 CONTINUE IF (NOR-1)3,5,3 3 CONTINUE C HERE IF OUTSIDE MOON AND NOT EARTH REFERENCED DO 4 I=1,3 POSM(I)=0. VOSM(I)=0. DO 4 J=1,3 K=23-J XED(I)=XED(I)-AN(I,J)*PO(K) VED(I)=VED(I)-AN(I,J)*VE(K) L=20-J POSM(I)=POSM(I)+AN(I,J)*(PO(L)-PO(K)) VOSM(I)=VOSM(I)+AN(I,J)*(VE(L)-VE(K)) C POSM IS A VECTOR FROM EARTH TO MOON 4 CONTINUE GO TO 7 5 CONTINUE C HERE IF OUTSIDE MOON AND EARTH REFERENCED DO 6 I=1,3 POSM(I)=0 VOSM(I)=0 DO 6 J=1,3 K=20-J POSM(I)=POSM(I)+AN(I,J)*PO(K) </pre>	<pre> EART EART EART0000 EART0005 EART0007 EART0010 EART0020 EART0030 EART0040 EART0050 EART0060 EART0070 EART0080 EART0090 EART0100 EART0110 EART0115 EART0120 EART0130 EART0140 EART0150 EART0160 EART0170 EART0180 EART0190 EART0200 EART0210 EART0220 EART0230 EART0240 EART0250 EART0260 EART0270 EART0280 EART0290 EART0300 EART0310 EART0320 EART0330 EART0340 EART0350 EART0360 EART0370 EART0380 EART0390 EART0400 EART0410 EART0420 EART0430 EART0440 EART0450 </pre>
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EARTR (Cont'd)

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VOSM(I)=VOSM(I)+AN(I,J)*VE(K)
6 CONTINUE
7 CONTINUE
  MS=2
  DO 8 I=1,3
    POVRM(I)=XED(I)-POSM(I)
8 CONTINUE
  RADM=FNORM(POVRM)
  DO 9 I=1,3
    POVRM(I)=POVRM(I)/RADM
9 CONTINUE
10 CONTINUE
  TIME=TW+TF
  CALL NUTAIT (TIME,OM,CR,DT,EM,ERSIL)
  FSEC=DTS+TF
  CALL GHA(FSEC,TW,GH,EM(2,1),OMEGA)
  GH=GH+DR
  NDUM=783
  NN=110
  DO 53 III=1,20
    NDUM=NDUM+5
    NN=NN+15
    IF(ISA(III)) 53,53,11
11 CONTINUE
  AT=S(NN+9)*DR
  ON=S(NN+10)*DR
  AL=S(NN+11)
  SNAME=S(NN+12)
  CALL TRAC(ON,AT,AL,GH,U,E,EN,RT,AC,SL,CL,ST,CT,A,B)
  TRAC  OBTAINS UNIT VECTORS UP,EAST AND NORTH, RT= VECTOR
  TO TRACK STATION
  DO 12 J=1,3
    Y(J)=XED(J)-RT(J)
    Y=VECTOR FROM TRACK STATION TO VEHICLE, TD=UNIT VECTOR IN
    DIRECTION OF Y
12 CONTINUE
  RAT=FNORM(Y)
  DO 13 J=1,3
    TD(J)=Y(J)/RAT
13 CONTINUE
  CE=DOT( U,TD)
  DOT FORMS A DOT PRODUCT OF ELEMENTS IN PARENTHESES
  SEC=CE/SQRTF(1.-CE**2)
  ELEV=ATANF(SEC)
  HORCOR=S(NDUM)
  S(NDUM) CONTAINS HORIZON CORRECTION FOR STATION
  IF(ELEV-HORCOR)22,14,14
14 CONTINUE
  HERE IF VEHICLE IS ABOVE STATION HORIZON
  GO TO (20,15),MS
15 CONTINUE

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EARTR (Cont'd)

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C      TO DETERMINE IF MOON OCCULTS VEHICLE
      DOTTD=DOT(POVRM,TD)
      IF(DOTTD)19,19,16
16     CONTINUE
      IF(DOTTD=(SQRTF(RADM**2-1739.**2))/RADM)19,19,17
17     WRITE OUTPUT TAPE (NUTS,18,SNAME
18     FORMAT (27H0MOON OCCULTS VEHICLE FROM,A6,8H TRACKER)
      GO TO 22
19     CONTINUE
20     CONTINUE
      SEC=DOT(TD,EN)
      CE=DOT(TD,E)
      AZMTH =ARKTNS(360,SEC,CE)
      IF(ISTAT(III))21,21,23
C      ISTAT IS SET ONE IF THE STATION SAW VEHICLE ON PREVIOUS TIME.
C      THROUGH MATSUB
C      ZERO IF IT COULD NOT SEE IT
21     CONTINUE
C      HERE IF STATION SEES THE VEHICLE.
      ISTAT(III)=1
      GO TO 53
22     CONTINUE
      ISTAT(III)=0
C      VEHICLE WAS NOT OBSERVED BY STATION
      GO TO 53
23     CONTINUE
      OBNO=INTF((TSEC-TSECP)/S(NN+13))
C      OBNO IS THE NUMBER OF OBSERVATIONS SINCE LAST TIME IN MATSUB
      XTU=DOT(Y,U)
      XTE=DOT(Y,E)
      XTN=DOT(Y,EN)
      TPD2=XTE**2+XTN**2
      TPD=SQRTF(TPD2)
      ALLY=XTN/TPD2
      GAM=XTU*XTE
      BET=XTE/TPD2
      DEL=XTU*XTN
      D=1./RAT**2/TPD
      CA=AC/A
      BA=B*B/(A*A)
      GG=CA*(1.-BA)*SL*CL*CA*CA
      DRT(1,1)=A*GG*U(1)+(AC+AL)*EN(1)
      DRT(2,1)=A*GG*U(2)+(AC+AL)*EN(2)
      DRT(3,1)=(B*B/A)*GG*U(3)+BA*(AC+AL)*EN(3)
      DRT(1,2)=(AC+AL)*CL*E(1)
      DRT(2,2)=(AC+AL)*CL*E(2)
      DRT(3,2)=0.0
      DO 24 I=1,3
      DRT(I,3)=U(I)
C      THE ABOVE QUATITIES ARE USED ONLY FOR H MATRIX CALCULATIONS
24     CONTINUE

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 EART141

EARTR (Cont'd)

```

AA=S(10)*CL*(AC+AL)
XD(1)=VED(1)-AA*E(1)
XD(2)=VED(2)-AA*E(2)
XD(3)=VED(3)
XDTU=DOT(XD,U)
XDTE=DOT(XD,E)
XDTN=DOT(XD,EN)
RDOT=DOT(XD,Y)/RAT
RDOT=RANGE RATE
ADOT=W*SL-W*CL*ALLY*XTU+ALLY*XDTE-BET*XDTN
ADOT=AZIMUTH RATE
EDOT=(1./TPD)*(W*CL*XTE+XDTU-RDOT*XTU/RAT)
EDOT=ELEVATION RATE
IF(S(NN+14))26,26,25
25 CONTINUE
RDOT2=RDOT*RDOT
QQRDOT=RDOT2*S(NN+14)
QQRDOT=RANGE VARIANCE DUE TO TIME BIAS
ADOT2=ADOT*ADOT
QQADOT=ADOT2*S(NN+14)
QQADOT=AZIMUTH VARIANCE DUE TO TIME BIAS
EDOT2=EDOT*EDOT
QQEDOT=EDOT2*S(NN+14)
QQEDOT=ELEVATION VARIANCE DUE TO TIME BIAS
GO TO 27
26 CONTINUE
QQRDOT=0.
QQADOT=0.
QQEDOT=0.
27 CONTINUE
DO 49 II=1,4
IF (IMSTA(II,III)) 49,49,28
28 CONTINUE
II=II
GO TO (29,35,35,45),II
II DESIGNATES TYPE OF MEASUREMENT 1=RANGE 2=AZ+EL 3=DIRCOS
4=RANGE RATE
29 CONTINUE
CALCULATES H MATRIX FOR RANGE
DO 30 J=1,3
H(J)=TD(J)
30 CONTINUE
DO 32 I=1,3
SPART(I)=0.
SPART=PARTIALS OF RANGE WRT STATION LOCATION
DO 31 K=1,3
SPART(I)=SPART(I)+H(K)*DRT(K,I)
31 CONTINUE
SPART2(I)=SPART(I)*SPART(I)
32 CONTINUE
QQS=0.

```

EART142
EART143
EART144
EART145
EART146
EART147
EART148
EART149
EART150
EART151
EART152
EART153
EART154
EART155
EART156
EART157
EART158
EART159
EART160
EART161
EART162
EART163
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EART166
EART167
EART168
EART169
EART170
EART171
EART172
EART173
EART174
EART175
EART176
EART176
EART176
EART177
EART178
EART179
EART180
EART181
EART182
EART183
EART184
EART185
EART186
EART187
EART188
EART189
EART190

EARTR (Cont'd)

```

      DO 33 I=1,3
C     QQS=RANGE VARIANCE DUE TO STATION LOCATION ERRORS
      KL=NN+3+I
      QQS=QQS+SPART2(I)*S(KL)
33  CONTINUE
      QQ=S(NN)/OBNO+RAT*S(425)*RAT+QQS+QQRDOT
C     QQ=TOTAL RANGE VARIANCE
      CALL TRANSH(H,1)
C     TRANSH TRANSFORMS H MATRIX FROM EQUINOX OF DATE TO 1950
34  CONTINUE
      CALL CORRTP (QQ,H,P)
C     CORRTP UPDATES COVARIANCE MATRIX FOR PARTICULAR TYPE
C     OF MEASUREMENT
      GO TO 49
35  CONTINUE
C     THE FOLLOWING CALCULATIONS GIVE H MATRIX FOR AZIMUTH
      DO 36 J=1,3
      HA(J)=ALLY*E(J)=BET*EN(J)
36  CONTINUE
      DO 37 I=1,3
      SPART(I)=0.
C     SPART=PARTIALS OF AZIMUTH WRT STATION LOCATION
      DO 37 K=1,3
      SPART(I)=SPART(I)-HA(K)*DRT(K,I)
37  CONTINUE
      SPART(1)=SPART(1)+BET*XTU
      PLUS=BET*SL*XTE=ALLY*(Y(1)*CT+Y(2)*ST)
      SPART(2)=SPART(2)+PLUS
      DO 38 I=1,3
      SPART2(I)=SPART(I)*SPART(I)
38  CONTINUE
      QQSA=0.
      DO 39 I=1,3
C     QQSA=AZIMUTH VARIANCE DUE TO STATION LOCATION ERRORS
      KL=NN+3+I
      QQSA=QQSA+SPART2(I)*S(KL)
39  CONTINUE
      QQ=S(NN+1)/OBNO+S(NN+7)+QQSA+QQADOT
C     QQ=TOTAL AZIMUTH VARIANCE
      CALL TRANSH(HA,1)
      IF(II=2)54,54,40
54  CONTINUE
      CALL CORRTP(QQ,HA,P)
40  CONTINUE
C     THE FOLLOWING CALCULATIONS GIVE H MATRIX FOR ELEVATION
      DO 41 J=1,3
      H(J)= U(J)/TPD=Y(J)*XTU*D
41  CONTINUE
      DO 42 I=1,3
      SPART(I)=0.
C     SPART=PARTIALS OF ELEVATION WRT STATION LOCATION

```

EART1910
 EART1920
 EART1930
 EART1940
 EART1950
 EART1960
 EART1970
 EART1980
 EART1990
 EART2000
 EART2010
 EART2015
 EART2016
 EART2020
 EART2030
 EART2040
 EART2050
 EART2060
 EART2070
 EART2080
 EART2090
 EART2100
 EART2110
 EART2120
 EART2130
 EART2140
 EART2150
 EART2160
 EART2170
 EART2180
 EART2190
 EART2200
 EART2210
 EART2220
 EART2230
 EART2240
 EART2250
 EART2260
 EART2270
 EART2280
 EART2290
 EART2300
 EART2310
 EART2320
 EART2330
 EART2340
 EART2350
 EART2360
 EART2370
 EART2380
 EART2390

EARTR (Cont'd)

DO 42 K=1,3	EART240
SPART(I)=SPART(I)-H(K)*DRT(K,I)	EART241
42 CONTINUE	EART242
SPART(1)=SPART(1)+XTN/TPD	EART243
SPART(2)=SPART(2)+XTE*CL/TPD	EART244
DO 43 I=1,3	EART245
SPART2(I)=SPART(I)*SPART(I)	EART246
43 CONTINUE	EART247
QQS=0.	EART248
DO 44 I=1,3	EART249
QQS=ELEVATION VARIANCE DUE TO STATION LOCATION ERRORS	EART250
KL=NN+3+I	EART251
QQS=QQS+SPART2(I)*S(KL)	EART252
44 CONTINUE	EART253
QQ=S(NN+2)/OBNO+S(NN+8)*QQS+QQEDOT	EART254
QQ=TOTAL ELEVATION VARIANCE	EART255
CALL TRANSH(H,1)	EART256
IF(II=2)34,34,55	EART257
55 CONTINUE	EART258
DIRCOS=DOT(EN,TD)	EART259
SINANG=SQRTF(1.-DIRCOS**2)	EART260
TANANG=SINANG/DIRCOS	EART261
ANGM=ATANF(TANANG)	EART262
ANGM=ANGM*RD	EART263
CA=COSF(AZMTH)	EART264
SA=SINF(AZMTH)	EART265
SE=SINF(ELEV)	EART266
CE=COSF(ELEV)	EART267
C1=-SA*CE	EART268
C2=-CA*SE	EART269
ANGMDT=C1*EDOT+C2*ADOT	EART270
ANGMDT=ANGMDT*RD	EART271
DO 56 I=1,3	EART272
HCOS(I)=C1*H(I)+C2*HA(I)	EART273
56 CONTINUE	EART274
QQSCOS=C1*QQS+C2*QQSA	EART275
QQSCOS IS THE VARIANCE IN THE M DIRECTION COSINE DUE TO STATION	EART276
LOCATION ERRORS	EART277
QQCDOT=C1*QQEDOT+C2*QQADOT	EART278
QQ=S(NDUM+1)/OBNO+S(NDUM+2)+QQSCOS+QQCDOT	EART279
QQ=TOTAL VARIANCE OF M DIRECTION COSINE	EART280
CALL CORRTP(QQ,HCOS,P)	EART281
57 CONTINUE	EART282
DIRCOS=DOT(E,TD)	EART283
SINANG=SQRTF(1.-DIRCOS**2)	EART284
TANANG=SINANG/DIRCOS	EART285
ANGL=ATANF(TANANG)	EART286
ANGL=ANGL*RD	EART287
C1=CA*CE	EART288
C2=-SA*SE	EART289
ANGLDT=C1*EDOT+C2*ADOT	EART290

EARTR (Cont'd)

```

      ANGLDT=ANGLDT*RD
      DO 58 I=1,3
      HCOS(I)=C1*H(I)+C2*HA(I)
58  CONTINUE
      QQSCOS=C1*QQS+C2*QQSA
C    QQSCOS IS THE L DIRECTION COSINE ERROR DUE TO STATION LOCATION
C    ERROR
      QQCDOT=C1*QQEDOT+C2*QQADOT
      QQ=S(NDUM+3)/OBNO+S(NDUM+4)*QQSCOS+QQODOT
C    QQ=TOTAL L DIRECTION COSINE VARIANCE
      CALL CORRTP(QQ,HCOS,P)
      GO TO 49
45  CONTINUE
C    THE FOLLOWING CALCULATIONS GIVE H MATRIX FOR RANGE RATE
47  DO 48 J=1,3
      K=J+3
      H(K)=TD(J)
      H(J)=(1./RAT)*(XD(J)-RDOT*TD(J))
48  CONTINUE
      CNST=B*B/A+((1./CA)**3)
      DO 65 JJ=1,3
      JJ=3*J-2
      SPART(J)=-DOT(H,DRT(JJ))
65  CONTINUE
      SPART(1)=SPART(1)*S(10)*U(3)*(CNST+AL)*XTE/RAT
      SPART(2)=SPART(2)-AA*(TD(2)*E(1)-TD(1)*E(2))
      SPART(3)=SPART(3)-S(10)*EN(3)*XTE/RAT
      QQS=0.
      DO 66 I=1,3
      KL=NN+3*I
      QQS=QQS+(SPART(I)**2)*S(KL)
66  CONTINUE
      QQ=S(NN+3)/OBNO+QQS
      CALL TRANSH(H,2)
      GO TO 34
49  CONTINUE
      NOUT=NOUT
      GO TO (52,50),NOUT
50  CONTINUE
      IF(IMSTA(3,III))59,59,60
59  CONTINUE
      EDOT=EDOT*RD
      ADOT=ADOT*RD
      AZMTH =AZMTH*RD
      ELEV=ELEV*RD
      WRITE OUTPUT TAPE NUTS,51,SNAME,RAT,RDOT,AZMTH,ADOT,ELEV,EDOT
51  FORMAT (17H TRACKER STATION ,A6, /4H RNGE15.8,5H RGRE15.8,
15H AZME15.8,5H AZRE15.8,5H ELEE15.8,5H ELRE15.8)
      GO TO 52
60  CONTINUE
      WRITE OUTPUT TAPE NUTS,61,SNAME,RAT,RDOT,ANGL,ANGLDT,ANGM,ANGMDT

```

```

EART2910
EART2920
EART2930
EART2940
EART2950
EART2960
EART2970
EART2980
EART2990
EART3000
EART3010
EART3020
EART3030
EART3040
EART3050
EART3060
EART3070
EART3080
EART3090
EART3091
EART3092
EART3093
EART3094
EART3095
EART3096
EART3097
EART3098
EART3099
EART3100
EART3101
EART3102
EART3103
EART3104
EART3110
EART3120
EART3130
EART3140
EART3150
EART3160
EART3170
EART3180
EART3190
EART3200
EART3210
EART3220
EART3230
EART3240
EART3250
EART3260
EART3270
EART3280

```

EARTR (Cont'd)

61 FORMAT (17H TRACKER STATION ,A6,/4H RNGE15.8,5H RGRE15.8,
15H LCSE15.8,5H LCRE15.8,5H MCSE15.8,5H MCRE15.8)
52 CONTINUE
GO TO 21
53 CONTINUE
RETURN
END

EART32
EART33
EART33
EART33
EART33
EART33
EART33
EART

S-143

EARTR-

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Subroutine: ECLIP

Purpose: To replace each of two 3-dimensional vectors by its product with a given 3 x 3 matrix. This subroutine is used for transforming position and velocity vectors.

Calling Sequence:

CALL ECLIP (X, VX, ECL)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I-O	X	3			$X_{out} = (ECL) X_{in}$
I-O	VX	3			$VX_{out} = (ECL) VX_{in}$
I	ECL	3,3			TRANSFORMATION MATRIX

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

ECLIP

WDL-TR2184

```
* LABEL
* SYMBOL TABLE
SUBROUTINE ECLIP(X,VX,ECL)
  DIMENSION X(3),VX(3),XP(3),VXP(3),ECL(3,3)
  DO 1 I=1,3
    XP(I) = 0.
    VXP(I) = 0.
  DO 1 J=1,3
    XP(I) = XP(I) + ECL(I,J)*X(J)
1 VXP(I) = VXP(I) + ECL(I,J)*VX(J)
  DO 2 I=1,3
    X(I) = XP(I)
2 VX(I) = VXP(I)
  RETURN
END
```

ECLP
ECLP
ECLP0000
ECLP0010
ECLP0020
ECLP0030
ECLP0040
ECLP0050
ECLP0060
ECLP0070
ECLP0080
ECLP0090
ECLP0100
ECLP0110
ECLP

ECLIP - 2

Subroutine: ENCKE

Purpose: To perform the calculation of the ENCKE contribution to the acceleration. These are perturbations in acceleration due to deviation from the osculating conic.

Calling Sequence:

CALL ENCKE (U, X, D, AE)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	U	1	μ	Km^3/sec^2	Gravitational constant
I	X	3	X, Y, Z	Km	Position on the conic
I	D	3	X', Y', Z'	Km	Position deviation from the conic
O	AE	3		Km/sec^2	ENCKE acceleration terms

Common storages used or required:

None

Subroutines required:

None

Functions required:

SQRT, DOT

Approximate number of storages required:

158 DEC

Equation Being Solved

The perturbation acceleration due to deviation from the reference conic is the following

$$\vec{AE} = \frac{\mu}{R_o^3} (\vec{R} F(Q) - \vec{D})$$

where $\vec{R} = \vec{R}_o + \vec{D}$. The solution, R_o , for the position in the two body orbit is provided by STEPC, and is saved from step to step so that a new R_o is calculated only when the time has changed.

$F(Q) = 1 - (1 + 2Q)^{-3/2}$ is calculated from the series expansion

$$F(Q) = Q \sum_{j=0}^6 a_j Q^j$$

where

$$a_0 = 3$$

$$a_1 = -7.5$$

$$a_2 = 17.5$$

$$a_3 = 39.375$$

$$a_4 = 86.625$$

$$a_5 = 187.6875$$

$$a_6 = 402.1875$$

and

$$Q = \frac{\vec{D} \cdot \left(\vec{R}_o + \frac{\vec{D}}{2} \right)}{R_o^2}$$

ENCKE

```

* LABEL
* SYMBOL TABLE
CEC2014 SUBROUTINE ENCKE
  SUBROUTINE ENCKE (U,X,D,AE)
    DIMENSION X(3),D(3),AE(3)
    R = DOT(X,X)
    DD = DOT(D,D)
    RD = DOT(X,D)
    Q = (RD+.5*DD)/R
    F = 1./SQRTF(2.*Q+1.)**3
    2 A = Q*(3.+Q*(-7.5+Q*(17.5+Q*(-39.375+Q*(86.625+Q*(-187.6875+Q*
    1402.1875))))))
    4 R3 = (SQRTF(R))*R
    UA = U*A/R3
    UF = U*F/R3
    DO 5 I=1,3
    5 AE(I) = UA*X(I)-UF*D(I)
    RETURN
  END

```

```

ENCK
ENCK
ENCK
ENCK000
ENCK000
ENCK000
ENCK000
ENCK000
ENCK000
ENCK011
ENCK011
ENCK011
ENCK011
ENCK011
ENCK011
ENCK011
ENCK011
ENCK011
ENCK011
ENCK

```

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Subroutine: ERP

Purpose: To write on the output tape: EPHEMERIS FAILED DUE TO TAPE REDUNDANCIES, and then to CALL EXIT. Should this message occur, and the tape was actually mounted on the correct unit, try again or try a different copy of the ephemeris tape.

Calling Sequence:

CALL ERP

Input and Output

Common storages used or required:	None
Subroutines required:	SETN, EXIT
Functions required:	
Approximate number of storages required:	

ERP

WDL-TR2184

```
* LABEL
CEC20GD
  SUBROUTINE ERP
  CALL SETN(NIN,NOUT)
  1  FORMAT(42H EPHEMERIS FAILED DUE TO TAPE REDUNDANCIES)
  WRITE OUTPUT TAPE NOUT,1
  CALL EXIT
  RETURN
  END
```

ERPO
ERPO
ERP0000
ERP0010
ERP0020
ERP0030
ERP0040
ERP0050
ERPO

S-152

ERP-2

Subroutine: ERPT

Purpose: To write on the output tape: EPHEMERIS FAILED LOOKING
FOR T = () DAYS SINCE 1950.0, and to call EXIT.

The cause of this condition is either incorrect input or not having the ephemeris tape mounted correctly.

Calling Sequence:

CALL ERPT(T)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	T			days	Time (in days since 1950.0)
					for which INTR was searching
					the tape

Common storages used or required:

None

Subroutines required:

SETN, EXIT

Functions required:

None

Approximate number of storages required:

ERPT

WDL-TR2184

```
*      LABEL
CEC20GE
      SUBROUTINE ERPT(T)
      CALL SETN(NIN,NOUT)
      WRITE OUTPUT TAPE NOUT,2,T
2      FORMAT(33H EPHEMERIS FAILED LOOKING FOR T =,F20.0,
118H DAYS SINCE 1950,0)
      CALL EXIT
      RETURN
      END
```

```
ERPT
ERPT
ERPT0000
ERPT0010
ERPT0020
ERPT0030
ERPT0040
ERPT0050
ERPT0060
ERPT
```

ERPT-2

S-154

Subroutine: FINP

Identification

RW FINP - Decimal, Octal, BCD, Variable Data Input
7090 FAP Subroutine
W.J. Stoner, August 24, 1961
Aerospace Corporation

Purpose

To read a set of Hollerith punched data and/or header cards into core with one FORTRAN CALL statement.

To convert the data fields to binary and store in core according to their associated conversion codes.

Restrictions

This routine uses (CSH)S to accomplish the BCD card image read. Tape troubles or other errors from this routine are indicated by the printout of HPR 1,4.

This routine uses (EXE) to print HPR 2,4 in case of errors such as non-Hollerith characters, data out of range, illegal format, subscripts too large for the array previously defined, etc. Upon detection of any error, control is immediately sent to (EXE) and no more cards are processed.

Method

Decimal numbers are converted to binary integers and then scaled to the indicated power of ten.

Octal numbers are converted to binary integers.

Hollerith words are stored directly.

Range: Decimal to floating binary conversion 10^{-38}
 Decimal to fixed binary; 1 to 9 digits*
 Decimal integer to binary integer; 1 to 5 digits
 Octal integer to binary integer; 0 to 235 - 1

*the magnitude of the number depends upon the location of the decimal point.

Usage

Format:

1. The data card format, available on keypunch form M-1, consists of four subfields containing the conversion code, location, number, and exponent, respectively.

FINP-1

	Data Field	Data Field	Data Field	Data Field
Subfield	1	2	3	4
Conversion Code	1	19	37	55
Location	2-6	20-24	38-42	56-60
Value	7-16	25-34	43-52	61-70
Exponent	17-18	35-36	53-54	71-72

where conversion code is one of the alphabetic characters defined below which specifies the type of conversion to be used on the value field, the location specifies the cell into which the converted value field is to be stored, the value subfield contains the data to be converted, and the exponent contains the power of ten by which floating data is to be scaled, or the location of the binary point of fixed point data.

2. The header card format consists of a conversion code in column 1, a sequence number in columns 2-6, and any Hollerith information in columns 7-72.

Decimal Points:

Decimal points may be placed anywhere in the value field except that they may not occur in the same column as a minus sign (11 punch) since this results in a non-Hollerith character. If the decimal point would normally appear at the right of the number punched in the value field, then it is optional.

Minus Signs:

Minus signs are 11 punches over any digit of the field. If all of the available columns of the field are not used, minus signs may be punched as the left character of the field.

Values:

Values must always be written to the extreme left of a field. It is not necessary that the entire field be filled as the first blank denotes the end of value. Superfluous low order zeros should be omitted as they increase conversion error.

The only exception to partial fields is BCK data where the entire field, including blanks, is stored.

Location:

The location may be specified by either absolute octal, a variable or array name, or the element subscripts in a one or two dimensional array. If the locations contain five digits, it is interpreted as octal. All five columns must be punched for octal locations.

If the location contains at least one non-numeric character, it is interpreted as a variable or array name which must appear exactly as given in the CALL statement (see Calling Sequence below). The contents of the number and exponent fields, if they are numeric data, are stored in the cell for the variable or the first cell for the array. This location then becomes the origin for all subscript locations following until another variable or array name is encountered. Caution must be taken to load an array name prior to subscript locations.

If the location contains four or fewer digits, it is interpreted as a subscript except for conversion code H explained below. Single dimension array subscripts must be left-justified with leading zeros optional. Two dimension array subscripts must be denoted by two subfields of two columns each containing i and j, respectively. The i and j subfields must be separated by a comma and must contain two-digit integers.

If the location is left blank, then the location counter within the routine is decreased by 1 and the associated number is stored in the cell immediately preceding the cell where the last number was stored. Thus, an entire array may be read in by specifying the initial location only.

Conversion Codes:

Blank: Floating decimal

The number in the value field times the power of ten in the exponent field is converted to floating binary. Checks are made for overflow and format errors.

F: Fixed decimal

The number in the value field is converted to fixed point binary and stored with the binary point located at the position specified by the number in the exponent field. An overflow error check is made.

I: Decimal integer

The number in the value field is converted to a fixed point binary integer with the binary point following position 17. The exponent field is ignored. A decimal point is considered an error.

B: Octal

The value plus exponent fields are converted as a logical octal word. It is not necessary to include leading zeros but the first octal digit must always occupy the leftmost position of the field.

D: BCI Data

The contents of the value plus exponent fields are interpreted as two BCI words and stored in two consecutive cells in descending order beginning at the location specified by the location field.

H: Heading Card

A card with an H in column 1 is considered a BCI heading card. If the location field is blank, the card is ignored. If the location field contains a left-justified one to four digit positive decimal integer V (octal, negative, or variable locations are not permitted), columns 7-72 of the card are stored directly in 11 consecutive words in descending order. The location of the first of these words is calculated by the routine as $HEAD + 11 * (V - 1)$ where HEAD is defined as the last variable or array named in the CALL statement. Each card may be used as one record of output using FORMAT option A with column 7 of the card providing the code for printer spacing on output.

A: Variable names as data

The value plus exponent fields are interpreted in a pseudo FAP instruction format AAAAA T DDDDD P where the fields to replace are address, tag, decrement, and prefix, respectively. The address and decrement fields are defined normally to be 5 characters and the tag and prefix as one octal numeric character each. Any field containing less than the normal number of characters must end with a comma while fields of normal length must not. Any address or decrement field containing less than 5 numeric characters are converted as octal. Any address or decrement field containing at least one non-numeric character is interpreted as a variable or array name. Variable addresses cause the entire word from the compiler generated calling sequence to be loaded into the location word (i.e., the TSX X is stored in the location specified if X is the variable appearing in the address field). Variable decrements cause the right-most 18 bits from the compiler generated calling sequence to be loaded into the location word's prefix and decrement. Numeric tags and prefixes are loaded directly into the corresponding parts of the location words. Null fields are not loaded. Since the first blank indicates the end of the loading of a word, address only, address-tag, address-tag-decrement, or entire word may be loaded as desired.

G: Temporary Origin

The value in the first location field on the card is used as a temporary origin for tables. The location is saved and if data cards follow with blank location fields the corresponding data is stored consecutively in descending order beginning with the cell specified in the location in the G card. Columns 7-72 are ignored and may be used to identify the table.

The first nonblank location starts a new origin. If this nonblank location is a subscript, it references the last variable or array named, which may or may not have been on the G card.

J: Transfer

The location specified with this prefix must be an octal address and is the only part of the data field that is interpreted. The subroutine causes a transfer to the octal location specified and does not interpret the remaining fields on the card.

L: Two dimension array i_{\max} , j_{\max} definition

The location field contains the name of the array to be loaded. The value field is defined to consist of 2 subfields, separated by a comma, of 2 columns each containing the two-digit decimal integers for i_{\max} and j_{\max} respectively where i_{\max} and j_{\max} generally appear in a DIMENSION statement. The i_{\max} and j_{\max} values are retained to compute the successive subscripted locations until redefined. Blank address fields may follow this array definition if successive elements of the array are to be loaded.

M: Two dimension array i_{\max} , j_{\max} definition

Conversion is identical to L except the entire array is preset to zero.

E: End Case

This defines an end-of-case and control is returned to the FORTRAN object program. The rest of this field and the remaining fields on the card are ignored.

Calling Sequence:

The following two types of CALL statements may be used:

I. CALL FINP (n,X,Y,ZETA,...,mHX(5)Y(5)ZETA(2)...) where

- A. n is the number of variables and/or arrays in the list, excluding n itself.
- B. X, Y, ZETA,... are the names of variables and/or arrays restricted to at most 5 characters each, one character of which is non-numeric.
- C. m is 6 times n. Hence, mH allows for 6n Hollerith characters to follow.

D. X(5)Y(5)ZETA(2)... is a list of the items previously named in exactly the same order with (1) indicating the number, i, of blanks necessary to provide six Hollerith characters for each item. Since each item name is restricted to 5 characters, the minimum value of (i) is (1).

II. CALL FINP (0) where the number of items is given as zero. This CALL statement must be used only after a CALL statement of type I has been executed. When the subroutine encounters a zero for the number of items, it immediately refers to the last executed CALL FINP with a nonzero number of items for the names of the items to be loaded.

Space Requirements

613 cells.

Number of Pages

Writeup	6
Listing	<u>12</u>
Total	18

[illegible]

GINC	TXL	GINC+2		FINP0049
	TXH	GINB,1,**		FINP0050
	TXL	GINA		FINP0051
	AXC	COMMON,1		FINP0052
	LDQ	0,1		FINP0053
GIN01	PXD	**	SAVE PREFIX CODE	FINP0054
	LGL	6		FINP0055
	STO	PREFIX		FINP0056
	STQ	0,1		FINP0057
	SUB	ME	E	FINP0058
	TZE	GIN13	END	FINP0059
	LGL	30	SAVE LAST DIGIT OF ADDRESS	FINP0060
	ANA	MASK1		FINP0061
	STO	ADDIND		FINP0062
	STZ	SUM	TEST FOR BLANK ADDRESS	FINP0063
	STZ	SIGN		FINP0064
	CLA	0,1		FINP0065
	CAS	MASK2		FINP0066
	TXL	**2		FINP0067
	TXL	GIN06	BLANK	FINP0068
	LRS	18	TEST FOR MATRIX	FINP0069
	ANA	MASK1		FINP0070
	SUB	MASK4		FINP0071
	TNZ	GIN17-2		FINP0072
	TSX	MTX00,4	MATRIX	FINP0073
	TRA	GINER	OUTSIDE MATRIX	FINP0074
	TRA	GIN20		FINP0075
MASK4	OCT	73		FINP0076
	AXT	5,4		FINP0077
	LDQ	0,1		FINP0078
GIN17	PXD			FINP0079
	LGL	6		FINP0080
	PAX	0,2		FINP0081
	TXL	GIN18,2,9		FINP0082
	TXH	GIN19,2,48		FINP0083
	TXL	GIN19,2,47		FINP0084
GIN18	TIH	GIN17,4,1		FINP0085
	TXL	GIN16		FINP0086
GIN19	CLA	0,1	SYMBOLIC	FINP0087
	ORA	MASK3		FINP0088
	TSX	TBL00,4		FINP0089
	LLS	35		FINP0090
	STA	GIN00		FINP0091
GIN20	CLA	MASK3		FINP0092
	STO	ADDIND		FINP0093
	TXL	GIN07		FINP0094
GIN16	CLA	ADDIND	TEST FOR OCTAL	FINP0095
	SUB	MASK3		FINP0096
	TZE	GIN04		FINP0097
	LXA	5B35,2	SET-UP OCTAL ADDRESS	FINP0098
	TSX	OCTAL,4		FINP0099

```

GIN02      TXH      5,,**
GIN03      TXL      GIN07,,**
GIN04      LXA      100B35,2
           CLA      4B35
           TSX      DECIM,4
GIN05      TXH      6,,**
           XCA
           SUB              1B35
           XCA
           TXL      GINER,2,100
           TXL              GIN07
GIN06      LDQ      MASK2
GIN07      STQ      CRDADD
           LXA      PREFIX,4
           TXH      GINER,4,48
           TXL      GIN08,4,47
           LXD      100B35,4
           TXL      GIN09
GIN08      TXH              GINER,4,36
           TXL              **2,4,32
           TXI              GIN09,4,-23
           TXH              GINER,4,25
           TNX      GINER,4,16
GIN09      TXI      GIN09+1,1,-1
           TRA      GIN10,4
           TXL              MCD00
           TXL              MCD00
           TXL              GINER
           TRA*      CRDADD
           TXL              IGIN00
           TXL              HGIN00
           TXL              GGIN00
           TXL              FGIN00
           TXL      GINER
           TXL              DGIN00
           TXL      GINER
           TXL              BGIN00
           TXL              ACD0
GIN10      TXL      LGIN00,,12
GIN11      TXI      GIN11+1,1,-1
           TXH              GIN01+1,1,**
GIN12      TXL      GINA
GIN13      LXD      GIN00,4
           LXD      GIN02,1
           LXD      GIN05,2
           TRA      2,4
GINER      PXD
           LDI      STOP2
           CALL      (EXE)
STOP2      PZE      2,4
ME          BCI      1,00000E

```

SET UP DECIMAL ADDRESS

SET-UP TRA TO
SUB-PROGRAM

```

M MATRIX IJ(ZERO
L MATRIX IJ=NO ZERO
K

```

I	INTEGER
H	HEADER
G	TABLE: ORIGIN
F	FIXED: FONT

F D BCD

B OCTAL
A SYMBOLIC
BLANK FLOATING
TEST END CARD

BLANK FLOATING
TEST END CARD

TO NEXT CARD

EXIT

S-163

[illegible]

FINP-9

```

BLANK BCI 1,
      REM
HGIN00 CLA CRDADD
      CAS MASK2
      TXL **2
      TXL GIN12
      LDQ CRDADD
      MPY 11B35
      STQ COMMON
      CAL GIN01
      SBM COMMON
      STA HGIN01
      LXD 1B35,4
      LXA 11B35,1
      CLA COMMON+12,1
HGIN01 STO **,4
      TXI **1,4,1
      TIX HGIN01=1,1,1
      TXL GIN12
GGIN00 CLA ADDIND
      SUB MASK3
      TZE GGIN01
      PXD
      TXL GGIN02
GGIN01 CAL GIN00
GGIN02 ADD 1B35
      ADD CRDADD
      STA SGIN03
      TXL GIN12
BGIN00 STZ SUM
      STZ SIGN
      LXA M6B35,2
      TSX OCTAL,4
      TXI BGIN04,1,-1
      TXI BGIN01,1,-1
BGIN01 LXA M6B35,2
      TSX OCTAL,4
      TXH 4
BGIN02 TSX SGIN00,4
BGIN03 TXL GIN11,**
BGIN04 TXH BGIN03,2,5
      TXL BGIN02
IGIN00 TSX DECNO,4
      TXH GINER,2,0
      LLS 18
      TXL BGIN02
DGIN00 LDQ 0,1
      TSX SGIN00,4
      CLA MASK2
      STO CRDADD
      LDQ 1,1

```

BLANK

EXIT FOR NEW PREFIX
BLANK

INTERGER FORMAT
ERROR FOR NON-INTEGER

```

FINP0151
FINP0152
FINP0153
FINP0154
FINP0155
FINP0156
FINP0157
FINP0158
FINP0159
FINP0160
FINP0161
FINP0162
FINP0163
FINP0164
FINP0165
FINP0166
FINP0167
FINP0168
FINP0169
FINP0170
FINP0171
FINP0172
FINP0173
FINP0174
FINP0175
FINP0176
FINP0177
FINP0178
FINP0179
FINP0180
FINP0181
FINP0182
FINP0183
FINP0184
FINP0185
FINP0186
FINP0187
FINP0188
FINP0189
FINP0190
FINP0191
FINP0192
FINP0193
FINP0194
FINP0195
FINP0196
FINP0197
FINP0198
FINP0199
FINP0200
FINP0201

```

```

DECNO TXI BGINO2,1,-1
      SxD BGINO3,4
      CLA 1,1
      ALS 24
      SLW COMMON*20
      STZ SUM
      STZ SIGN
      LXA 100B35,2
      CLS M6B35
      TSX DECIM,4
      TXI DEC2+1,1,-1
      TXI DEC1,1,-1
DECN1 CLA 4B35
      TSX DECIM,4
DECN2 TXH 2,,**
      TXL DEC4,2,99
      TXL GIN11,2,100
DECN3 LXD 1B35,2
DECN4 LXD BGINO3,4
      LXD BGINO3,4
      TRA 1,4
DECEN SxD GINO3,4
      TSX DECNO,4
      STQ COMMON*13
      SxD DEC2,2
      CLA DEC2
      STZ SUM
      STZ SIGN
      LDQ COMMON*20
      STQ 0,1
      TSX DECIM,4
      TXH
      LXD GINO3,4
      TRA 1,4
FGIN00 TSX DECEN,4
      STQ COMMON
      CAL DEC2
      COM
      ADD 1B17
      PDX 0,2
      CLA COMMON
      SUB BREF,2
      TMI GINER
      STA FGINO1
      LDQ COMMON*13
      MPY FREF,2
FGIN01 LRS **
      TNZ GINER
      TXL BGINO2,,**
LGIN00 TSX DECEN,4
      STQ COMMON

```

6

END ON BLANK

4

FIXED PT. CONVERSION

FLTG. PT. CONVERSION

```

FINP0202
FINP0203
FINP0204
FINP0205
FINP0206
FINP0207
FINP0208
FINP0209
FINP0210
FINP0211
FINP0212
FINP0213
FINP0214
FINP0215
FINP0216
FINP0217
FINP0218
FINP0219
FINP0220
FINP0221
FINP0222
FINP0223
FINP0224
FINP0225
FINP0226
FINP0227
FINP0228
FINP0229
FINP0230
FINP0231
FINP0232
FINP0233
FINP0234
FINP0235
FINP0236
FINP0237
FINP0238
FINP0239
FINP0240
FINP0241
FINP0242
FINP0243
FINP0244
FINP0245
FINP0246
FINP0247
FINP0248
FINP0249
FINP0250
FINP0251
FINP0252

```

```

LXD DECN2,2
PXD ,2
ARS 18
SSM
ADD COMMON
LRS 35
DVP 10B35
SUB M9B35
PAX ,2
CLM
LLS 35
ADD 5B35
TMI GINER
PAX ,4
SXD FGINO1*2,1
CLA XREF1,2
ADD XREF2,4
ADD 126B35
TPL LGINOA
STZ COMMON+13
LGINOA PAX 0,1
LDQ FREF1,2
MPR FREF2,4
LRS 35
MPY COMMON+13
LLS 2
TZE LGINO3
LGINO1 TZE LGINO2
LRS 1
TXI LGINO1,1,1
LGINO2 PXD ,1
ARS 18
LLS 0
LRS 8
LGINO3 LXD FGINO1*2,1
TNZ GINER
TXL BGINO2
SGIN00 CLA CRDADD
SUB MASK2
TZE SGIN01
CLA ADDIND
SUB MASK3
TZE SGINOA
CLA CRDADD
TXL SGINO2
SGINOA CAL GIN00
SUB CRDADD
TXL SGINO2
SGIN01 CAL SGIN03
SUB 1B35
SGIN02 STA SGIN03

```

HIGH DIGIT

SAVE ADD REFERENCE

EXIT TO STORE
STORE ROUTINE

ADD 1 TO OLD ADDRESS

```

FINP0253
FINP0254
FINP0255
FINP0256
FINP0257
FINP0258
FINP0259
FINP0260
FINP0261
FINP0262
FINP0263
FINP0264
FINP0265
FINP0266
FINP0267
FINP0268
FINP0269
FINP0270
FINP0271
FINP0272
FINP0273
FINP0274
FINP0275
FINP0276
FINP0277
FINP0278
FINP0279
FINP0280
FINP0281
FINP0282
FINP0283
FINP0284
FINP0285
FINP0286
FINP0287
FINP0288
FINP0289
FINP0290
FINP0291
FINP0292
FINP0293
FINP0294
FINP0295
FINP0296
FINP0297
FINP0298
FINP0299
FINP0300
FINP0301
FINP0302
FINP0303

```

GENERATE DECIMAL INTEGER

END ON BLANK

FINP-13

DECIM7 TIX DECIM1,4,1
 LXD DECIM2,4
 TXI DECIM8*1,4,-1 END ON DIGIT COUNT
 DEC 133
 100B35 DEC 100
 DEC 67
 DEC 34
 1B35 DEC 1
 DEC -33
 DEC -66
 DEC -99
 DEC -132
 XREF2 DEC .918354961680
 DEC .788860905380
 DEC .677626357980
 DEC .582076609280
 DEC .580
 DEC .858993459280
 DEC .737869763080
 DEC .633825300280
 DEC .544451787180
 FREF2 DEC 30
 DEC 27
 DEC 24
 DEC 20
 17B35 DEC 17
 DEC 14
 10B35 DEC 10
 DEC 7
 4B35 DEC 4
 BREF DEC 1
 DEC -3
 M6B35 DEC -6
 M9B35 DEC -9
 DEC -13
 DEC -16
 DEC -19
 DEC -23
 DEC -26
 XREF1 DEC -29
 DEC .931322574780
 DEC .745058059780
 DEC .596046447880
 DEC .953674316580
 DEC .762939453180
 DEC .610351562580
 DEC .976562580
 DEC .7812580
 DEC .62580
 FREF DEC .580
 DEC .880

FINP0355
 FINP0356
 FINP0357
 FINP0358
 FINP0359
 FINP0360
 FINP0361
 FINP0362
 FINP0363
 FINP0364
 FINP0365
 FINP0366
 FINP0367
 FINP0368
 FINP0369
 FINP0370
 FINP0371
 FINP0372
 FINP0373
 FINP0374
 FINP0375
 FINP0376
 FINP0377
 FINP0378
 FINP0379
 FINP0380
 FINP0381
 FINP0382
 FINP0383
 FINP0384
 FINP0385
 FINP0386
 FINP0387
 FINP0388
 FINP0389
 FINP0390
 FINP0391
 FINP0392
 FINP0393
 FINP0394
 FINP0395
 FINP0396
 FINP0397
 FINP0398
 FINP0399
 FINP0400
 FINP0401
 FINP0402
 FINP0403
 FINP0404
 FINP0405

	DEC	.6480	
	DEC	.51280	
	DEC	.819280	
	DEC	.6553680	
	DEC	.52428880	
	DEC	.838860880	
	DEC	.6710886480	
FREF1	DEC	.53687091280	
5B35	DEC	5	
126B35	PZE	126	
MASK1	OCT	000000000077	
MASK2	OCT	606060606000	
MASK3	OCT	000000000060	
1B17	OCT	1000000	
2B35	DEC	2B35	
3B35	PZE	3	
8B35	DEC	8B35	
11B35	PZE	11	
12B35	PZE	12	
MTX00	SXA	MTX10,4	
	AXT	2,4	
MTX01	SXA	MTX02,4	
	STZ	SIGN	
	STZ	SUM	
	LXA	100B35,2	
	CLA	2B35	
	TSX	DECIM,4	
	TXH	0,0,0	
	TXL	GINER,2,100	
MTX02	AXT	**,4	
	STQ	I+2,4	
	LDQ	0,1	
	LQL	6	
	STQ	0,1	
	TIK	MTX01,4,1	
MTX10	AXT	**,4	
	CLA	J	
	SUB	1B35	
	XCA		
	MPY	IMAX	
	XCA		
	ADD	I	
	LDQ	IJ	
	TLQ	1,4	
	SUB	1B35	
	XCA		
	TRA	2,4	
*	SET UP	IJ WORD	
MCD00	SXA	MCD02,4	
	CAL	GIN00	
	ADD	1B35	

TSX.MTX00,4
IJ RETURN
NORMAL RETURN

I,J
REMOVE
;COMMA

LOC. GTR MAX

[illegible]

	STA	SGIN03		FINP0457
	TSX	MTX00,4		FINP0458
MCD02	INOP	**		FINP0459
	LDQ	I		FINP0460
	STQ	IMAX		FINP0461
	MPY	J		FINP0462
	STQ	IJ		FINP0463
	LXA	MCD02,4		FINP0464
	TXL	MCD04,4,12		FINP0465
	LXA	IJ,4		FINP0466
	TXI	**1,4,-1		FINP0467
	SXD	**6,4		FINP0468
	CLA	GIN00		FINP0469
	STA	**2		FINP0470
	LXD	1B35,4		FINP0471
	STZ	**,4		FINP0472
	TXI	**1,4,1		FINP0473
	TXL	*-2,4,**		FINP0474
MCD04	TXI	GIN11,1,-1		FINP0475
*				FINP0476
ACD0	STZ	CTR		FINP0477
	STZ	PASS		FINP0478
ACD1	STZ	PF		FINP0479
	AXT	5,2		FINP0480
	TSX	SYM00,4		FINP0481
	AXT	0,4	BLANK	FINP0482
	TXH	ACD6,2,1		FINP0483
	TXL	ACD12,4,0	NULL AND BLANK	FINP0484
	TXL	ACD6+1	NULL	FINP0485
ACD6	STQ	PF		FINP0486
	TXL	ACD10,4,0	BLANK	FINP0487
	AXT	1,2		FINP0488
	TSX	SYM00,4		FINP0489
	AXT	0,4	BLANK	FINP0490
	TXL	ACD10,2,1	NULL	FINP0491
	XCL			FINP0492
	ALS	15		FINP0493
	STT	PF		FINP0494
ACD10	LDQ	PF		FINP0495
	CLS	PASS		FINP0496
	STO	PASS		FINP0497
	TPL	ACD15		FINP0498
	STQ	WORD		FINP0499
	TXH	ACD1,4,0	NOT BLANK	FINP0500
ACD12	LXA	CTR,4		FINP0501
	TXH	ACD14,4,6		FINP0502
	TXI	**1,1,-1		FINP0503
	TXL	**3,4,1	BLANK	FINP0504
ACD14	LDQ	WORD		FINP0505
	TSX	SGIN00,4		FINP0506
	TXL	GIN11		FINP0507

[illegible]

7

BLANK

СОННА

NO CHARACTERS:

LEFT JUSTIFY

SYMBOLIC

NO CHARACTERS

DECIMAL

OCTAL

	CLA	SYMBL		FINP0559
	STO	0,1		FINP0560
	TSX	SYM14,2		FINP0561
SYM10	CLA	SYMBL		FINP0562
	TSX	TBL00,4		FINP0563
SYM14	AXT	** ,4		FINP0564
	TRA	2,4	EXIT	FINP0565
SYM20	TXI	**1,4,1	BLANK	FINP0566
	SXA	SYM14,4		FINP0567
SYM21	TXL	SYM14+1,2,1	NULL FIELD	FINP0568
SYM25	CAL	PSYM		FINP0569
	ARS	6		FINP0570
	SLW	PSYM		FINP0571
	TXL	SYM03		FINP0572
TBL00	LXD	TBL01+1,2		FINP0573
TBL01	CAS	** ,2		FINP0574
	TXL	**2		FINP0575
	TXI	TBL02,2,-2		FINP0576
	TXI	**1,2,-1		FINP0577
TBL03	TXH	TBL01,2,**		FINP0578
	TXL	GINER,0,-1		FINP0579
TBL02	SXA	**1,2		FINP0580
	AXC	0,2		FINP0581
	SXA	**2,2		FINP0582
	LXD	FINPT,2		FINP0583
	LDQ	** ,2		FINP0584
	LXD	TBL03+1,2		FINP0585
	TRA	1,4		FINP0586
IMAX	PZE			FINP0587
IJ	PZE			FINP0588
COMMON	BSS	31		FINP0589
GIN00	SYN	COMMON+30		FINP0590
PF	SYN	COMMON+15		FINP0591
PASS	SYN	COMMON+16		FINP0592
CTR	EQU	COMMON+17		FINP0593
SYMBL	EQU	COMMON+18		FINP0594
PSYM	EQU	COMMON+19		FINP0595
CRDADD	EQU	COMMON+21		FINP0596
SIGN	EQU	COMMON+22		FINP0597
SUM	EQU	COMMON+23		FINP0598
ADDIND	EQU	COMMON+24		FINP0599
PREFIX	EQU	COMMON+25		FINP0600
WORD	SYN	COMMON+26		FINP0601
ERROR	SYN	COMMON+27		FINP0602
I	SYN	PASS		FINP0603
J	SYN	CTR		FINP0604
FINPT	SYN	FINP		FINP0605
	END			FINP

FINP-18

Function: FNORM

Purpose: To find the magnitude of a 3-dimensional vector.

Calling Sequence:

Y = FNORM(X)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	X	3	X_1, X_2, X_3		
O	FNORM	1			$FNORM = (X_1^2 + X_2^2 + X_3^2)^{\frac{1}{2}}$

Common storages used or required:

None

Subroutines required:

None

Functions required:

SQRTF

Approximate number of storages required:

FNORM

```
*      SYMBOL TABLE
CEC2018  FUNCTION FNORM
        FUNCTION FNORM(X)
        DIMENSION X(3)
1  FNORM = SQRTF(X(1)**2+X(2)**2+X(3)**2)
3  RETURN
END
```

```
FNOR
FNOR
FNOR0000
FNOR0010
FNOR0020
FNOR0030
FNOR
```

Subroutine: GHA

Purpose: To determine the Greenwich Hour Angle of the first point of Aries for a given date and time.

Calling Sequence:

CALL GHA (TSEC, D, GHAN, DA, OMEGA)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TSEC	1		seconds	Fractional part of day from D
I	D	1		days	Whole days from Jan. 1, 1950
O	GHAN	1		degrees	Greenwich Hour Angle,
					$0 \leq \text{GHA} < 360$
I	DA	1			Adjustment due to nutation*
O	OMEGA	1	ω_e	degrees/sec	Rate of rotation of the earth
					*DA = EN(2,1) of EN nutation
					matrix from NUTATE

Common storages used or required:

None

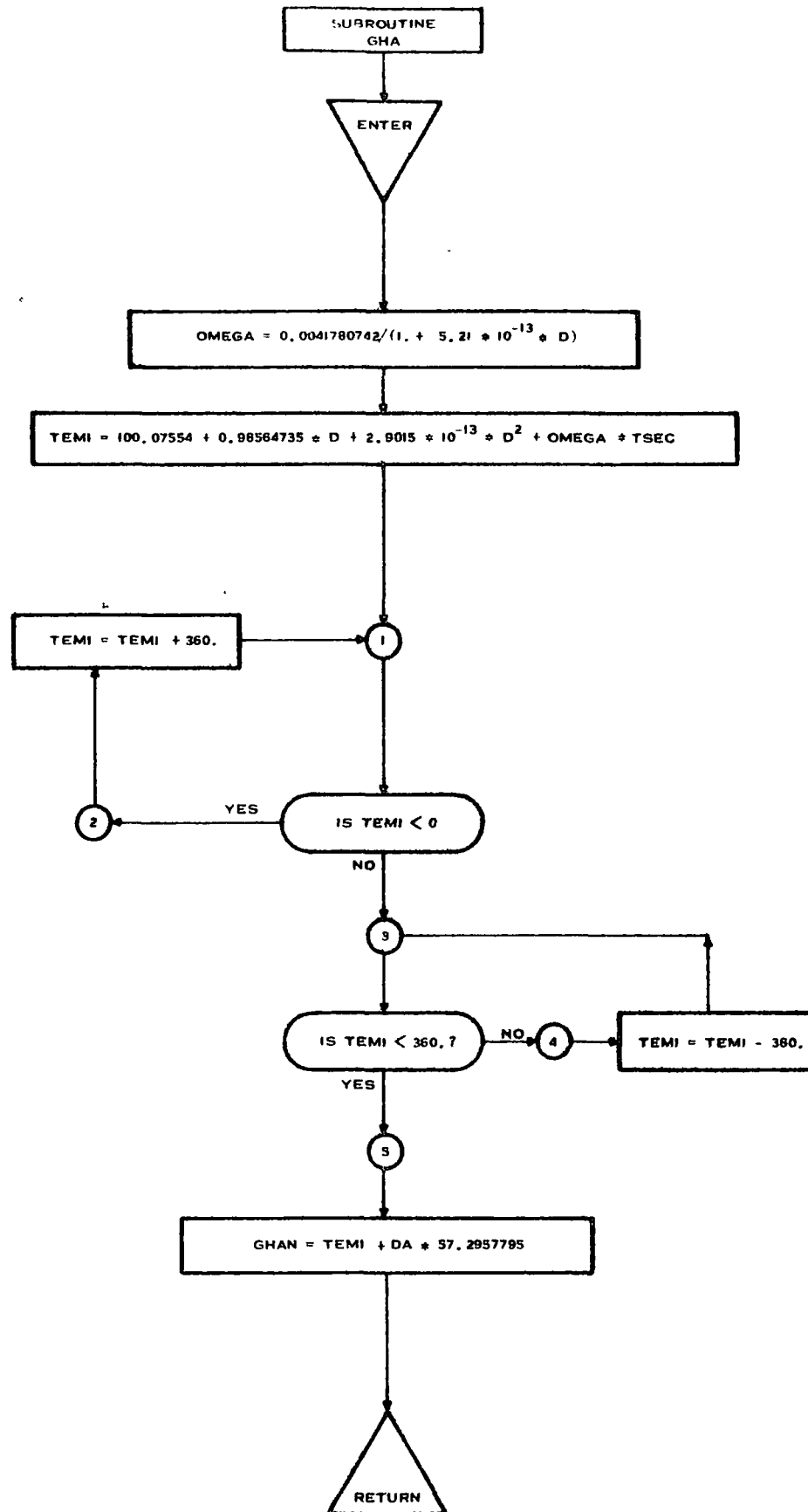
Subroutines required:

None

Functions required:

None

Approximate number of storages required:



GHA

* LABEL

CEC20AG

SUBROUTINE GHA(TSEC,D,GHAN,DA,OMEGA)

OMEGA = .0041780742/(1.+5.21E-13*D)

DD=D

D DD=DD*(.98564735/360.)

D DD=DD-INTF(DD)

DF=DD

TEM1 = 100.07554+360.*DF +2.9015E-13*D*D+OMEGA*TSEC

1 IF (TEM1) 2,3,3

2 TEM1 = TEM1+360.

GO TO 1

3 IF (TEM1-360.) 5,4,4

4 TEM1 = TEM1-360.

GO TO 3

5 GHAN = TEM1*DA*57.2957795

RETURN

END

GHA0
GHA0
GHA000
GHA001
GHA002
GHA003
GHA004
GHA005
GHA006
GHA007
GHA008
GHA009
GHA010
GHA011
GHA012
GHA013
GHA014
GHA0

GHA-3

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Subroutine: GOTOB

Purpose: It is a logic type of subroutine to read input data cards, set up a sequence for calling subroutine MATSUB, interpret types of measurements being made, and control integration package to perform specific operations (read new data, call MATSUB, stop, etc.) at specified times.

Calling Sequence:

CALL GOTOB (TSTPD)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TSTPD	1	time	days	Desired stop time in days from start

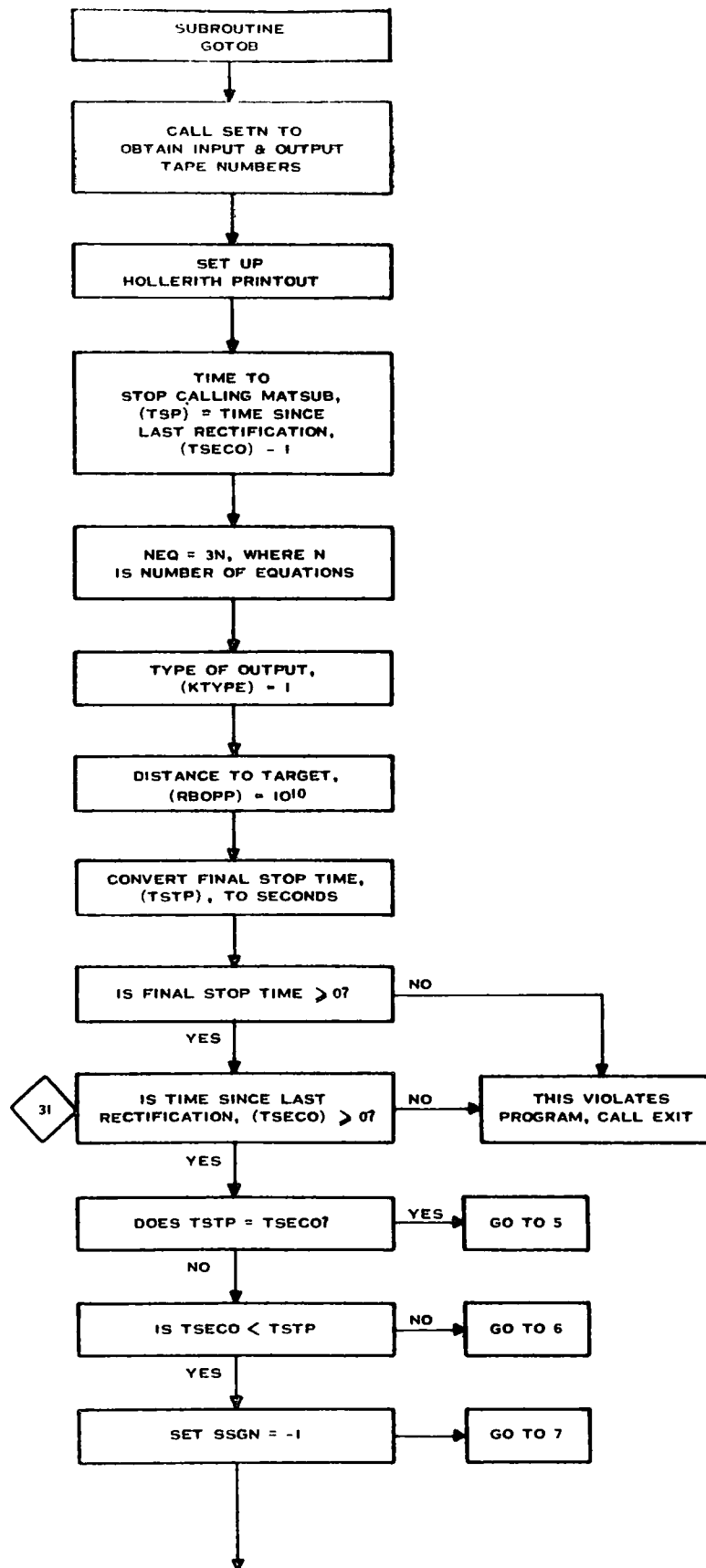
Common storages used or required:

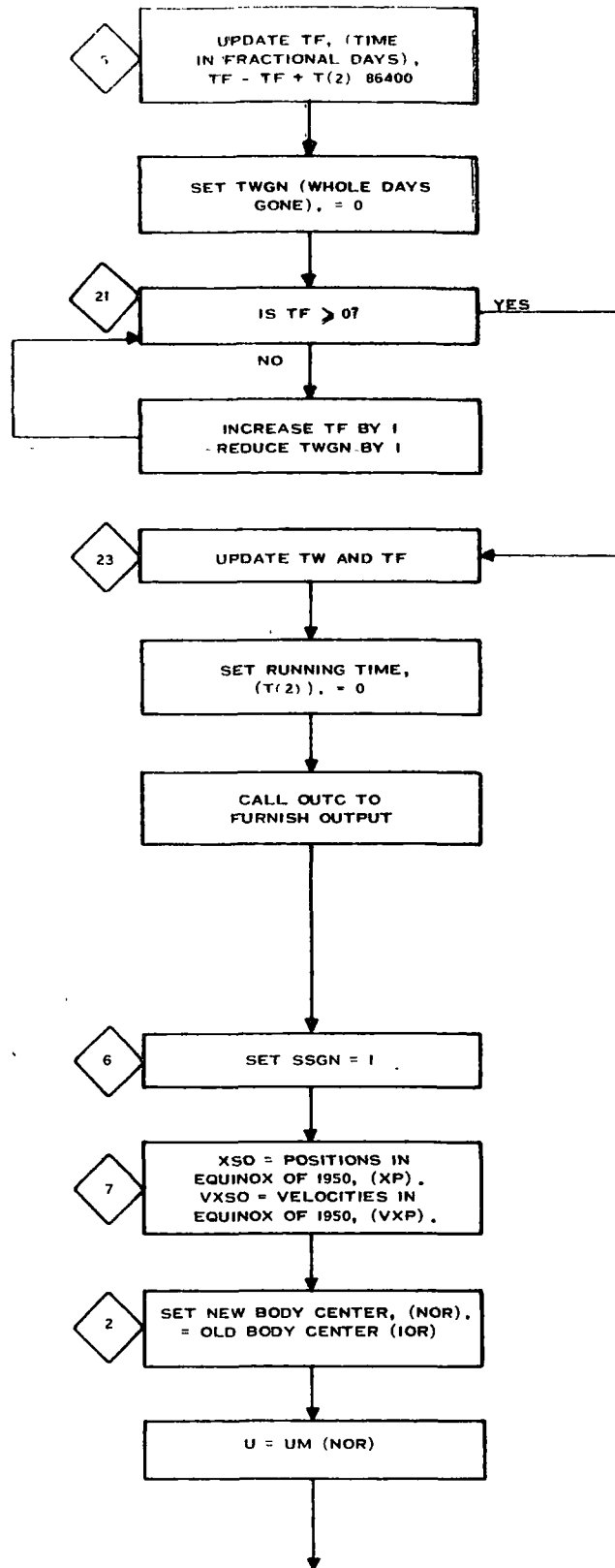
Subroutines required:

Functions required:

Approximate number of storages required:

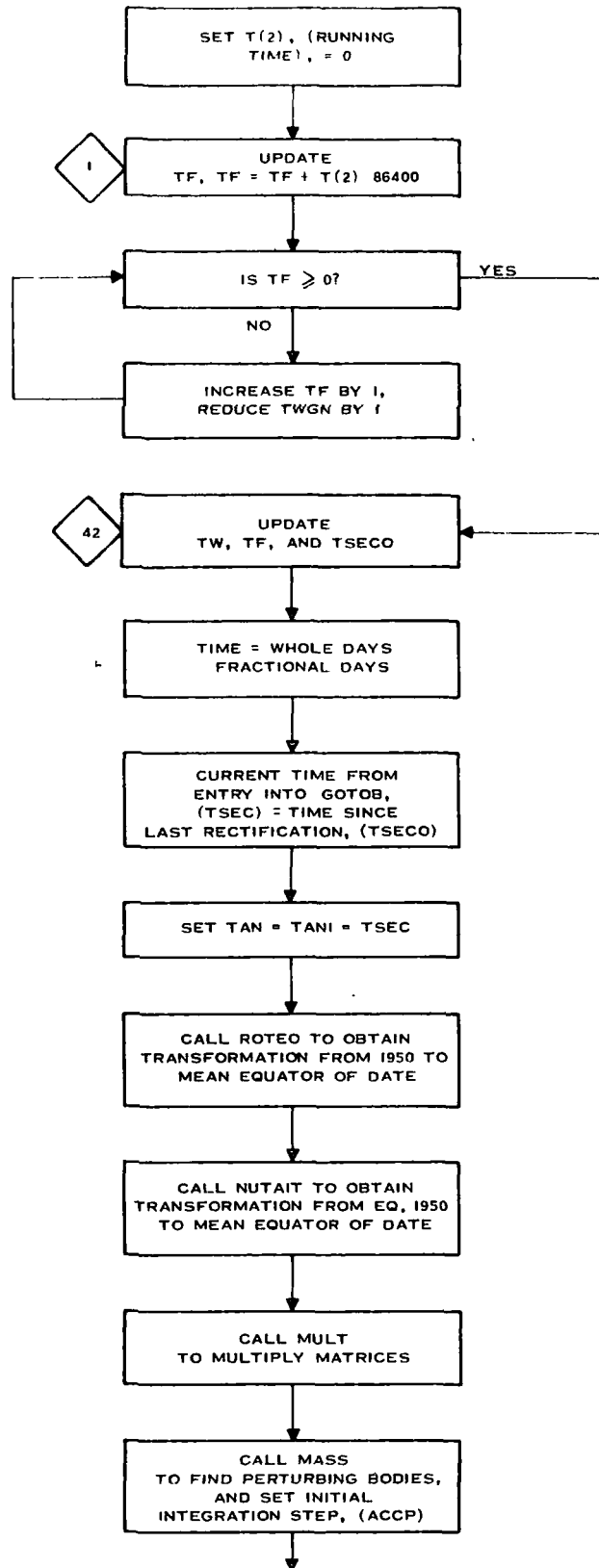
T, S, C, IC
 CHNGP, DE6FN, DE6FP, DE6FP3,
 DE6FP4, EXIT, MASS, MATSUB,
 MULT, NUTAIT, OUTC, ROTEQ,
 SDEC, SETN, SHIFTP, TIMED
 FNORM (FIL) (RTN) (SLI)
 1242 DEC

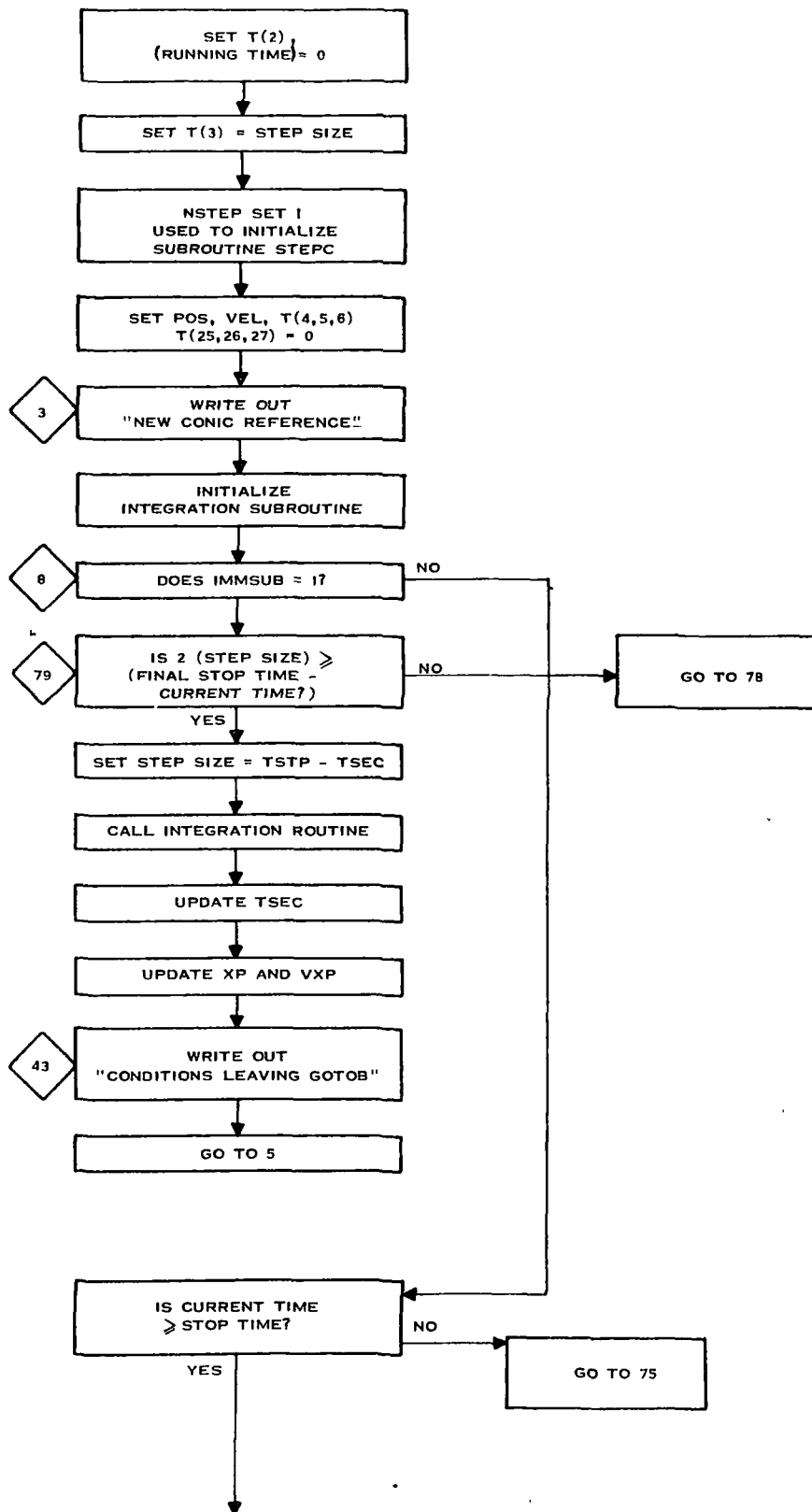




S-181

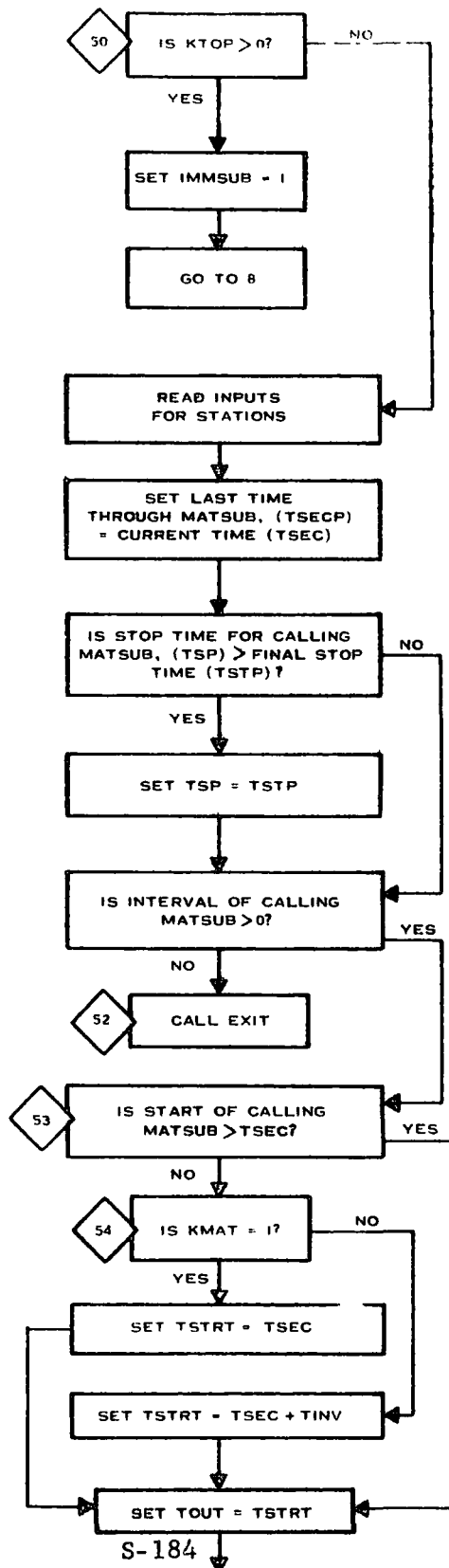
GOTOB-3





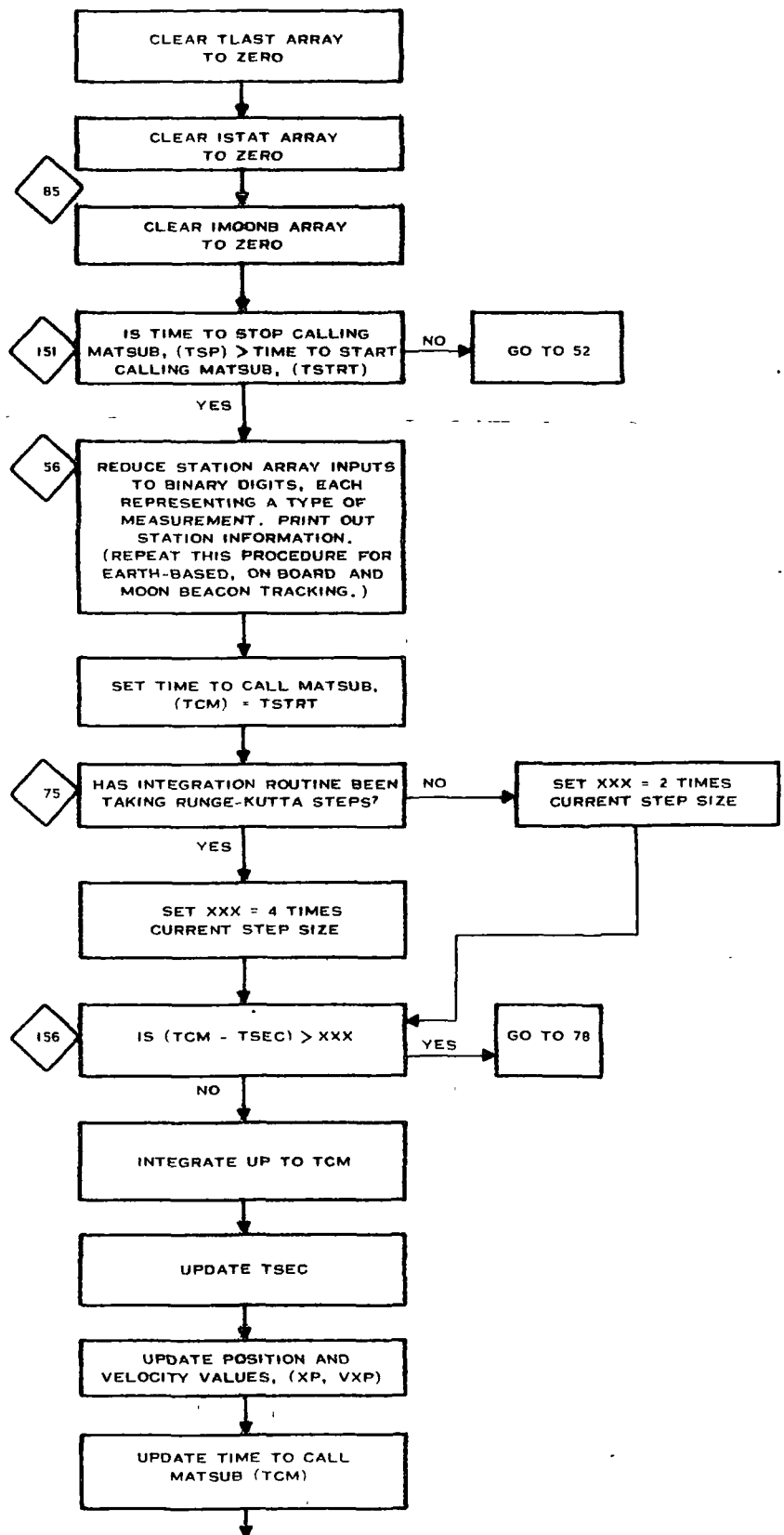
S-183

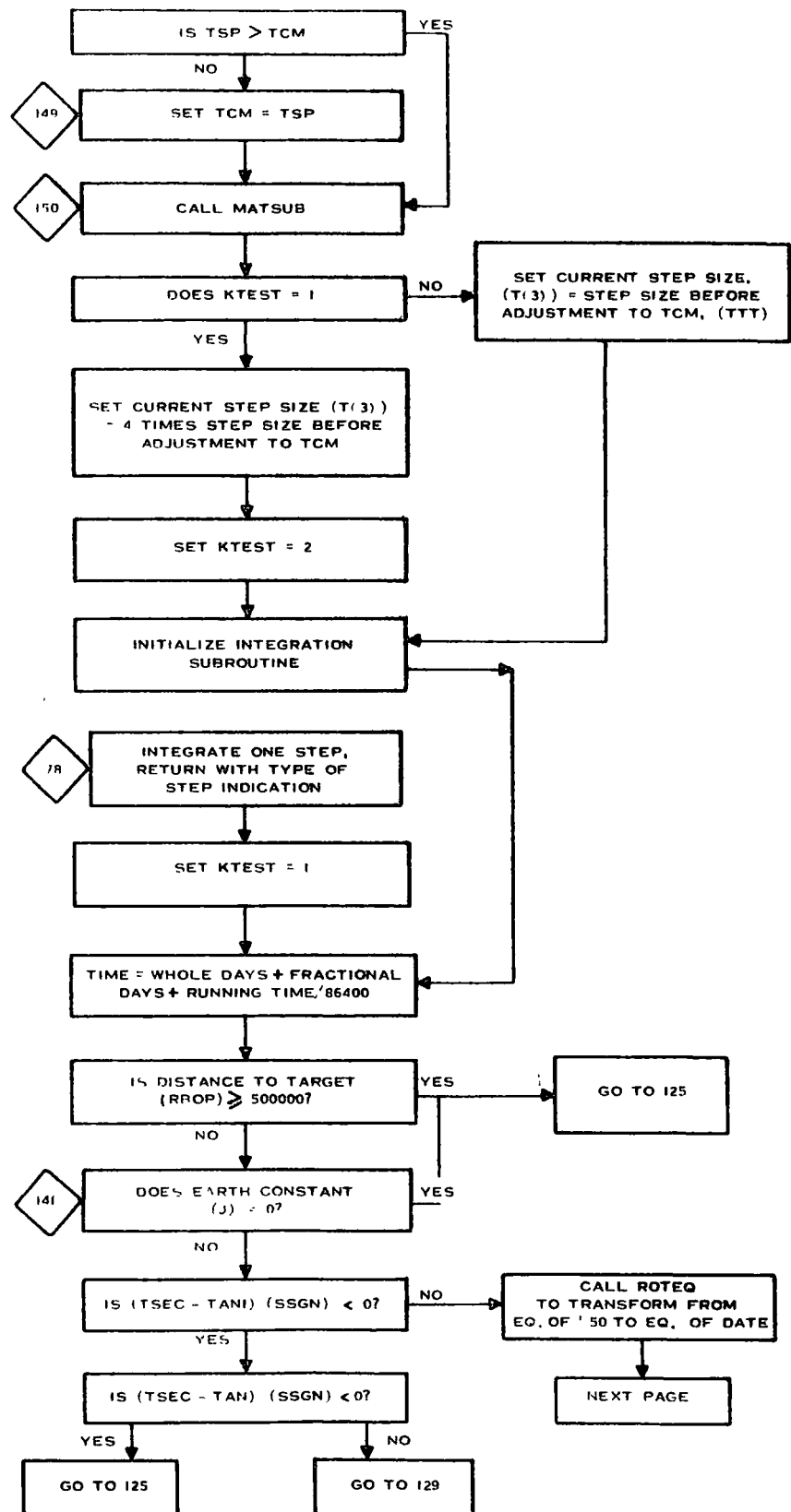
GOTOB-5



S-184

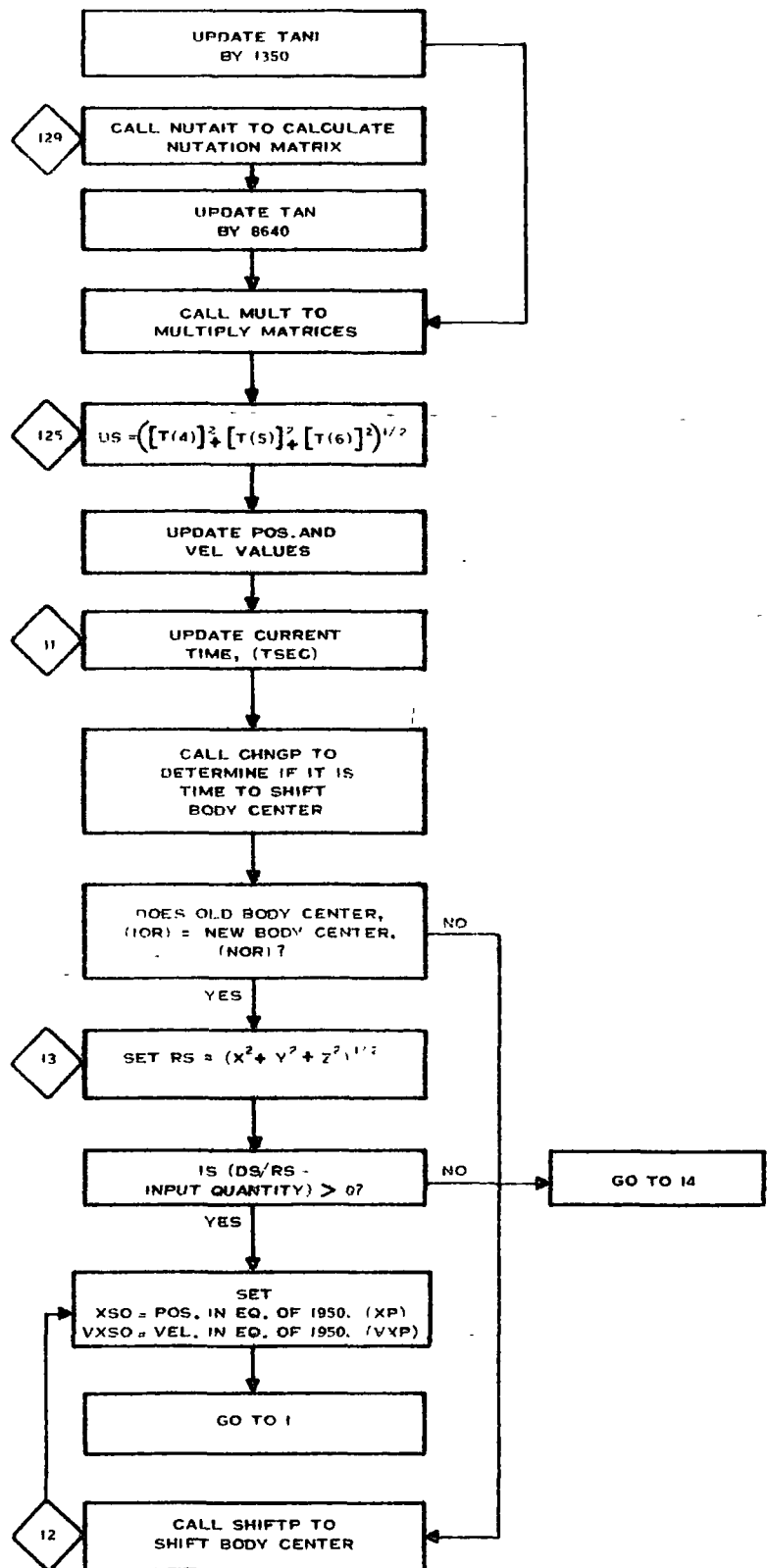
GOTOB-6

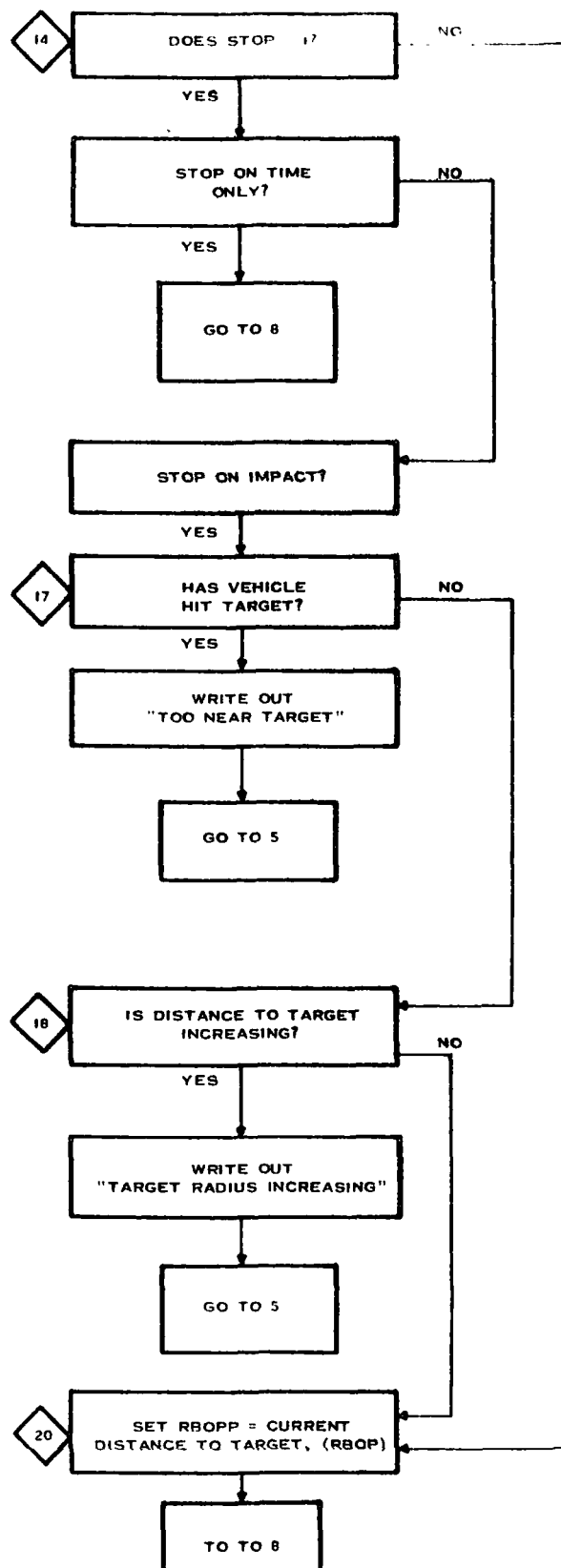




S-186

GOTOB-8





GOTOB-1

1010 (Cont'd)

K=I+NEQV	GOTB1320
XP(I)=X(I)+T(I+3)	GOTB1330
VXP(I)=VX(I)+T(K)	GOTB1340
43 CONTINUE	GOTB1350
WRITE OUTPUT TAPE NOUT,39	GOTB1360
39 FORMAT(25H0CONDITIONS LEAVING GOTOB)	GOTB1370
WRITE OUTPUT TAPE NOUT,750	GOTB1380
750 FORMAT(21H STOPPED ON TIME STOP)	GOTB1390
GO TO 5	GOTB1400
10 CONTINUE	GOTB1410
IF(TSEC=TSP)75,50,50	GOTB1420
50 CONTINUE	GOTB1430
C KTOP IS SET +1 ON LAST CARD OF SEQUENCE FOR NORMAL TIME STOP	GOTB1435
C OF GOTOB	GOTB1436
IF(KTOP)51,51,80	GOTB1440
80 CONTINUE	GOTB1450
IMMSUB=1	GOTB1460
GO TO 8	GOTB1470
51 READ INPUT TAPE NIN,700,ISA,IONB,IMB	GOTB1480
700 FORMAT(20I2,4X,6I2,4X,10I2)	GOTB1490
READ INPUT TAPE NIN,701,KTOP,TSTR,TSP1,TINT,TPRIN	GOTB1500
701 FORMAT(1X,I1,4E17.8)	GOTB1510
WRITE OUTPUT TAPE NOUT,708,KTOP,TSTR,TSP1,TINT,TPRIN	GOTB1520
708 FORMAT(/7H0 KTOP=,I1,7H TSTR=,1E17.8,7H TSP1=,1E17.8,7H TINT=	GOTB1530
1,1E17.8,8H TPRIN=,1E17.8)	GOTB1540
TSEC=TSEC	GOTB1550
C SUBROUTINE TIMED CONVERTS INPUT TIMES FROM FORMAT	GOTB1555
C (DAYS HOURS).(MIN SEC)	GOTB1556
CALL TIMED(TSTR,TSTRT)	GOTB1560
C TSTRT =START TIME FOR CALLING MATSUB	GOTB1570
CALL TIMED(TSP1,TSP)	GOTB1580
C TSP =STOP TIME AND INDICATOR FOR NEW DATA	GOTB1590
STOP=KTOP	GOTB1600
IF(TSP-TSTP)101,101,100	GOTB1610
100 TSP=TSTP	GOTB1620
101 CONTINUE	GOTB1630
CALL TIMED(TINT,TINV)	GOTB1640
C TINV =INTERVAL OF CALLING MATSUB	GOTB1650
CALL TIMED(TPRIN,TPRINT)	GOTB1660
C TPRINT=PRINT INTERVAL FOR MATSUB	GOTB1670
IF(TINV) 52,52,53	GOTB1680
52 WRITE OUTPUT TAPE NOUT,702	GOTB1690
702 FORMAT(26H0YOU BOTCHED UP INPUT DATA)	GOTB1700
CALL EXIT	GOTB1710
53 CONTINUE	GOTB1720
IF(TSTRT-TSEC) 54,54,158	GOTB1730
54 CONTINUE	GOTB1740
GO TO (152,153),KMAT	GOTB1750
152 TSTRT=TSEC	GOTB1760
TOUT=TSEC	GOTB1770
GO TO 158	GOTB1780

GOTOB-(Con't)

153	TSTRT=TSEC+TINV	GOTB179
	TOUT=TSEC+TPRINT	GOTB180
	GO TO 151	GOTB181
158	CONTINUE	GOTB182
	TOUT=TSTRT	GOTB183
	DO 84 I=1,4	GOTB184
	DO 84 J=1,6	GOTB185
	TLAST(I,J)=0.	GOTB186
84	CONTINUE	GOTB187
	DO 85 I=1,20	GOTB188
	ISTAT(I)=0	GOTB189
85	CONTINUE	GOTB190
	DO 86 I=1,10	GOTB191
	IMOONB(I)=0.	GOTB192
86	CONTINUE	GOTB193
151	CONTINUE	GOTB194
	IF(TSP-TSTRT) 52,52,55	GOTB195
55	CONTINUE	GOTB196
	LSTAT=1	GOTB197
	LONB=1	GOTB198
	LMB=1	GOTB199
	L=122	GOTB200
	DO 61 I=1,20	GOTB201
	L=L+15	GOTB202
	IF (ISA(I)) 61,61,56	GOTB203
56	CONTINUE	GOTB204
	WRITE OUTPUT TAPE NOUT,709,I,S(L)	GOTB205
709	FORMAT (17H STATION NUMBER ,I2,2H , ,A6,2H , ,10H MEASURES)	GOTB206
	BBB = ISA(I)	GOTB207
	LSTAT=2	GOTB208
	DO 60 J=1,4	GOTB209
	CCC=BBB/2.	GOTB210
	DDD=INTF(CCC)	GOTB211
	IF(CCC-DDD) 57,57,58	GOTB212
57	CONTINUE	GOTB213
C.	THE KS, KONB, AND KMB ARRAYS ARE COLUMN WISE ARRANGED IN BINARY	GOTB214
C.	FOR INDICATING TYPE MEASUREMENTS MADE ,KS FOR EARTH BASED TRACKING	GOTB215
C.	KONB FOR ONBOARD TRACKING, KMB FOR LUNAR BEACONS.	GOTB216
	KS(J,I)=0	GOTB217
	GO TO 59	GOTB218
58	CONTINUE	GOTB219
	KS(J,I)=1	GOTB220
	WRITE OUTPUT TAPE NOUT,703,SMEAS(J)	GOTB221
703	FORMAT (1H A6)	GOTB222
59	CONTINUE	GOTB223
	BBB=DDD	GOTB224
60	CONTINUE	GOTB225
61	CONTINUE	GOTB226
	DO 62 I=1,6	GOTB227
	IF (IONB(I)) 62,62,63	GOTB228
63	CONTINUE	GOTB229

GOTOB (Cont'd)

```

      WRITE OUTPUT TAPE NOUT,704,BNAME(I)
704  FORMAT (28H  VEHICLE TO CELESTIAL BODY ,A6,10H  MEASURES)
      LONB=2
      BBB=IONB(I)
      DO 68 J=1,4
      CCC=BBB/2.
      DDD=INTF(CCC)
      IF(CCC-DDD) 64,64,65
64  CONTINUE
      KONB(J,I)=0
      GO TO 67
65  CONTINUE
      KONB(J,I)=1
      WRITE OUTPUT TAPE NOUT,703,TOBM(J)
67  CONTINUE
      BBB=DDD
68  CONTINUE
62  CONTINUE
      DO 74 I=1,10
      IF (IMB(I)) 74,74,69
69  CONTINUE
      WRITE OUTPUT TAPE NOUT,706,I
706  FORMAT (33H  VEHICLE TO LUNAR BEACON NUMBER ,I2,10H  MEASURES)
      LMB=2
      BBB=IMB(I)
      DO 73 J=1,4
      CCC=BBB/2.
      DDD=INTF(CCC)
      IF(CCC-DDD) 70,70,71
70  CONTINUE
      KMB(J,I)=0
      GO TO 72
71  CONTINUE
      KMB(J,I)=1
      WRITE OUTPUT TAPE NOUT,703,TOBM(J)
72  CONTINUE
      BBB=DDD
73  CONTINUE
74  CONTINUE
      TCM=TSTRT
75  CONTINUE
      IF(ACCUM) 154,154,155
155  XXX=4.*T(3)
      GO TO 156
154  XXX=2.*T(3)
156  CONTINUE
      IF(TCM-TSEC=XXX) 76,76,78
76  CONTINUE
      TT=TCM-TSEC
      TTT=T(3)
      T(3)=TT

```

GOTB2300
 GOTB2310
 GOTB2320
 GOTB2330
 GOTB2340
 GOTB2350
 GOTB2360
 GOTB2370
 GOTB2380
 GOTB2390
 GOTB2400
 GOTB2410
 GOTB2420
 GOTB2430
 GOTB2440
 GOTB2450
 GOTB2460
 GOTB2470
 GOTB2480
 GOTB2490
 GOTB2500
 GOTB2510
 GOTB2520
 GOTB2530
 GOTB2540
 GOTB2550
 GOTB2560
 GOTB2570
 GOTB2580
 GOTB2590
 GOTB2600
 GOTB2610
 GOTB2620
 GOTB2630
 GOTB2640
 GOTB2650
 GOTB2660
 GOTB2670
 GOTB2680
 GOTB2690
 GOTB2700
 GOTB2710
 GOTB2720
 GOTB2730
 GOTB2740
 GOTB2750
 GOTB2760
 GOTB2770
 GOTB2780
 GOTB2790
 GOTB2800

GOTOB- (Cont'd)

DO 77 I=1,4	GOTB281
CALL DE6FP3(TT)	GOTB282
77 CONTINUE	GOTB283
TSEC = TSECO + T(2)	GOTB284
DO 157 I=1,3	GOTB285
K=I+NEQV	GOTB286
XP(I) = X(I)+T(I+3)	GOTB287
157 VXP(I) = VX(I)+T(K)	GOTB288
TCM=TCM+TINV	GOTB289
IF(TCM-TSP) 150,150,149	GOTB290
149 TCM=TSP	GOTB291
150 CONTINUE	GOTB292
CALL MATSUB	GOTB293
KMAT=2	GOTB294
IF(KTEST-1)81,81,82	GOTB295
81 T(3)=4.*TTT	GOTB296
KTEST=2	GOTB297
GO TO 87	GOTB298
82 T(3)=TTT	GOTB298
87 CONTINUE	GOTB299
CALL DE6FN(-1,1,T,NEQ,SDEC,3,4,1,E-9,3.456,172800.,86400.)	GOTB300
GO TO 113	GOTB301
78 CONTINUE	GOTB302
CALL DE6FP1(ACCUM)	GOTB303
KTEST=1	GOTB303
113 TIME = TW+TF + T(2)/86400.	GOTB304
IF (RBOP-500000.) 141,125,125	GOTB305
141 IF (VJ) 127,125,127	GOTB306
127 IF((TSEC-TAN1)*SSGN)142,126,126	GOTB307
142 IF((TSEC-TAN)*SSGN)125,129,129	GOTB308
126 CALL ROTEQ(TIME,EA)	GOTB309
TAN1=TAN1+1350.*SSGN	GOTB310
GO TO 140	GOTB311
129 CALL NUTAIT (TIME,CM,CRUD,DDC,EN,EPSIL)	GOTB312
TAN=TAN+8640.*SSGN	GOTB313
140 CALL MULT(EN,EA,AN,0)	GOTB314
125 CONTINUE	GOTB315
DS=FNORM(T(4))	GOTB316
DO 11 I=1,3	GOTB317
K=I+NEQV	GOTB318
XP(I)=X(I)+T(I+3)	GOTB319
VXP(I)=VX(I)+T(K)	GOTB320
11 CONTINUE	GOTB321
TSEC = TSECO + T(2)	GOTB322
CALL CHNGP(NOR,IOR,RBOP)	GOTB323
IF(IOR-NOR)12,13,12	GOTB324
13 CONTINUE	GOTB325
RS=FNORM(X)	GOTB326
IF(DS/RS-ENKE)14,15,15	GOTB327
15 CONTINUE	GOTB328
DO 16 I=1,3	GOTB329

GOTOB (Cont'd)

XSO(I)=XP(I)	GOTB3300
VXSO(I)=VXP(I)	GOTB3310
16 CONTINUE	GOTB3320
GO TO 1	GOTB3330
12 CONTINUE	GOTB3340
CALL SHIFTP(IOR,NOR,U,UM,XP,VXP,PO,VE,TF,TW,T(2))	GOTB3350
GO TO 15	GOTB3360
14 CONTINUE	GOTB3370
ITARG = ITARG	GOTB3380
IF(STOP=1.)20,83,83	GOTB3390
83 CONTINUE	GOTB3400
KSTP=KSTP	GOTB3410
GO TO (17,18,8),KSTP	GOTB3420
17 CONTINUE	GOTB3430
IF(RBOP(ITARG)-RAD(ITARG))19,19,18	GOTB3440
19 CONTINUE	GOTB3450
WRITE OUTPUT TAPE NOUT,39	GOTB3460
WRITE OUTPUT TAPE NOUT,34,RBOP(ITARG),RAD(ITARG),ITARG	GOTB3470
34 FORMAT(21H TOO NEAR TARG RBOP=,1E17.8,5H RAD=,1E17.8,6H TARG=,I1)	GOTB3480
KTYPE=2	GOTB3490
GO TO 5	GOTB3500
18 CONTINUE	GOTB3510
IF(RBOP(ITARG)-RBOPP)20,35,35	GOTB3520
35 CONTINUE	GOTB3530
WRITE OUTPUT TAPE NOUT,39	GOTB3540
WRITE OUTPUT TAPE NOUT,36,RBOP(ITARG),RBOPP,ITARG	GOTB3550
36 FORMAT(29H TARG RADIUS INCREASING RBOP=,1E17.8,7H RBOPP=,1E17.8,6H	GOTB3560
1 TARG=,I1)	GOTB3570
KTYPE=2	GOTB3580
GO TO 5	GOTB3590
20 CONTINUE	GOTB3600
RBOPP=RBOP(ITARG)	GOTB3610
GO TO 8	GOTB3620
END	GOTB

Subroutine: GOTOR

Purpose: To solve Kepler's equation for incremental excentric anomaly on a conic section given the incremental mean anomaly (time).

Calling Sequence:

CALL GOTOR (K, VM, C, F, E1)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	K	1	K		Orbit type (1) Elliptic
					(2) Hyperbolic
I	VM	1	ΔM	RAD	Incremental mean anomaly
I	C	2	$C_1 C_2$		Kepler's equation coefficients
O	F	4	F		Trigonometric functions of
					incremental eccentric anomaly
I/O		1	ΔE	RAD	Incremental eccentric anomaly

Common storages used or required:

None

Subroutines required:

None

Functions required:

SIN, COS, EXP

Approximate number of storages required: 476 DEC

Discussion (See subroutine STEPC)

The incremental eccentric anomaly, φ , is implicitly expressed as a function of incremental mean anomaly, ΔM , and conic coefficients, C_1 and C_2 , by transcendental equations

$$\Delta M = (\varphi - \sin \varphi) + C_1 \sin \varphi - C_2 (\cos \varphi - 1) \quad \text{elliptical}$$

$$\Delta M = (\sinh \varphi - \varphi) + C_1 \sinh \varphi + C_2 (\cosh \varphi - 1) \quad \text{hyperbolic}$$

The two equations above may be written as a single equation

$$\Delta M = f_1(\varphi) + C_1 f_3(\varphi) + C_2 f_4(\varphi)$$

if the convention below is adopted.

For the elliptical case, let

$$f_1(\varphi) = \varphi - \sin \varphi$$

$$f_2(\varphi) = 1 - \cos \varphi$$

$$f_3(\varphi) = \sin \varphi$$

$$f_4(\varphi) = \cos \varphi$$

and for the hyperbolic case, let

$$f_1(\varphi) = \sinh \varphi - \varphi$$

$$f_2(\varphi) = \cosh \varphi - 1$$

$$f_3(\varphi) = \sinh \varphi$$

$$f_4(\varphi) = \cosh \varphi$$

When $|\varphi| \leq 1$, numerical accuracy requires that $f_1(\varphi)$ and $f_2(\varphi)$ be computed by truncated series expansions. Otherwise, the computer library functions SIN, COS and EXP are used in the computation.

The slope of the function

$$F(\varphi) = f_1(\varphi) + C_1 f_3(\varphi) + C_2 f_4(\varphi)$$

at φ is seen to be

$$F'(\varphi) = f_2(\varphi) + C_1 f_4(\varphi) + C_2 f_3(\varphi).$$

$F(\varphi)$ is a monotonically increasing function of φ so that any solution of the equation $F(\varphi) = \Delta M$ is obviously unique. Newton's method of iteration is used. That is, letting φ_n be the n^{th} estimate of φ , the $(n+1)^{\text{st}}$ estimate is calculated from

$$\varphi_{n+1} = \varphi_n + \frac{\Delta M - F(\varphi_n)}{F'(\varphi_n)}$$

The iteration is halted and φ is said to be φ_n when

$$\left| \frac{\varphi_{n+1} - \varphi_n}{\varphi_{n+1} + \varphi_n} \right| \leq 3. \times 10^{-8}$$

or when $n = 20$, whichever occurs first. The $f_1(\varphi)$ as well as φ are output from GOTOR to avoid their re-computation outside the subroutine.

GOTOR

*	LABEL	GOTR
CEC2091	NEW GOTOR	GOTR
	SUBROUTINE GOTOR(K,VM,C,F,E1)	GOTR0010
	DIMENSION C(2),F(4)	GOTR0020
	NMAX=20	GOTR0030
	N=0	GOTR0040
	GO TO (1,2),K	GOTR0050
1	CONTINUE	GOTR0060
C	FIRST GUESS IS OBTAINED FOR ELLIPTICAL CASE	GOTR0070
8	CONTINUE	GOTR0080
	IF(E1=1.)30,31,31	GOTR0090
30	CONTINUE	GOTR0100
	D2=E1*E1	GOTR0110
	F(1)=E1*D2*(0.16666667E+00-D2*(0.83333333E-02-D2*(0.198412698E-03	GOTR0120
	1-D2*(0.275573192E-05-D2*0.250521083E-07)))	GOTR0130
	F(2)=D2*(0.5-D2*(0.41666667E-1-D2*(0.13888889E-2-D2*(0.24801587E-	GOTR0140
	14-D2*0.27557319E-6)))	GOTR0150
	F(3)=E1-F(1)	GOTR0160
	F(4)=1.-F(2)	GOTR0170
	GO TO 3	GOTR0180
31	CONTINUE	GOTR0190
	F(3)=SINF(E1)	GOTR0200
	F(4)=COSF(E1)	GOTR0210
	F(1)=E1-F(3)	GOTR0220
	F(2)=1.-F(4)	GOTR0230
	GO TO 3	GOTR0240
2	CONTINUE	GOTR0250
C	FIRST GUESS IS OBTAINED FOR HYPERBOLIC CASE	GOTR0260
9	CONTINUE	GOTR0270
	IF(E1=1.)32,33,33	GOTR0280
32	CONTINUE	GOTR0290
	D2=E1*E1	GOTR0300
	F(1)=E1*D2*(0.16666667E+00+D2*(0.83333333E-02+D2*(0.198412698E-03	GOTR0310
	1+D2*(0.275573192E-05+D2*0.250521083E-07)))	GOTR0320
	F(2)=D2*(0.5+D2*(0.41666667E-1+D2*(0.13888889E-2+D2*(0.24801587E-	GOTR0330
	1-4+D2*0.27557319E-6)))	GOTR0340
	F(3)=E1-F(1)	GOTR0350
	F(4)=1.+F(2)	GOTR0360
	GO TO 3	GOTR0370
33	CONTINUE	GOTR0380
	EX=.5*EXPF(E1)	GOTR0390
	OX=.25/EX	GOTR0400
	F(3)=EX*OX	GOTR0410
	F(4)=EX*OX	GOTR0420
	F(1)=F(3)-E1	GOTR0430
	F(2)=F(4)-1.	GOTR0440
3	CONTINUE	GOTR0450
	CM=F(1)+C(1)*F(3)+C(2)*F(2)	GOTR0460
	DM=F(2)+C(1)*F(4)+C(2)*F(3)	GOTR0470
	DE=(VM-CM)/DM	GOTR0480
	ERROR=DE	GOTR0490

GOTOR(Cont'd)

```
      AB=ABSF(DE)
      IF(AB=1, )10,10,11
11  DE=DE/AB
10  E2=E1+DE
      IF(ABSF((E2-E1)/(E2+E1))-3.E-8)4,4,5
5   CONTINUE
      IF(N=NMAX)6,7,7
7   CONTINUE
      GO TO 4
6   CONTINUE
      N=N+1
      E1=E2
      GO TO (8,9),K
4   CONTINUE
      RETURN
      END
```

```
GOTR050
GOTR051
GOTR052
GOTR053
GOTR054
GOTR055
GOTR056
GOTR057
GOTR058
GOTR059
GOTR060
GOTR061
GOTR062
GOTR063
GOTR064
GOTR
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Subroutine: GUID

Purpose: To determine the times when guidance corrections are to be made. Compute the correction to be made and determine the error in the correction being performed. Then the subroutine updates both the state and guidance covariance matrices for the correction.

Calling Sequence:

CALL GUID

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities returned to common

Common storages used or required:

T, S, C, IC

Subroutines required:

INV3, MARX, SETN, SQRTF, TIMED

Functions required:

(FIL)(STH)

Approximate number of storages required:

1022 DEC

Theory for updating covariance matrices for a guidance correction.

The following quantities will be used in the derivation to follow.

$PAR(t_0)$ = covariance matrix of errors at injection

$\hat{x}(t)$ = estimate of state at time t

$\tilde{x}(t)$ = error in estimate of state at time t

$x(t)$ = true state at time t

$E(\tilde{x} \tilde{x}^T) = P(t)$ = covariance matrix of error in estimate at time t

The quantities \hat{x} , \tilde{x} , and x are all considered as deviation quantities from the nominal trajectory which arrives at the target in the desired manner.

Using linear theory for the deviations

$$x(t) = \Phi X(t_0)$$

where Φ is the transition matrix relating unit deviations in injection errors to deviations at time t . Then

$$PAR(t) = E(x(t) x(t)^T) = \Phi PAR(t_0) \Phi^T \quad (1)$$

where $PAR(t)$ is the covariance matrix of deviations from the nominal trajectory prior to any midcourse corrections.

Assuming we have a transition matrix which relates the vehicle state at time (t) to some desired conditions at the target, a guidance law may be derived to meet the desired end conditions. The two laws which the program can solve are: (1) Fixed Time of Arrival, and (2) Constant Energy with Respect to the Target.

$$\underline{C}(T) = \begin{pmatrix} A_1 & A_2 \end{pmatrix} \begin{pmatrix} \underline{x}(t) \\ \underline{\dot{x}}(t) \end{pmatrix} \quad (2)$$

3 x 1 3 x 6 6 x 1

where $\underline{C}(T)$ = target conditions at time T

$(A_1 \ A_2)$ = transition matrix

For Fixed Time of Arrival:

$$\underline{C}(T) = \begin{pmatrix} x(T) \\ y(T) \\ z(T) \end{pmatrix}$$

3 x 1 3 x 1

For Constant Energy with Respect to the Target:

$$\underline{C}(T) = \begin{pmatrix} \delta \ B \cdot T(T) \\ \delta \ B \cdot R(T) \\ \delta \ VINF \end{pmatrix}$$

The guidance law is derived such that the estimate of $\underline{C}(T)$, which represents deviations from the nominal trajectory at the target, is zero when the vehicle arrives at the target.

$$\underline{C}(T) = A_1 \hat{\underline{x}}(t) + A_2 \hat{\underline{\dot{x}}}(t)$$

3x1 3x3 3x1 3x3 3x1

(3)

The velocity correction is selected such that:

$$\underline{C}(T) + A_2 \dot{\underline{x}}_g = 0 = A_1 \hat{\underline{x}}(t) + A_2 \hat{\underline{x}}(t) + A_2 \dot{\underline{x}}_g \quad (4)$$

$\dot{\underline{x}}_g$ is multiplied by A_2 because as can be seen in equation (3), A_2 is a matrix of sensitivity partials relating $\underline{C}(T)$ to velocity deviations at time (t).

Solving equation 4 for $\dot{\underline{x}}_g$ yields

$$\dot{\underline{x}}_g = A_2^{-1} \underline{C}(T) = -A_2^{-1} A_1 \hat{\underline{x}}(t) - I \hat{\underline{x}}(t) \quad (5)$$

$$\dot{\underline{x}}_g = - \begin{bmatrix} A_2^{-1} A_1 & I \end{bmatrix} \begin{pmatrix} \hat{\underline{x}}(t) \\ \hat{\underline{x}}(t) \end{pmatrix} \quad (6)$$

We are interested in the covariance matrix PAR at (T), that is, at the time of arrival, since this is the covariance matrix of errors in guidance.

If we find $E(\underline{x}(t) \underline{x}(t)^T)$ after a correction, the use of equation (1) will propagate it to the target.

Let subscript (a) define the state after a correction, and subscript (b) define the state before the correction.

Then

$$\begin{pmatrix} \underline{x}_a \\ \dot{\underline{x}}_a \end{pmatrix} = \begin{pmatrix} \underline{x}_b \\ \dot{\underline{x}}_b \end{pmatrix} + \begin{pmatrix} 0 \\ \dot{\underline{x}}_g \end{pmatrix} + \begin{pmatrix} 0 \\ q \end{pmatrix}$$

where $\dot{\mathbf{x}}_g$ is the computed velocity correction and q is the error in making the correction. This is under the assumption of an impulsive correction.

Utilizing equation (5), and since $\mathbf{x}_a = \hat{\mathbf{x}}_a + \tilde{\mathbf{x}}_a$

$$\begin{pmatrix} \mathbf{x}_a \\ \dot{\mathbf{x}}_a \end{pmatrix} = \begin{pmatrix} \mathbf{I} & 0 \\ -\mathbf{A}_2\mathbf{A}_1 & 0 \end{pmatrix} \begin{pmatrix} \hat{\mathbf{x}}_b \\ \dot{\hat{\mathbf{x}}}_b \end{pmatrix} + \begin{pmatrix} \tilde{\mathbf{x}}_b \\ \dot{\tilde{\mathbf{x}}}_b \end{pmatrix} + \begin{pmatrix} 0 \\ q \end{pmatrix} \quad (7)$$

and

$$\begin{aligned} E(\mathbf{x}_a \mathbf{x}_a^T) &= \begin{bmatrix} \mathbf{I} & 0 \\ -\mathbf{A}_2\mathbf{A}_1 & 0 \end{bmatrix}_{6 \times 6} E(\hat{\mathbf{x}}_b \hat{\mathbf{x}}_b^T)_{6 \times 6} \begin{bmatrix} \mathbf{I} & 0 \\ -\mathbf{A}_2\mathbf{A}_1 & 0 \end{bmatrix}_{6 \times 6}^T + E(\tilde{\mathbf{x}}_b \tilde{\mathbf{x}}_b^T)_{6 \times 6} \\ &+ E \begin{bmatrix} 0 & (0 \quad q^T) \\ q & \end{bmatrix}_{6 \times 6} + \text{CROSS TERMS} \end{aligned}$$

The cross terms are zero because:

1. $E(\hat{\mathbf{x}} \hat{\mathbf{x}}^T) = 0$ because of using an optimum estimation procedure

2. $E(\hat{\mathbf{x}} q_s^T) = E(\hat{\mathbf{x}} \hat{\mathbf{x}}^T) E(S) = 0$

$E(\hat{\mathbf{x}} q_p^T) = E(\hat{\mathbf{x}} \hat{\mathbf{x}}^T) E(U) = 0$

for the two types of correction errors described below.

The two types of errors considered in making a guidance correction are shutoff error and pointing.

A. Shutoff Error

Let the correction by $\dot{\mathbf{x}}_g = \begin{pmatrix} v_x \\ v_y \\ v_z \end{pmatrix}$

The shutoff error is

$$\vec{\epsilon}_s = S \dot{\underline{x}}_g$$

where S is a scalar random variable which is gaussian $(0, \sigma_s)$.

B. Pointing Error

The pointing error is $\vec{\epsilon}_p = \vec{U} \times \dot{\underline{x}}_g$

where $U = (U_x, U_y, U_z)$ is a three dimensional spherical gaussian random variable with sigmas equal to σ_p and mean 0.

The two types of expected values of interest in equation (8) for the error in correction are $E(q q^T)$ and $E(\hat{x} q^T)$

$$\vec{q} = \vec{\epsilon}_p + \vec{\epsilon}_s$$

$$E(q q^T) = (\sigma_s^2 - \sigma_p^2) E(\dot{\underline{x}}_g \dot{\underline{x}}_g^T) + \sigma_p^2 E(\dot{\underline{x}}_g^T \dot{\underline{x}}_g) I$$

$$E(\hat{x} q^T) = 0$$

The two remaining expected values in equation (8) may be written as follows:

$$E(\hat{x} \hat{x}^T) = E(x - \tilde{x}) (x - \tilde{x})^T = E(x x^T) - E(x \tilde{x}^T) + E(\tilde{x} \tilde{x}^T) - E(\tilde{x} x^T)$$

$$\text{but } E(x \tilde{x}^T) = E([\hat{x} + \tilde{x}] \tilde{x}^T) = E(\tilde{x} \tilde{x}^T)$$

$$\text{since } E(\hat{x} \tilde{x}) = 0$$

$$\therefore E(\hat{x} \hat{x}^T) = E(x x^T) - E(\tilde{x} \tilde{x}^T)$$

$$E(\hat{x} \hat{x}^T) = PAR_b - P_b$$

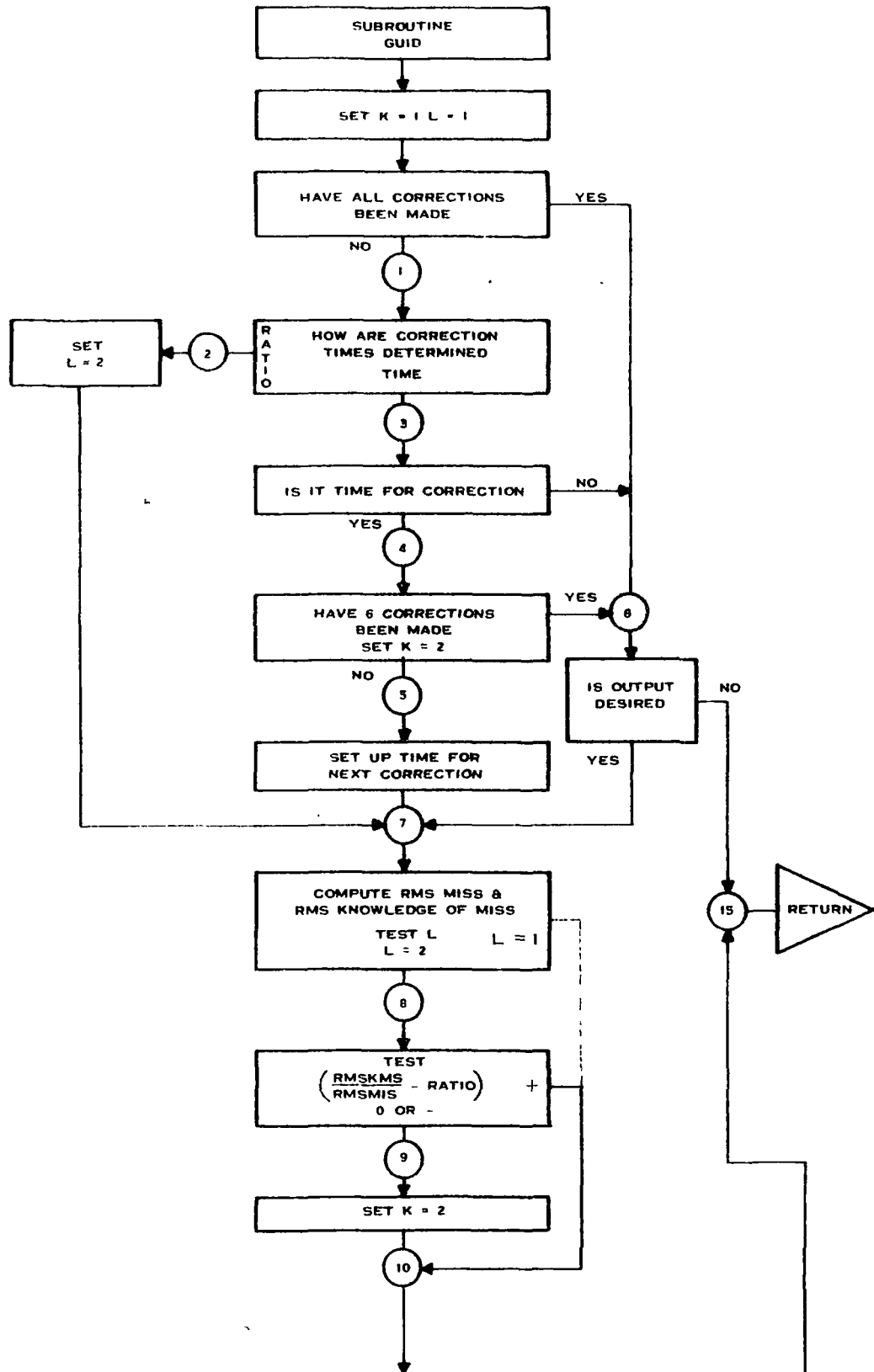
Finally

$$\begin{aligned}
 \text{PAR}_a &= \begin{bmatrix} I & 0 \\ -A_2^{-1} A_1 & 0 \end{bmatrix} \begin{bmatrix} \text{PAR}_b - P_b \end{bmatrix} \begin{bmatrix} I & 0 \\ -A_2^{-1} A_1 & 0 \end{bmatrix}^T \\
 6 \times 6 & \quad \quad 6 \times 6 \quad \quad 6 \times 6 \quad \quad 6 \times 6 \\
 &+ P_b + \begin{bmatrix} 0 & 0 \\ 0 & E(qq^T) \end{bmatrix} \\
 6 \times 6 & \quad 6 \times 6
 \end{aligned}$$

The covariance matrix of the knowledge of the state is updated to account for the lack of exact knowledge of the correction.

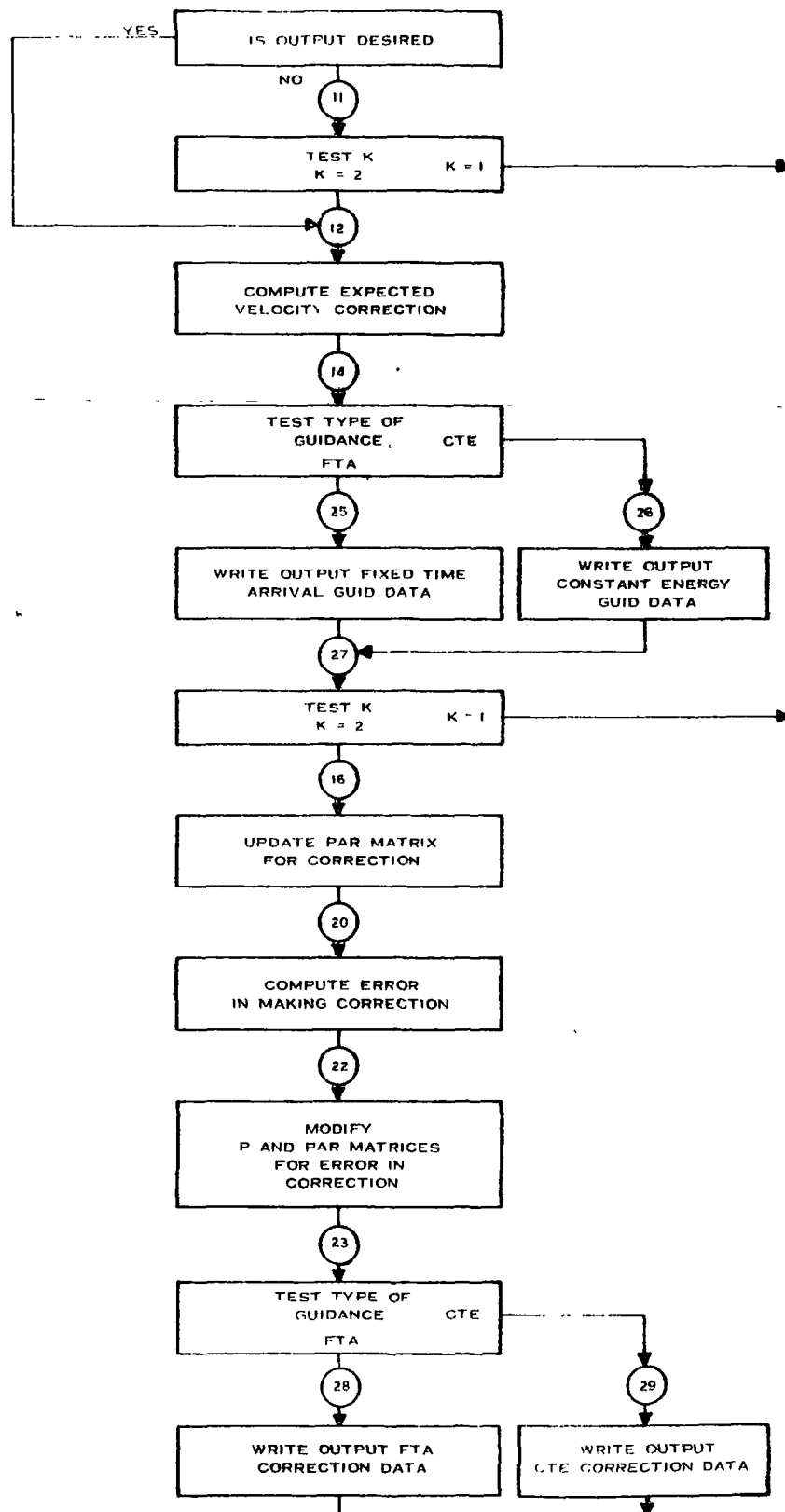
$$\begin{aligned}
 P_a &= P_b + \delta \begin{bmatrix} 0 & 0 \\ 0 & E(qq^T) \end{bmatrix} \\
 6 \times 6 \quad 6 \times 6 & \quad \quad 6 \times 6
 \end{aligned}$$

where δ indicates the ability to monitor (ON BOARD) the error in correction.



S-210

GUID-8



S-211

GUID-9

GUID

```

* LABEL
* SYMBOL TABLE
DEC2005 SUBROUTINE GUID
  SUBROUTINE GUID
  COMMON T,S,C,IC
  DIMENSION T(1360),S(1000),C(1000),IC(1)
  1,TPAR(3,6),PAR(6,6),P(6,6),DUP(3,3)
  2,TGUID(6),DUM(3,3),DUN(3,3),DUMM(6,6)
  EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM)
  1,(IC,ICDUM),(C(568),TPAR),(C(460),PAR)
  2,(C(652),P),(IC(218),N),(C(648),TGUIDE)
  3,(IC(219),IGD),(IC(217),IGDTP),(IC(214),NOUT)
  4,(C(30),TSEC),(S(476),TGUID),(S(483),RATIO)
  5,(S(473),QQPT),(S(471),QQSO),(S(484),DMONIT)
  CALL SETN(NIN,NUTS)
  IGD=NUMBER OF GUIDANCE CORRECTIONS TO BE MADE
  N KEY USED TO TEST NUMBER OF GUIDANCE CORRECTIONS WHICH HAVE
  BEEN MADE
  S(475) 0=GUIDE ON INPUT TIMES + GUIDE ON A RATIO TEST
  IGDTP 1.FTA 2.CTE 3.MINIMUM FUEL
  DMONIT=ACCURACY OF MONITORING THE GUIDANCE CORRECTION
  NOUT=NOUT
  K=1
  L=1
  IF(IGD-N)6,1,1
  1 IF(S(475))3,3,2
  2 L=2
  GO TO 7
  3 IF(TGUIDE-TSEC)4,4,6
  4 CONTINUE
  K=2
  N=N+1
  IF(N-7)5,6,6
  5 CALL TIMED(TGUID(N),TGUIDE)
  GO TO 7
  6 CONTINUE
  GO TO (15,7),NOUT
  7 CALL MATRX(TPAR,P,DUM,3,6,6,1)
  RMSKMS=SQRTF(DUM(1,1)+DUM(2,2)+DUM(3,3))
  CALL MATRX(TPAR,PAR,DUN,3,6,6,1)
  RMSMIS=SQRTF(DUN(1,1)+DUN(2,2)+DUN(3,3))
  GO TO (10,8),L
  8 IF((RMSKMS/RMSMIS)-RATIO)9,9,10
  9 K=2
  N=N+1
  10 GO TO (11,12),NOUT
  11 GO TO (15,12),K
  12 CONTINUE
  DO 13 I=1,3
  DO 13 J=1,3
  JJ=J+3

```

```

GUID
GUID
GUID
GUID0000
GUID0010
GUID0020
GUID0030
GUID0040
GUID0050
GUID0060
GUID0070
GUID0080
GUID0090
GUID0100
GUID0105
GUID0110
GUID0120
GUID0130
GUID0140
GUID0150
GUID0160
GUID0170
GUID0180
GUID0190
GUID0200
GUID0210
GUID0220
GUID0230
GUID0240
GUID0250
GUID0260
GUID0270
GUID0280
GUID0290
GUID0300
GUID0310
GUID0320
GUID0330
GUID0340
GUID0350
GUID0360
GUID0370
GUID0380
GUID0390
GUID0400
GUID0410
GUID0420
GUID0430
GUID0440
GUID0450
GUID0460

```

GUID (Cont'd)

	DUP(I,J)=-TPAR(I,JJ)	GUID047
13	CONTINUE	GUID048
	CALL INV3(DUP,3,DET)	GUID049
	DO 14 I=1,3	GUID050
	DO 14 J=1,3	GUID051
	DUM(I,J)=DUN(I,J)-DUM(I,J)	GUID052
14	CONTINUE	GUID053
	RMSPAP=SQRTF(PAR(1,1)+PAR(2,2)+PAR(3,3))	GUID054
	RMSPAV=SQRTF(PAR(4,4)+PAR(5,5)+PAR(6,6))	GUID055
	CALL MATRX(DUP,DUM,DUM,3,3,3,1)	GUID056
C	DUM IS THE COVARIANCE MATRIX OF INDICATED VELOCITY CORRECTION	GUID057
	RMSV2=DUM(1,1)+DUM(2,2)+DUM(3,3)	GUID058
	RMSV=SQRTF(RMSV2)	GUID059
	IGDTP=IGDTP	GUID059
	GO TO (25,26),IGDTP	GUID059
25	CONTINUE	GUID059
	WRITE OUTPUT TAPE NUTS,800,RMSMIS,RMSPAP,RMSKMS,RMSPAV,RMSV	GUID060
800	FORMAT(18HOGUID DATA FOLLOWS, /	GUID061
	124H RMS FTA TARGET MISS=,E15.8,	GUID062
	225H RMS POS DEV FROM NOM=,E15.8, /	GUID063
	324H RMS KNOW. OF MISS=,E15.8,	GUID064
	425H RMS VEL DEV FROM NOM=,E15.8, /	GUID065
	524H RMS VEL REQ=,E15.8)	GUID065
	GO TO 27	GUID065
26	CONTINUE	GUID065
	RMSMIS=SQRTF(DUN(1,1)+DUN(2,2))	GUID065
	RMSVIN=SQRTF(DUN(3,3))	GUID065
	WRITE OUTPUT TAPE NUTS,802,RMSMIS,RMSPAP,RMSVIN,RMSPAV,RMSKMS,RMSV	GUID066
802	FORMAT(18HOGUID DATA FOLLOWS, /	GUID066
	124H RMS TARGET POS MISS=,E15.8,	GUID066
	225H RMS POS DEV FROM NOM=,E15.8, /	GUID066
	324H RMS VINFINITY MISS=,E15.8,	GUID066
	425H RMS VEL DEV FROM NOM=,E15.8, /	GUID066
	324H RMS KNOW. OF MISS=,E15.8,	GUID066
	525H RMS VEL REQ=,E15.8)	GUID066
27	CONTINUE	GUID066
	GO TO (15,16),K	GUID067
15	RETURN	GUID068
16	CONTINUE	GUID069
C	FOLLOWING IS UPDATING OF PAR MATRIX FOR GUIDANCE CORRECTION	GUID070
	DO 17 I=1,6	GUID071
	DO 17 J=I,6	GUID072
	PAR(I,J)=PAR(I,J)-P(I,J)	GUID073
	PAR(J,I)=PAR(I,J)	GUID074
17	CONTINUE	GUID075
	CALL MATRX(DUP,TPAR,DUP,3,3,3,0)	GUID076
	DO 19 I=1,3	GUID077
	II=I+3	GUID078
	DO 18 J=1,3	GUID079
	IJJ=J+3	GUID080
	DUMM(II,J)=DUP(I,J)	GUID081

GUID (Cont'd)

	DUMM(I,JJ)=0.	GUID0820
	DUMM(II,JJ)=0.	GUID0830
18	DUMM(I,J)=0.	GUID0840
19	DUMM(I,I)=1.	GUID0850
	CALL MATRX(DUMM,PAR,PAR,6,6,6,1)	GUID0860
	DO 20 I=1,6	GUID0870
	DO 20 J=I,6	GUID0880
	PAR(I,J)=PAR(I,J)+P(I,J)	GUID0890
	PAR(J,I)=PAR(I,J)	GUID0900
20	CONTINUE	GUID0910
	CRUD=QQPT*RMSV2	GUID0920
	QQ=QQSO-QQPT	GUID0930
	DO 22 I=1,3	GUID0940
	DO 21 J=I,3	GUID0950
	DUN(I,J)=QQ*DUM(I,J)	GUID0960
	DUN(J,I)=DUN(I,J)	GUID0965
21	CONTINUE	GUID0970
	DUN(I,I)=DUN(I,I)+CRUD	GUID0980
22	CONTINUE	GUID0990
	RMSERR=SQRTF(DUN(1,1)+DUN(2,2)+DUN(3,3))	GUID1000
	DO 23 I=1,3	GUID1010
	II=I+3	GUID1020
	DO 23 J=I,3	GUID1030
	JJ=J+3	GUID1040
	PAR(II,JJ)=PAR(II,JJ)+DUN(I,J)	GUID1050
	PAR(JJ,II)=PAR(II,JJ)	GUID1060
	P(II,JJ)=P(II,JJ)+DMONIT*DUN(I,J)	GUID1070
	P(JJ,II)=P(II,JJ)	GUID1080
23	CONTINUE	GUID1090
	CALL MATRX(TPAR,PAR,DUN,3,6,6,1)	GUID1100
	RMSPAP=SQRTF(PAR(1,1)+PAR(2,2)+PAR(3,3))	GUID1105
	RMSPAP=SQRTF(PAR(1,1)+PAR(2,2)+PAR(3,3))	GUID1110
	RMSPAV=SQRTF(PAR(4,4)+PAR(5,5)+PAR(6,6))	GUID1115
	GO TO (28,29),IGDTP	GUID1120
28	CONTINUE	GUID1125
	RMSMIS=SQRTF(DUN(1,1)+DUN(2,2)+DUN(3,3))	GUID1130
	WRITE OUTPUT TAPE NUTS,801,RMSERR,RMSPAP,RMSMIS,RMSPAV	GUID1140
801	FORMAT(32H ***GUIDANCE CORRECTION MADE***,	GUID1150
	1/24H RMS ERROR IN CORR.=,E15.8,	GUID1160
	225H RMS POS DEV FROM NOM=,E15.8,	GUID1170
	3/24H RMS MIS AFT CORR.=,E15.8,	GUID1180
	425H RMS VEL DEV FROM NOM=,E15.8)	GUID1190
	GO TO 15	GUID1200
29	CONTINUE	GUID1210
	RMSMIS=SQRTF(DUN(1,1)+DUN(2,2))	GUID1220
	RMSVIN=SQRTF(DUN(3,3))	GUID1230
	WRITE OUTPUT TAPE NUTS,803,RMSERR,RMSPAP,RMSMIS,RMSPAV,RMSVIN	GUID1240
803	FORMAT(32H ***GUIDANCE CORRECTION MADE***,	GUID1250
	1/24H RMS ERROR IN CORR.=,E15.8,	GUID1260
	225H RMS POS DEV FROM NOM=,E15.8,/	GUID1270
	3/24H RMS POS MIS AFT CORR.=,E15.8,	GUID1280

GUID (Cont'd)

425H RMS VEL DEV FROM NOM=,E15.8,
5/24H RMS VINP AFT CORR.=,E15.8)
30 CONTINUE
GO TO 15
END

GUID129
GUID130
GUID131
GUID132
GUID

S-215

GUID-13

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Subroutine: HOUR

Purpose: To provide a reading of the printer clock in hours since midnight. This is the STL subroutine RW HOUR.

Calling Sequence:

CALL HOUR(A)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	A			hours	Time

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

86 cells

Restrictions

Clock advance is suppressed during readout so that elapsed time will be off .4N seconds where N is the number of times the clock is selected.

HOURL will always provide a floating point number if the printer is available. Therefore, a faulty clock or the wrong board will be indicated.

Use

The main application of HOURL is to time cases through use of the FINP "CLOCK" option.

HOUR

FAP

HOUR SUBROUTINE 10-27-31

HOUR

HOUR

ENTRY

HOUR

CLA

1,4

STA

SSAM

SXA

SAMX,4

SXA

SAMX+1,2

TCOA

*

DELAY

RPRA

ECHO CHECK

SPRA

6

READ CLOCK

SPRA

9

SUPPRESS SPACING

SPRA

10

AND PRINTING

AXT

24,4

STZ

SAMZ+24,4

TIX

*-1,4,1

RCHA

SAMIO

TRANSMIT CLOCK READING

TCOA

*

STZ

SAMZ+18

STZ

SAMZ+20

AXT

18,4

8-4 LEFT ADD ECHOS

SAM1

CAL

SAMZ+18,4

AND CONVERT TO

ORS

SAMZ+18

BCD

LDQ

SAMZ+18

PXD

AXT

5,2

SAM3

LGL

1

ALS

5

TIX

SAM3,2,1

LGL

1

ACL

SAMZ+20

SLW

SAMZ+20

TIX

SAM1,4,2

STZ

SAMZ+22

AXT

6,4

SAM4

LDQ

SAMZ+20

PXD

LGL

6

SLW

SAMZ+23

CLA

SAMZ+22

ALS

2

ADD

SAMZ+22

ALS

1

ADD

SAMZ+23

STO

SAMZ+22

TIX

SAM4,4,1

LDQ

SAMZZ

DVP

SIX

XCL

ORA

SA

FAD

SA

HOUR000

HOUR001

HOUR002

HOUR003

HOUR004

HOUR005

HOUR006

HOUR007

HOUR008

HOUR009

HOUR010

HOUR011

HOUR012

HOUR013

HOUR014

HOUR015

HOUR016

HOUR017

HOUR018

HOUR019

HOUR020

HOUR021

HOUR022

HOUR023

HOUR024

HOUR025

HOUR026

HOUR027

HOUR028

HOUR029

HOUR030

HOUR031

HOUR032

HOUR033

HOUR034

HOUR035

HOUR036

HOUR037

HOUR038

HOUR039

HOUR040

HOUR041

HOUR042

HOUR043

HOUR044

HOUR045

HOUR046

HOUR047

HOUR048

HOUR049

HOURL (Cont'd)

	CAS	M24			HOURL0500
	FSB	M24	MOD 24 HOURS		HOURL0510
	NOP		MIDNIGHT ONLY		HOURL0520
SSAM	STO	**0			HOURL0530
SAMX	AXT	**0,4			HOURL0540
	AXT	**0,2			HOURL0550
	TRA	2,4	EXIT		HOURL0560
SAMIO	IOCP	SAMZ,2+0,26	NON TRANSMIT 26 COPIES		HOURL0570
	IOCP	SAMZ,0,1	27TH COPY 9L ECHO		HOURL0580
	IOCP	SAMZ+1,2,3	NON TRANSMIT 9R,12L,12R		HOURL0590
	IOCD	SAMZ+2,0,16	8L TO 1R ECHOS		HOURL0600
SA	OCT	214000000000			HOURL0610
M24	DEC	24,			HOURL0620
SIX	DEC	6000B15			HOURL0630
SAMZZ	PZE				HOURL0640
SAMZ	BSS	24			HOURL0650
	END				HOURL0660

Subroutine: HPHT

Purpose: To perform the matrix multiplication $(RMS)^2 = H \cdot P \cdot H^T$.

The square root of $(RMS)^2$ is taken and RMS, which is the standard deviation of the parameter being considered, is output from the subroutine.

Calling Sequence:

CALL HPHT (H, P, RMS)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	H	(1,6)	$\frac{\partial \text{PAR}}{\partial \text{STATE}}$		Parameter Partial Matrix
I	P	(6,6)	$E(\vec{X} \vec{X}^T)$		State Covariance Matrix
O	RMS	1			Standard deviation of parameter
					due to state variance.

Common storages used or required:

None

Subroutines required:

None

Functions required:

SQRT

Approximate number of storages required:

HPHT

```

* LABEL
* SYMBOL TABLE
SUBROUTINE HPHT(H,P,RMS)
DIMENSION H(6),P(6,6),DUM(6)
DO 1 I=1,6
DUM(I)=0.
DO 1 J=1,6
DUM(I)=DUM(I)+H(J)*P(J,I)
1 CONTINUE
VAR2=0.
DO 2 I=1,6
VAR2=VAR2+DUM(I)*H(I)
2 CONTINUE
RMS=SQRTF(VAR2)
RETURN
END

```

```

HPHT
HPHT
HPHT0000
HPHT0010
HPHT0020
HPHT0030
HPHT0040
HPHT0050
HPHT0060
HPHT0070
HPHT0080
HPHT0090
HPHT0100
HPHT0110
HPHT0120
HPHT

```

Subroutine: INPUT

Purpose: To transform input initial conditions of position and velocity in various coordinate systems to Cartesian coordinates with respect to earth's equator and equinox of 1950. Input may be Cartesian referred to (1) mean equator and equinox, 1950; (2) true equator and equinox of date; (3) earth-fixed or spherical; (4) mean equator and equinox of 1950; (5) true equator and equinox of date; (6) earth-fixed.

Calling Sequence:

CALL INPUT (K, XOUT, VOUT, TW, TF, AN, XIN, VIN)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	K	1			Type of input: K=1 for (1) above, etc.
O	XOUT	3		see following pgs	Position, equinox 1950.0
O	VOUT	3			Velocity, equinox 1950.0
I	TW	1		days	Whole number of days past 1950.
I	TF	1		days	Fractional number of days past TW
O	AN	3,3			Transformation matrix from system (1) to (2)
I	XIN	3		see following pgs	Input position vector
I	VIN	3		see following pgs	Input velocity vector

Common storages used or required:

None

Subroutines required:

ROTEQ, NUTAIT, MULT, RVIN, INV3, GHA, SETN

Functions required:

SIN, COS

Approximate number of storages required:

Input format:For Cartesian coordinates: $[K = 1, 2, 3]$

$$XIN(1) = X$$

$$XIN(2) = Y$$

$$XIN(3) = Z$$

$$VIN(1) = \dot{X}$$

$$VIN(2) = \dot{Y}$$

$$VIN(3) = \dot{Z}$$

For sperical coordinates: $[K = 4, 5, 6]$

$$XIN(1) = R = \text{magnitude of radius vector}$$

$$XIN(2) = O = \text{declination (degrees)}$$

$$XIN(3) = \theta = \text{right ascension (degrees)}$$

$$VIN(1) = V = \text{magnitude of velocity}$$

$$VIN(2) = \gamma = \text{flight path angle (degrees)}$$

$$VIN(3) = \sigma = \text{azimuth angle (degrees)}$$

Input Transformations:

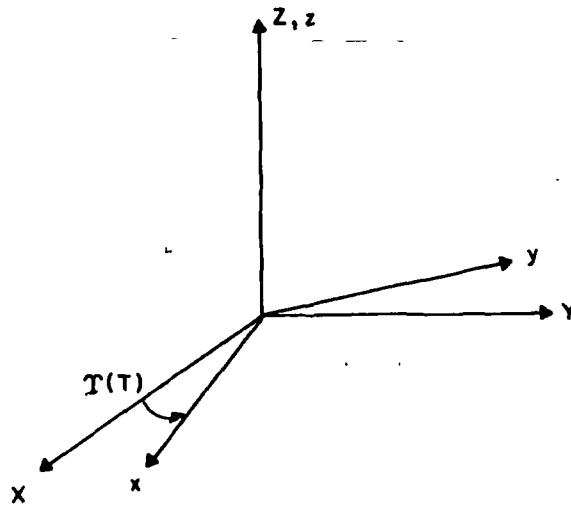
K = 1 The input is in mean equinox of 1950 and no transformation is required

$$\begin{array}{ccc} \vec{XOUT}_{50} & = & \vec{XIN}_{50} \\ 3 \times 1 & & 3 \times 1 \end{array} \quad \begin{array}{ccc} \vec{VOUT}_{50} & = & \vec{VIN}_{50} \\ 3 \times 1 & & 3 \times 1 \end{array}$$

K = 2 Subroutines ROTEQ and NUTAIT are called to obtain the transformation matrix, AN, from mean equator 1950 to true equator of date

$$\begin{array}{ccccc} \vec{XOUT}_{50} & = & (AN)^T & XIN_{DATE} & \vec{VOUT}_{50} & = & (AN)^T & \vec{VIN}_{DATE} \\ 3 \times 1 & & 3 \times 3 & 3 \times 1 & 3 \times 1 & & 3 \times 3 & 3 \times 1 \end{array}$$

K = 3 The earth fixed Cartesian coordinate system is assumed to rotate with the earth. The X-Y plane is coincident with the earth's true equator of date, the X axis lying in the Greenwich meridian and the Z axis along the earth's spin axis. Subroutine GHA is called with time, T, to obtain the Greenwich hour angle, $\gamma^{(T)}$, of the true vernal equinox of date. The transformations from earth fixed coordinates to true equator of date are the following:



X, Y, Z: TRUE EQUATOR DATE

x, y, z: EARTH FIXED

$$\begin{matrix} 3 \times 1 \\ X_{\text{DATE}} \end{matrix} = \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}_{\text{DATE}} = \begin{pmatrix} \cos \gamma & -\sin \gamma & 0 \\ \sin \gamma & \cos \gamma & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} z \\ y \\ z \end{pmatrix}_{\text{EF}}$$

and

$$V_{\text{DATE}} = \begin{pmatrix} \dot{X} \\ \dot{Y} \\ \dot{Z} \end{pmatrix}_{\text{DATE}} = \begin{pmatrix} \cos \gamma & -\sin \gamma & 0 \\ \sin \gamma & \cos \gamma & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{pmatrix}_{\text{EF}} +$$

3x1 DATE EF

$$\omega = \begin{pmatrix} -\sin \gamma & -\cos \gamma & 0 \\ \cos \gamma & -\sin \gamma & 0 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} x \\ y \\ z \end{pmatrix}_{\text{EF}}$$

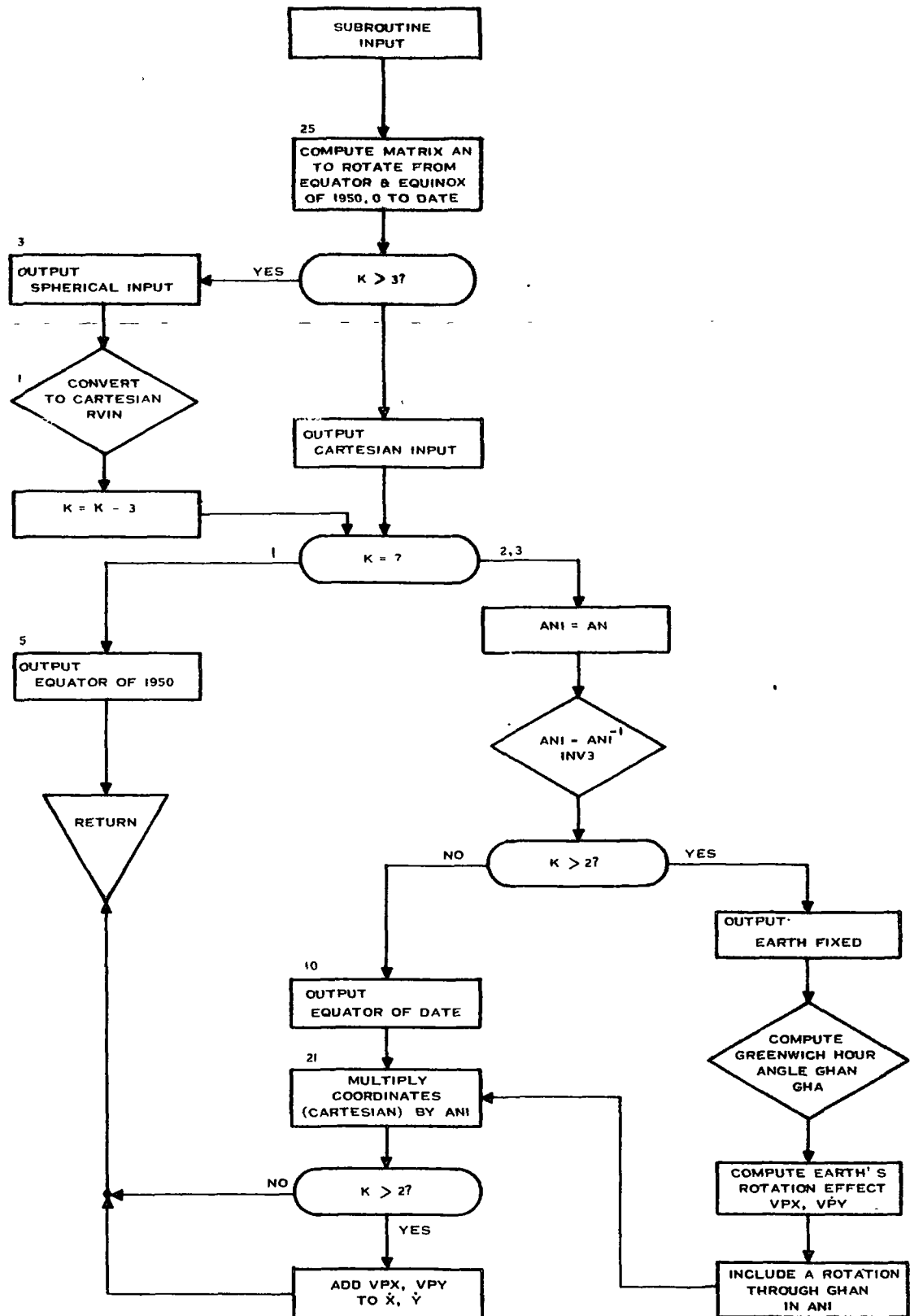
EF

where $\omega = \frac{d}{dt}\{\gamma(t)\}$ = earth's rotation rate

Subroutines ROTEQ and NUTAIT are called to obtain the AN transformation which completes the transformation to equator 1950.

$$\begin{matrix} \vec{X}_{\text{OUT}} = (\text{AN})^T \vec{X}_{\text{DATE}} & \vec{V}_{\text{OUT}} = (\text{AN})^T \vec{V}_{\text{DATE}} \\ 3 \times 1 & 3 \times 3 & 3 \times 1 & 3 \times 1 & 3 \times 3 & 3 \times 1 \end{matrix}$$

K = 4, 5, or 6 In each of these cases, subroutine RVIN is called to transform the spherical sets of coordinates to Cartesian coordinates of the same reference frame. Following this spherical to Cartesian conversion, the transformation procedures which are followed for the transformation to 1950 are identical to those described for the corresponding reference frames for K = 1, 2, or 3.



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INPUT-5

INPUT

* LABEL	INPT
* SYMBOL TABLE	INPT
CEC2013. SUBROUTINE INPUT	INPT
SUBROUTINE INPUT(K,X,V,TW,TF,AN,XIN,VIN)	INPT0000
C XIN AND VIN ARE INPUTS, X AND V ARE OUTPUTS IN EQUINOX 1950	INPT0010
C K IS TYPE INPUT (1) EQUATOR 1950; (2) EQUATOR OF DATE (3)	INPT0015
C EARTH-FIXED	INPT0016
C (4),(5),(6), ARE SPHERICAL INPUT RESP., (1),(2),(3)	INPT0020
DIMENSION X(3),V(3),SP(6),EN(3,3),A(3,3),AN(3,3),ANI(3,3),B(3,3)	INPT0030
DIMENSION XIN(3),VIN(3)	INPT0040
CALL SETN(NIN,NOUT)	INPT0045
TD = TW+TF	INPT0050
DO 25 I=1,3	INPT0060
X(I)=XIN(I)	INPT0070
V(I)=VIN(I)	INPT0080
25 CONTINUE	INPT0090
CALL ROTEQ(TD,A)	INPT0100
CALL NUTAIT (TD,OM,CRUD,DDC,EN,EPSIL)	INPT0110
CALL MULT(EN,A,AN,0)	INPT0120
IF (K-3) 4,4,3	INPT0130
4 WRITE OUTPUT TAPE NOUT,15,X,V	INPT0140
15 FORMAT(17H CARTESIAN INPUT 6E17.8)	INPT0150
GO TO 16	INPT0160
3 WRITE OUTPUT TAPE NOUT,17,X,V	INPT0170
17 FORMAT(17H SPHERICAL INPUT 6E17.8)	INPT0180
DO 2 I=1,3	INPT0190
J = I+3	INPT0200
SP(I) = X(I)	INPT0210
2 SP(J) = V(I)	INPT0220
1 CALL RVIN(SP,X,V)	INPT0230
K = K-3	INPT0240
16 DO 12 I=1,3	INPT0250
J = I+3	INPT0260
SP(I) = X(I)	INPT0270
12 SP(J) = V(I)	INPT0280
GO TO (5,7,7), K	INPT0290
5 WRITE OUTPUT TAPE NOUT,18	INPT0300
18 FORMAT(16H EQUATOR OF 1950)	INPT0310
GO TO 13	INPT0320
7 CONTINUE	INPT0330
DO 6 I=1,3	INPT0340
DO 6 J=1,3	INPT0350
6 ANI(I,J) = AN(I,J)	INPT0360
CALL INV3(ANI,3,D)	INPT0370
IF (K-2) 10,10,8	INPT0380
8 DD = EN(2,1)	INPT0390
WRITE OUTPUT TAPE NOUT,20	INPT0400
20 FORMAT(12H EARTH FIXED)	INPT0410
TS = TF*86400.	INPT0420
CALL GHA(TS,TW,GHAN,DD,OMEGA)	INPT0430
OMEGA = OMEGA*.017453296	INPT0440

[illegible]

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Subroutine: INTR, INTRI

Purpose: The purpose of INTR is to interpolate as a function of the central body on the coordinates of the other bodies, to the given time, and return the interpolated position values. The purpose of INTRI is the same as INTR, but in addition it numerically differentiates the positions to obtain the velocities and also return them.

Calling Sequence:

CALL INTR, INTRI (TW, TF, NB, PO, NV, VE, DIS)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TW	1		whole days	Time in days since 1950.0
I	TF	1		fractional days	Time in fractional days since TW
I	NB	1			Central body
O	PO	22		Km	Array of position values
I	NV	1			Dummy variable
O	VE	22		Km/sec	Array of velocity values
I	DIS	1		Km	Jupiter included if $DIS > 10^6$

Common storages used or required:

C

Subroutines required:

FIX, FLOAT

Functions required:

Approximate number of storages required: 2063 OCTAL

For interpolation, the following formula is used:

$$y(t) = \left\{ uy_0 + ty_1 \right\} + \left\{ \frac{u(u^2-1)}{3!} \delta^2 y_0 + \frac{t(t^2-1)}{3!} \delta^2 y_1 \right\} \\ + \left\{ \frac{u(u^2-1)(u^2-4)}{5!} \delta^4 y_0 + \frac{t(t^2-1)(t^2-4)}{5!} \delta^4 y_1 \right\}$$

where $y_0 = y(T_j)$

$y_1 = y(T_j + h)$

h = ephemeris interval

$$t = \frac{T - T_j}{h}$$

$u = 1 - t$

$T_j \leq T < T + h$

For the velocity values, the following is used:

$$\dot{y}(T) = \frac{1}{h} \left\{ -y_0 + y_1 \right\} + \frac{1}{h} \left\{ -\frac{3u^2-1}{3!} \delta^2 y_0 + \frac{3t^2-1}{3!} \delta^2 y_1 \right\} \\ + \frac{1}{h} \left\{ -\frac{5u^4-15u^2+4}{5!} \delta^4 y_0 + \frac{5t^4-15t^2+4}{5!} \delta^4 y_1 \right\}$$

The locations of variables in the position and velocity arrays are as follows:

PO(5)	Z value of Jupiter
PO(6)	Y value of Jupiter
PO(7)	X value of Jupiter

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INTR, INTRI - 2

PO(8) - PO(10)	values of Mars
PO(11) - PO(13)	values of Venus
PO(14) - PO(16)	values of the Sun
PO(17) - PO(19)	values of the Moon
PO(20) - PO(22)	values of the Earth

The VE array is arranged the same as the PO array with velocity values in place of positions.

INTR, INTR1

FAP
 TTL JPL EPHEMERIS LOOKUP NEW ERP 6/63
 LBL INTR
 COUNT 530
 ENTRY INTR
 ENTRY INTR1
 REM CALL INTR A,B,C,D,E,F,G POSITIONS AND VELOCITIES
 REM A=ARG INTEGRAL DAYS SINCE 1950.0
 REM B=FRACTION OF DAY
 REM C=CENTRAL BODY 0=EARTH 1=MOON 2=SUN 3=VEN 4=MARS
 REM D=OUTPUT TABLE STARTING ADDRESS
 REM E=IGNORED (VELOCITY OPTION INDICATOR)
 REM F=ADDRESS OF VELOCITY TABLE
 REM G=RADIUS FROM CENTRAL BODY
 REM EPHEMERIS TAPE MUST BE MOUNTED ON A6
 INTR TXL **3,**
 INTR1 SXD VEL,4
 TXL **2,**
 STZ VEL
 CLA 1,4
 STA TAR
 CLA 2,4 FRA
 STA FRA CEN
 CLA 3,4 CEN
 STA CEN OUP
 CLA 4,4 OUP
 STA OUP VELOCITY
 CLA 6,4
 STA XN,V
 CLA 7,4
 STA RADS
 FAR CLA **
 STO TARG
 FRA CLA **
 STO TARG+1
 CEN CLA **
 ARS 18
 STO CENTER
 RADS CLA **
 STO R
 SXD TRAP,4
 SXD TRAP+1,2
 SXD HELIO-1,1
 CLA VEL
 TNZ NEU : MUST INTERPOLATE TO
 REM OBTAIN VELOCITY
 CLA CENTER
 SUB KERNO
 TNZ NEU : MUST INTERPOLATE FOR
 REM NEW CENTRAL BODY
 CLA TARG

INTR
 INTR0000
 INTR0010
 INTR0020
 INTR0030
 INTR0040
 INTR0050
 INTR0060
 INTR0070
 INTR0080
 INTR0090
 INTR0100
 INTR0110
 INTR0120
 INTR0130
 INTR0140
 INTR0150
 INTR0160
 INTR0170
 INTR0180
 INTR0190
 INTR0200
 INTR0210
 INTR0220
 INTR0230
 INTR0240
 INTR0250
 INTR0260
 INTR0270
 INTR0280
 INTR0290
 INTR0300
 INTR0310
 INTR0320
 INTR0330
 INTR0340
 INTR0350
 INTR0360
 INTR0370
 INTR0380
 INTR0390
 INTR0400
 INTR0410
 INTR0420
 INTR0430
 INTR0440
 INTR0450
 INTR0460
 INTR0470
 INTR0480
 INTR0490

INTR, INTRI(Cont'd)

SUB TARGO
 TNZ NEU
 CLA TARG+1
 SUB TARGO+1
 TZE FLEE+6
 REM
 REM
 REM
 REM
 NEU CLA TARG
 FSB TABLE
 TMI LOOKUP
 STO COM+19
 SUB 20,
 TPL LOOKUP
 CLA COM+19
 FDH 4.
 STQ COM+18
 CLA COM+18
 CALL FIX
 CALL FLOAT
 STO COM+17
 CHS
 FAD COM+18
 STO COM+1
 CLA TARG+1
 FDH 4.
 STQ COM
 CLA COM
 FAD COM+1
 STO TARG+2
 LDQ COM+19
 FMP =9,
 CALL FIX
 ADD KERNO+1
 STA GG
 LDQ COM+17
 FMP =54,
 CALL FIX
 ADD KERNO+2
 STA HH
 AXT 2*SEP,4
 STZ XN+2*SEP,4
 TIX *-1,4,1
 AXT BSEP,4
 STZ KBO+BSEP,4
 TIX *-1,4,1
 LXA CENTER,4
 PXD ,4
 COM
 PDX ,2

TIME HAS CHANGED

ANALYZE TABLE
 NEEDS AS A
 FUNCTION OF
 CENTRAL BODY

POSITION EPHEMERIS TAPE
 T-T0

(T-T0)/4.

MUST INTERPOLATE
 SO CLEAR STORAGE

SET GRAVITATIONAL
 COEFFICIENTS
 TO ZERO

INTR050
 INTR051
 INTR052
 INTR053
 INTR054
 INTR055
 INTR056
 INTR057
 INTR058
 INTR059
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 INTR061
 INTR062
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 INTR091
 INTR092
 INTR093
 INTR094
 INTR095
 INTR096
 INTR097
 INTR098
 INTR099
 INTR100

NTR, INTRI (Cont'd)

	TXH	HELIO,4,1		INTR1010
GEO	AXT	3,1		INTR1020
	CLA	GRAV+3,1		INTR1030
	STO	KBO+3,1		INTR1040
	TIX	*-2,1,1		INTR1050
	STZ	KBO-1,2		INTR1060
	CLA	EWORTO		INTR1070
	STO	EWORT		INTR1080
	CLA	HWORTE		INTR1090
	STO	HWORT		INTR1100
	TXH	GG12,4,0		INTR1110
	CLA	RJ	TEST FOR	INTR1120
	SUB	R	INCLUSION OF	INTR1130
	TPL	GG12	JUPITER IF	INTR1140
	CLA	HWORTJ	EARTH IS	INTR1150
	STO	HWORT	CENTRAL BODY	INTR1160
	CLA	GRAV+6		INTR1170
	STO	KB6		INTR1180
	TXL	GG12,,**		INTR1190
HELIO	AXT	BSEP,1		INTR1200
	CLA	GRAV+BSEP,1		INTR1210
	STO	KBO+BSEP,1		INTR1220
	TIX	*-2,1,1		INTR1230
	STZ	KB2-3,2		INTR1240
ORTHO	CLA	EWORTO		INTR1250
	STO	EWORT		INTR1260
	CLA	HWORTO		INTR1270
	STO	HWORT		INTR1280
GG12	CLA	VEL	CHECK	INTR1290
	TZE	GG6	FOR VELOCITY	INTR1300
	CLA	EWORTO	OPTIONS	INTR1310
	STO	EWORT		INTR1320
	CLA	HWORTV		INTR1330
	STO	HWORT		INTR1340
GG6	CLA	EWORT		INTR1350
	TZE	GG+2		INTR1360
	CLA	EVEL		INTR1370
	STO	VEL+1		INTR1380
	CLA	TARG+1	GEOCENTRIC	INTR1390
	TSX	TAB,4	INTERPOLATION	INTR1400
GG	PZE	**,,9		INTR1410
	PZE	XN,,EWORT+1		INTR1420
	CLA	HWORT		INTR1430
	TZE	HH+2		INTR1440
	CLA	HVEL		INTR1450
	STO	VEL+1		INTR1460
	CLA	TARG+2	HELIOCENTRIC	INTR1470
	TSX	TAB,4	INTERPOLATION	INTR1480
HH	PZE	**,,54		INTR1490
	PZE	XN+3,,HWORT+1		INTR1500
RESET	AXT	3,4	PLACE	INTR1510

INTR, INTRI (Cont'd)

CLA XN+6,4
 FDH EVEL
 STQ XN,+18,4
 CLA XN+9,4
 FDH EVEL
 STQ XN,+12,4
 LDQ XN+3,4
 STQ XN+6,4
 FMP MU
 FSB XN+18,4
 STO XN+9,4
 STZ XN+3,4
 LDQ XN,+3,4
 STQ XN,+6,4
 FMP MU
 FSB XN,+18,4
 STO XN,+9,4
 STZ XN,+3,4
 TIX RESET+1,4,1
 LXA CENTER,4
 LXD VEL,2
 TXH RVPRT,2,0
 TXH TESTM,4,0
 NZT KB6
 TRA FLEE
 AXT 3,1
 CLA XN+21,1
 FAD XN+9,1
 STO XN+21,1
 TIX *-3,1,1
 TXL FLEE
 TESTM TXH RVPRT,4,1
 AXT 3,1
 CLS XN+6,1
 STO XN+3,1
 CLA XN+9,1
 FSB XN+6,1
 STO XN+9,1
 STZ XN+6,1
 TIX *-6,1,1
 FLEE CLA CENTER
 STO KERN
 CLA TARG
 STO TARGO
 CLA TARG+1
 STO TARGO+1
 AXT 21,1
 CLA XN+21,1
 OUP STO **,1
 TIX OUP-1,1,1
 CLA VEL

COORDINATES
 IN OLD
 FORMAT

POSITION OF SUN

VELOCITY OF SUN

IX2 NOT ZERO IF VELOCITY OPTION
 GET COORDINATES FOR PRINTING

EARTH-CENTERED

MOON-CENTERED

TRANSFER POSITIONS

INTR1520
 INTR1530
 INTR1540
 INTR1550
 INTR1560
 INTR1570
 INTR1580
 INTR1590
 INTR1600
 INTR1610
 INTR1620
 INTR1630
 INTR1640
 INTR1650
 INTR1660
 INTR1670
 INTR1680
 INTR1690
 INTR1700
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 INTR1800
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 INTR1870
 INTR1880
 INTR1890
 INTR1900
 INTR1910
 INTR1920
 INTR1930
 INTR1940
 INTR1950
 INTR1960
 INTR1970
 INTR1980
 INTR1990
 INTR2000
 INTR2010
 INTR2020

INTR, INTRI (Cont'd)

	TZE	OUT
	AXT	21,1
	CLA	XN,+21,1
(N,V	STO	++,1
	TIX	XN,V-1,1,1
OUT	LXD	HELIO-1,1
	LXD	TRAP+1,2
	LXD	TRAP,4
	TRA	8,4
	REM	TSX TAB,4
	REM	PZE B,,K
	REM	PZE A,,C
	REM	
	REM	
	REM	
AB	SXD	COM+9,4
	SXD	COM+8,2
	SXD	COM+7,1
	STO	ARG
	CLA	1,4
	STA	TAB18
	LRS	18
	ADD	1,4
	STA	TAB21
	CLA	2,4
	PAX	,1
	TXI	++1,1,SEP
	SXA	TAB29,1
	ARS	18
	STA	VELOP
	AXT	2,1
	CLA	VEL
	TNZ	VELOP
	TXI	VELOP,1,-1
VELOP	CLA	++,1
	STO	VEL+2
	TXL	POSOP,1,1
	REM	
	CLA	ARG
	TSX	COEFF.,4
	AXT	3,4
	CLS	COM+13,4
	STO	COM+16,4
	TIX	*-2,4,1
	CLA	1,
	FSB	ARG
	TSX	COEFF.,4
	TRA	TAB1-1
	REM	
OSOP	CLA	ARG

DO NOT TRANSFER VELOCITY

TRANSFER VELOCITIES

(AC)=INTERPOLATIVE ARGUMENT

B=START OF DATA BLOCK

K=WORDS PER SUB BLOCK

A=START OF RESULT BLOCK

C=SKIP CODE WORD LOCATION

PICK UP SKIP
CODE WORD

VELOCITY OPTION

FORM THE
E1(2J).FORM THE
E0(2J).

POSITION OPTION

INTR2030
INTR2040
INTR2050
INTR2060
INTR2070
INTR2080
INTR2090
INTR2100
INTR2110
INTR2120
INTR2130
INTR2140
INTR2150
INTR2160
INTR2170
INTR2180
INTR2190
INTR2200
INTR2210
INTR2220
INTR2230
INTR2240
INTR2250
INTR2260
INTR2270
INTR2280
INTR2290
INTR2300
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INTR2360
INTR2370
INTR2380
INTR2390
INTR2400
INTR2410
INTR2420
INTR2430
INTR2440
INTR2450
INTR2460
INTR2470
INTR2480
INTR2490
INTR2500
INTR2510
INTR2520
INTR2530

INTR, INTRI (Cont'd)

TSX COEFF,4
 AXT 3,4
 CLA COM+13,4
 STO COM+16,4
 TIX *-2,4,1
 CLA 1.
 FSB ARG
 TSX COEFF,4
 LXA TAB29,4
 TXI **1,4,-SEP
 SXA TAB29,4
 SXD COM+4,1
 TAB1 AXT 0,3
 LDQ VEL+2
 PXD
 LGL 2.
 PAX ,4
 STQ VEL+2
 CAL =03
 ORS VEL+2
 TXH END,4,2
 TXH FORT,4,0
 TXI **1,1,-3
 TXI TAB1+1,2,-1
 FORT AXT 3,4
 TAB18 LDQ **,1
 FMP COM+13,4
 STO COM
 TAB21 LDQ **,1
 FMP COM+16,4
 FAD COM
 STO COM+4,4
 TXI **1,1,-1
 TIX *-8,4,1
 FAD COM+2
 FAD COM+1
 TAB29 STO **,2
 TXI TAB1+1,2,-1
 END LXD COM+4,1
 TIX VELOP,1,1
 LXD COM+9,4
 LXD COM+8,2
 LXD COM+7,1
 TRA 3,4
 COEFF STO COM+10
 LDQ COM+10
 FMP COM+10
 STO COM+12
 FSB 1.
 FDH 6.
 FMP COM+10

FORM THE
 E1(2J)

FORM THE
 E0(2J)

X(0)

X(1)

X(T)

CALCULATE
 POSITION
 COEFFICIENTS
 FOR EVERETT,S
 INTERPOLATION
 FORMULA

INTR254
 INTR255
 INTR256
 INTR257
 INTR258
 INTR259
 INTR260
 INTR261
 INTR262
 INTR263
 INTR264
 INTR265
 INTR266
 INTR267
 INTR268
 INTR269
 INTR270
 INTR271
 INTR272
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 INTR294
 INTR295
 INTR296
 INTR297
 INTR298
 INTR299
 INTR300
 INTR301
 INTR302
 INTR303
 INTR304

INTR, INTRI (Cont'd)

INTR3050
INTR3060
INTR3070
INTR3080
INTR3090
INTR3100
INTR3110
INTR3120
INTR3130
INTR3140
INTR3150
INTR3160
INTR3170
INTR3180
INTR3190
INTR3200
INTR3210
INTR3220
INTR3230
INTR3240
INTR3250
INTR3260
INTR3270
INTR3280
INTR3290
INTR3300
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INTR3450
INTR3460
INTR3470
INTR3480
INTR3490
INTR3500
INTR3510
INTR3520
INTR3530
INTR3540
INTR3550

CALCULATE
VELOCITY
COEFFICIENTS
FOR EVERETT,S
INTERPOLATION
FORMULA

EXPRESS ALL
BODIES GEOCENTRICALLY

BUFFER
CENTRAL
BODY

STO COM+11
CLA COM+12
FSB 4.
FDH 20.
FMP COM+11
STO COM+12
TRA 1,4
DOEFF, STO COM
CLS 1.
FDH VEL+1
STO COM+10
LDQ COM
FMP COM
STO COM+12

XCA
FMP 3.
FSB 1.
FDH 6.
FMP COM+10
STO COM+11
CLA COM+12
FSB 3.

XCA
FMP 5.
XCA
FMP COM+12
FAD 4.
FDH 120.
FMP COM+10
STO COM+12

TRA 1,4
RVPRT AXT 0,2
AXT 3,5
CLA XN+9,2
FAD XN+9,4
STO XN+9,2
CLA VEL
TZE ++4

CLA XN,+9,2
FAD XN,+9,4
STO XN,+9,2
TXI ++1,2,-1
TIX RVPRT+2,4,1
TXH RVPRT+1,2,9-SEP
CLA CENTER
ALS 1
ADD CENTER
PAC ,4
CLA XN,4
STO COM+3,1
CLA XN,,4

INTR, INTRI (Cont'd)

STO COM+6,1
 TXI **1,4,-1
 TIX *-5,1,1
 RVPRT1 AXT 0,2
 AXT 3,4
 CLA XN,2
 FSB COM+3,4
 STO XN,2
 CLA VEL
 TZE **4
 CLA XN,,2
 FSB COM+6,4
 STO XN,,2
 TXI **1,2,-1
 TIX RVPRT1+2,4,1
 TXH RVPRT1+1,2,-SEP
 TXL FLEE
 LOOKUP CLA TLAST
 FSB TARG
 TNZ **2
 TRA ERR1
 TMI *-1
 CLA TARG
 FSB TFIRST
 TPL **2
 TRA ERR1
 FDH 20,
 XCA
 CALL FIX
 CALL FLOAT
 XCA
 FMP 20,
 FAD TFIRST
 STO COM+1
 CLA TABLE
 FSB COM+1
 TMI FINDIT
 FDH 20,
 XCA
 CALL FIX
 ADD 1F
 PAX ,4
 TEFA **1
 TXL **3,4,20
 REWA 6
 TRA FINDIT
 BSRA 6
 TIX *-1,4,1
 FINDIT AXT 10,2
 SDHA 6
 RTBA 6

EXPRESS ALL
 BODIES IN TERMS
 OF THE CENTRAL
 BODY

TIME ON RECORD

RECORDS TO
 BE BACKED

OVER

INTR356
 INTR357
 INTR358
 INTR359
 INTR360
 INTR361
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 INTR364
 INTR365
 INTR366
 INTR367
 INTR368
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 INTR404
 INTR405
 INTR406

INTR, INTRI (Cont'd)

	RCHA	IO		INTR4070
	TCOA	*		INTR4080
	TEFA	ERR1		INTR4090
	CLA	TABLE		INTR4100
	SUB	COM+1		INTR4110
	TMI	++2		INTR4120
	TNZ	LOOKUP	TAPE NOT POSITIONED PROPERLY	INTR4130
	TNZ	FINDIT		INTR4140
	AXT	513,4		INTR4150
	CAL	TABLE	CHECK	INTR4160
	ACL	A+513,4	SUM	INTR4170
	TIX	*-1,4,1		INTR4180
	TRCA	BSRA		INTR4190
	LAS	C		INTR4200
	TRA	++2		INTR4210
	TRA	SCALE		INTR4220
BSRA	BSRA	6		INTR4230
	TIX	FINDIT+1,2,1		INTR4240
	CALL	ERP		INTR4250
IO	IOCD	TABLE,,515		INTR4260
ERR1	CALL	ERPT		INTR4270
	PZE	TARG		INTR4280
	REM		SCALING	INTR4290
	REM		LOOP	INTR4300
SCALE	AXT	189,4		INTR4310
	LDQ	A+189,4	SCALE	INTR4320
	FMP	SCALE1	GEOCENTRIC	INTR4330
	STO	A+189,4	EPHEMERIS	INTR4340
	TIX	*-3,4,1		INTR4350
	AXT	324,4	SCALE	INTR4360
	LDQ	B+324,4	HELIOCENTRIC	INTR4370
	FMP	SCALE2	EPHEMERIS	INTR4380
	STO	B+324,4		INTR4390
	TIX	*-3,4,1		INTR4400
	CLA	GRAV	COMPUTE	INTR4410
	FAD	GRAV+1	MASS RATIO	INTR4420
	STO	COM	OF MOON	INTR4430
	CLA	GRAV+1	TO EARTH-MOON	INTR4440
	FDH	COM	BARYCENTER	INTR4450
	STQ	MU	FOR POSITION OF EARTH	INTR4460
	TRA	NEU		INTR4470
SCALE1	DEC	6378.150	EARTH RADIUS	INTR4480
SCALE2	DEC	149598500.	ASTRONOMICAL UNIT (JPL, JULY 1961	INTR4490
IFIRST	DEC	3892.0	0 HR AUG 28, 1960 JD = 2437174,5	INTR4500
FLAST	DEC	7292.0	0 HR DEC 19, 1969 JD = 2440554,5	INTR4510
IRAP	PZE			INTR4520
	PZE			INTR4530
RJ	DEC	1E6	JUPITER TEST DISTANCE	INTR4540
TEMPDT	DEC	34,	E.T.-U.T.	INTR4550
	PZE			INTR4560
GRAV	DEC	3.98602E5	EARTH	INTR4570

INTR, INTRI (Cont'd)

DEC 4.8983349E3
 DEC 1.3252312E11
 DEC 3.2429889E5
 DEC 4.2915518E4
 DEC 0
 DEC 1.2652701E8
 DEC 86400.
 DEC 345600.

MU PZE
 OCT 000000520052
 HWORT OCT 0
 OCT 527777777777

EWORT OCT 0
 HWORTJ OCT 000000005252
 HWORTE OCT 000000005200
 EWORTO OCT 527777777777
 HWORTO OCT 000052525252
 HWORTV OCT 525252525252
 TARGO DEC 20.,0

KERNO PZE
 PZE A
 PZE B

ARG PZE 0
 1F DEC 1
 1. DEC 1.

3. DEC 3.
 4. DEC 4.
 5. DEC 5.

6. DEC 6.
 20. DEC 20.
 120. DEC 120.

86400. DEC 86400.
 VEL BSS 3

*
 TABLE DEC 0
 A BSS 189
 B BSS 324
 C BSS 1

*
 TARG PZE
 PZE
 PZE

CENTER PZE
 COM BSS 21
 VAFLG PZE
 FQFLG BSS 3

KB0 PZE
 KB1 PZE
 KB2 PZE
 KB3 PZE
 KB4 PZE

MOON
 SUN
 VENUS
 MARS
 REMOVE BARYCENTER
 JUPITER

MASS RATIO OF MOON TO BARYCENTER
 MARS, JUPITER VELOCITY

MOON VELOCITY

BARYCENTER, JUPITER
 BARYCENTER

FORMER TIME
 FORMER CENTER
 GEOCENTRIC REFERENCE
 HELIOCENTRIC REFERENCE

VELOCITY OPTION,H,SKIP CODE

RESERVE
 FOR
 WORKING
 EPHEMERIS

INTR458
 INTR459
 INTR460
 INTR461
 INTR462
 INTR463
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 INTR506
 INTR507
 INTR508

INTR, INTRI (Cont'd)

KB5	PZE	
KB6	PZE	
XN	BSS	21
XN.	BSS	21
T	PZE	
	PZE	
R	PZE	
BSEP	SYN	7
SEP	SYN	XN, - XN
	END	

INTR5090
INTR5100
INTR5110
INTR5120
INTR5130
INTR5140
INTR5150
INTR5160
INTR5170
INTR

Subroutine: INV3

Purpose: To invert a matrix of any dimension up to a 6 by 6.

Calling Sequence:

CALL INV3 (A, N, DETERM)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
IO	A	6,6			A(I) Matrix to be inverted
					A(0) Inverse of input matrix
I	N	1			Dimension of input matrix
O	DETERM	1			Matrix determinant

Common storages used or required:

None

Subroutines required:

None

Functions required:

ABS

Approximate number of storages required:

INV3

```

* LABEL INV3
C SUBROUTINE FOR INVERTING SQUARE MATRICES WHICH ARE 6 BY 6 OR LESS INV30000
C (TO INVERT LARGER MATRICES, SAY M BY M, DIMENSION IPIVOT(M), A(M*M), INV30010
C INDEX(M,2), PIVOT(M) AND RECOMPILE) INV30020
C A IS THE SQUARE MATRIX TO BE INVERTED INV30030
C N IS THE SIZE OF A (A IS AN N BY N MATRIX) INV30040
C THE SUBROUTINE RETURNS A INVERSE IN PLACE OF A AND THE DETERMINANT INV30050
C IN DETERM. INV30060
C SUBROUTINE INV3(A,N,DETERM) INV30070
C DIMENSION IPIVOT(6), A(36), INDEX(6,2), PIVOT(6) INV30080
C EQUIVALENCE (IROW,JROW), (ICOLUMN,JCOLUMN), (AMAX,T,SWAP) INV30090
C DETERM=1.0 INV30100
C DO 20 J=1,N INV30110
20 IPIVOT(J)=0 INV30120
C DO 550 I=1,N INV30130
C AMAX=0.0 INV30140
C DO 105 J=1,N INV30150
C IF(IPIVOT(J)-1) 60,105,60 INV30160
60 DO 100 K=1,N INV30170
C IF(IPIVOT(K)-1) 80,100,740 INV30180
80 M = N*(K-1)+J INV30190
C IF (ABSF(AMAX)-ABSF(A(M))) 85,100,100 INV30200
85 IROW=J INV30210
C ICOLUMN=K INV30220
C AMAX = A(M) INV30230
100 CONTINUE INV30240
105 CONTINUE INV30250
C IPIVOT(ICOLUMN)=IPIVOT(ICOLUMN)+1 INV30260
C IF(IROW-ICOLUMN) 140,260,140 INV30270
140 DETERM=-DETERM INV30280
C DO 200 L=1,N INV30290
C M = N*(L-1) INV30300
C M1 = M+ICOLUMN INV30310
C M = M+IROW INV30320
C SWAP = A(M) INV30330
C A(M) = A(M1) INV30340
200 A(M1) = SWAP INV30350
260 INDEX(I,1)=IROW INV30360
C INDEX(I,2)=ICOLUMN INV30370
C M = N*(ICOLUMN-1)+ICOLUMN INV30380
C PIVOT(I) = A(M) INV30390
C DETERM=DETERM*PIVOT(I) INV30400
C A(M) = 1.0 INV30410
C DO 350 L=1,N INV30420
C M = N*(L-1)+ICOLUMN INV30430
350 A(M) = A(M)/PIVOT(I) INV30440
C DO 550 L1=1,N INV30450
C IF(L1-ICOLUMN) 400,550,400 INV30460
400 M = N*(ICOLUMN-1)+L1 INV30470
C T = A(M) INV30480
C A(M) = 0. INV30490

```

INV3 (Cont'd)

```

DO 450 L=1,N
M = N*(L-1)
M1 = M+ICOLUM
M = M+L1
450 A(M) = A(M)-A(M1)*T
550 CONTINUE
DO 710 I=1,N
L=N+1-I
IF(INDEX(L,1)-INDEX(L,2)) 630,710,630
630 JROW=INDEX(L,1)
JCOLUM=INDEX(L,2)
M = N*(JROW-1)
M1 = N*(JCOLUM-1)
DO 705 K=1,N
M = M+1
M1 = M1+1
SWAP = A(M)
A(M) = A(M1)
A(M1) = SWAP
705 CONTINUE
710 CONTINUE
740 RETURN
END

```

INV3050
 INV3051
 INV3052
 INV3053
 INV3054
 INV3055
 INV3056
 INV3057
 INV3058
 INV3059
 INV3060
 INV3061
 INV3062
 INV3063
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 INV3066
 INV3067
 INV3068
 INV3069
 INV3070
 INV3071
 INV3

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Subroutine: INVAO

Purpose: To form the inverse of a transition matrix for a linear, conservative dynamic system. If Φ is a partitioned matrix such as

$$\Phi = \begin{pmatrix} \Phi_1 & \Phi_2 \\ \Phi_3 & \Phi_4 \end{pmatrix} \quad \text{then INVAO computes } \Phi^{-1} = \begin{pmatrix} \Phi_4^T & -\Phi_2^T \\ -\Phi_3^T & \Phi_1^T \end{pmatrix}$$

Calling Sequence:

CALL INVAO (AO, AOI)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	AO	6,6	$\Phi(t_2, t_1)$		Transition Matrix
O	AOI	6,6	$\Phi^{-1}(t_2, t_1)$		Inverse Transition Matrix

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

INVAO

```

* LABEL
* SYMBOL TABLE
SUBROUTINE INVAO(AO,AOI)
DIMENSION AO(6,6),AOI(6,6)
DO 1 I=1,3
  II=I+3
  DO 1 J=1,3
    JJ=J+3
    AOI(I,J)=AO(JJ,II)
    AOI(II,J)=-AO(JJ,I)
    AOI(II,JJ)=AO(J,I)
1  AOI(I,JJ)=-AO(J,II)
RETURN
END

```

```

INVA
INVA
INVA0000
INVA0010
INVA0020
INVA0030
INVA0040
INVA0050
INVA0060
INVA0070
INVA0080
INVA0090
INVA0100
INVA

```


Subroutine: LOADO

Purpose: To transfer the transition matrix from its storage in the integration package's T block to the matrix in the call list.

Calling Sequence:

CALL LOADO (AO)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
0	AO	(6,6)	$\Phi(t_2 t_1)$		Transition Matrix

Common storages used or required:

T

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

LOADO

```

* LABEL
* SYMBOL TABLE
SUBROUTINE LOADO(AC)
COMMON T
DIMENSION T(1360),AO(6,6)
K=6
JJ=27
DO1 I=1,6
DO 1 J=1,3
K=K+1
KK=J+3
JJ=JJ+1
AO(KK,I)=T(JJ)
AO(J,I)=T(K)
1 CONTINUE
RETURN
END

```

```

LOAD
LOAD
LOAD0000
LOAD0010
LOAD0020
LOAD0030
LOAD0040
LOAD0050
LOAD0060
LOAD0070
LOAD0080
LOAD0090
LOAD0100
LOAD0110
LOAD0120
LOAD0130
LOAD

```

Subroutine: LOADT

Purpose: To place unit initial conditions in the T block for the
variational equations which are being used to generate the transition matrix.

Calling Sequence:

CALL LOADT

Input and Output

Common storages used or required:

T

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

LOADT

```

* LABEL
* SYMBOL TABLE
SUBROUTINE LOADT
C SUBROUTINE LOADT PUTS UNIT ICS ON PERTURBATION EQUATIONS
COMMON T
DIMENSION T(1360),X(3,6),V(3,6)
EQUIVALENCE (T(7), X),(T(28),V)
DO 2 I=1,3
  L=I+3
  DO 1 J=1,3
    K=J+3
    X(I,J)=0.
    V(I,K)=0.
    X(I,K)=0.
    V(I,J)=0.
1 CONTINUE
  X(I,I)=1.
  V(I,L)=1.
2 CONTINUE
RETURN
END

```

```

LOAT
LOAT
LOAT0000
LOAT0010
LOAT0020
LOAT0030
LOAT0040
LOAT0050
LOAT0060
LOAT0070
LOAT0080
LOAT0090
LOAT0100
LOAT0110
LOAT0120
LOAT0130
LOAT0140
LOAT0150
LOAT0160
LOAT0170
LOAT

```

Subroutine: MASS

Purpose: To find the relevant gravitational constants to be used in computing planetary perturbations for a given central body. MASS also chooses the initial integration step size as a function of central body.

Calling Sequence:

CALL MASS (NOR, UM, VKB, X, ACCP)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	NOR	1			Central Body Indicator.
					1=Earth; 2, Moon; 3, Sun; 4,
					Venus; 5, Mars; 6, Jupiter
I	UM	6	μ_i	Km^3/sec^2	Gravitational constants, arranged
					as above
O	VKB	6	μ_i	Km^3/sec^2	μ_i for bodies
I	X	3	X,Y,Z	Km	Position coordinates
O	ACCP	1		seconds	Initial integration step size

Common storages used or required:

None

Subroutines required:

None

Functions required:

FNORM

Approximate number of storages required:

Method of Establishing Integration Step Size and Perturbing Bodies

Central Body	Integration Step Size	Other Bodies to be Considered
Earth	60.0	Moon, Sun. If $ X \geq 10^6$ Km, Jupiter.
Moon	60.0	Earth, Sun.
Sun	43200.0	All
Venus, Mars, Jupiter	60.0	All

The bodies which are not to be used in calculation of perturbation accelerations are eliminated from consideration by placing zeros in array VKB(6). For the bodies which are being considered, the appropriate gravitational constant is placed in VKB(6).

MASS

```

* LABEL
* SYMBOL TABLE
SUBROUTINE MASS(NOR,UM,VKB,X,ACCP)
DIMENSION UM(6),VKB(6),X(3)
N = NOR
DO 1 I=1,6
1 VKB(I) = 0.
GO TO (2,3,6,4,4,4),N
2 VKB(2) = UM(2)
ACCP = 60.
DIS = FNORM(X)
VKB(3) = UM(3)
IF (DIS=10.000000.) 11,10,10
10 VKB(6) = UM(6)
GO TO 12
11 VKB(6) = 0.
12 RETURN
3 VKB(1) = UM(1)
VKB(3) = UM(3)
ACCP = 60.
RETURN
6 ACCP = 43200.
GO TO 7
4 ACCP = 60.
7 DO 5 I=1,6
5 VKB(I) = UM(I)
VKB(N) = 0.
RETURN
END

```

```

MASS
MASS
MASS000
MASS001
MASS002
MASS003
MASS004
MASS005
MASS006
MASS007
MASS008
MASS009
MASS010
MASS011
MASS012
MASS013
MASS014
MASS015
MASS016
MASS017
MASS018
MASS019
MASS020
MASS021
MASS022
MASS023
MASS024
MASS025
MASS

```

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Subroutine: MATRX

Purpose: To perform matrix multiplications of matrices with any dimensions up to maximum dimensions of 10 by 10. A zero in the call sequence (J) yields an output matrix $C = A \cdot B$. A one in the call sequence (J) yields an output matrix $C = A \cdot B \cdot A^T$. The matrix products are obtained in double precision.

Calling Sequence:

CALL MATRX (A, B, C, NRA, NCA, NCB, J)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	A	(10,10)			Input Matrix
I	B	(10,10)			Input Matrix
O	C	(10,10)			Output Matrix
I	NRA	1			Number of Rows of A
I	NCA	1			Number of Columns of A
I	NCB	1			Number of Columns of B
I	J	1			Type of multiplication desired

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

MATRIX

```

* LABEL
* SYMBOL TABLE
CEC2000 SUBROUTINE MATRX
SUBROUTINE MATRX(A,B,C,NRA,NCA,NCB,J)
C J=0 A*B=C
C J=1 A*B*AT=C T MEANS TRANSPOSE
C NRA=NUMBER OF ROWS OF A
C NCA=COLUMNS OF A
C NCB=COLUMNS OF B
C ACCUMULATION OF PRODUCTS IN DOUBLE PRECISION
DIMENSION A(100),B(100),C(100),D(100)
D DUD=0.
D DUM=0.
DO 1 I=1,NRA
DO 1 K=1,NCB
NC=I+(K-1)*NRA
D CRUD=0.
DO 2 L=1,NCA
NA=I+(L-1)*NRA
NB=L+(K-1)*NCA
DUD=A(NA)
DUM=B(NB)
D CRUD=CRUD+DUD*DUM
2 CONTINUE
D(NC)=CRUD
1 CONTINUE
IF(J)3,3,4
3 CONTINUE
KK=NCB+NRA
DO 5 I=1,KK
5 C(I)=D(I)
GO TO 10
4 CONTINUE
DO 6 I=1,NRA
DO 6 K=1,NRA
NC=I+(K-1)*NRA
D CRUD=0.
DO 7 L=1,NCA
NA=I+(L-1)*NRA
NB=K+(L-1)*NRA
DUM=D(NA)
DUD=A(NB)
D CRUD=CRUD+DUM*DUD
7 CONTINUE
C(NC)=CRUD
6 CONTINUE
10 CONTINUE
RETURN
END

```

```

MATX
MATX
MATX
MATX0000
MATX0010
MATX0020
MATX0030
MATX0040
MATX0050
MATX0060
MATX0080
MATX0090
MATX0100
MATX0110
MATX0120
MATX0130
MATX0140
MATX0150
MATX0160
MATX0170
MATX0180
MATX0190
MATX0200
MATX0210
MATX0220
MATX0230
MATX0240
MATX0250
MATX0260
MATX0270
MATX0280
MATX0290
MATX0300
MATX0310
MATX0320
MATX0340
MATX0350
MATX0360
MATX0370
MATX0380
MATX0390
MATX0400
MATX0410
MATX0420
MATX0430
MATX0440
MATX0510
MATX0520
MATX

```

Subroutine: MATSUB

Purpose: The subroutine is primarily logic which controls (1) trajectory and data printout, (2) updating of the state covariance matrix for observations by calling subroutines EARTR, ONBTR, and MONBTR, and (3) updating of the guidance covariance matrix by calling subroutine GUID.

Calling Sequence:

CALL MATSUB

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities returned to common

Common storages used or required:

T, S, C, IC

Subroutines required:

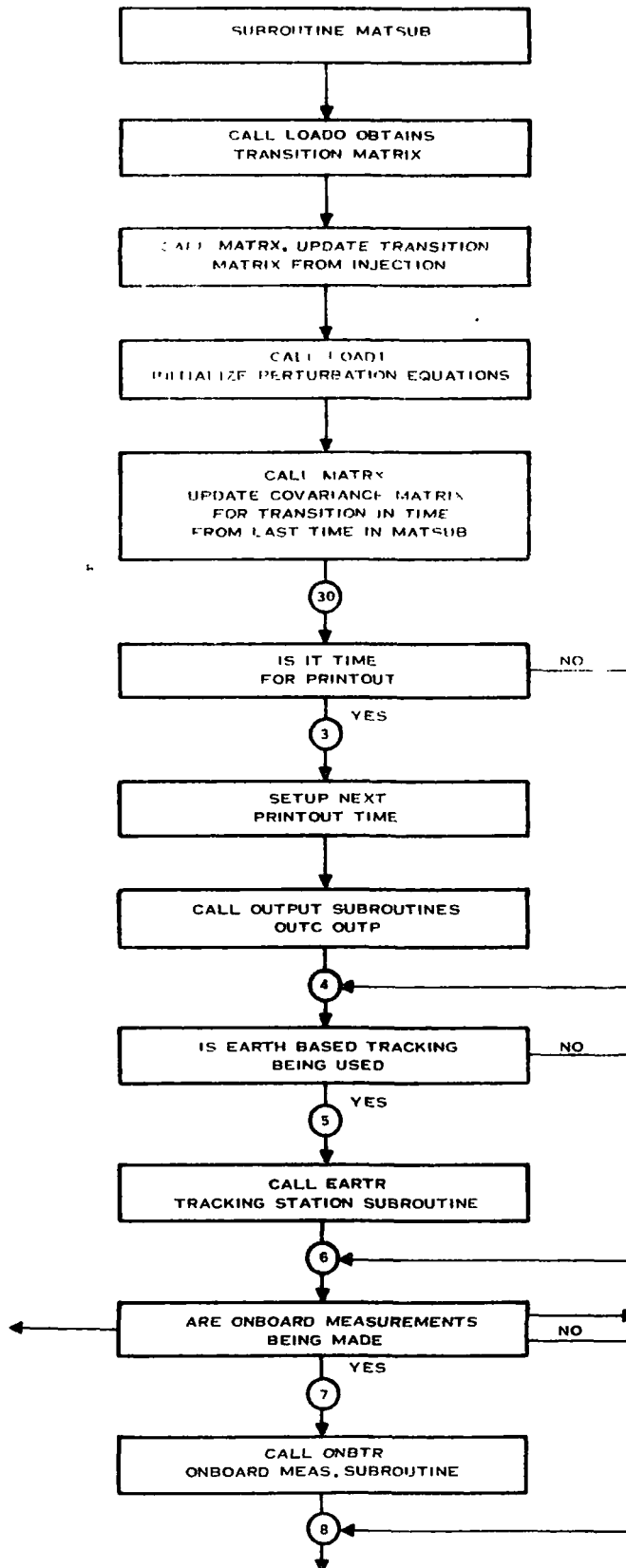
EARTR, GUID, INVAO, LOADO, LOADT, MATRX, MONBTR, ONBTR, OUTC, OUTP

Functions required:

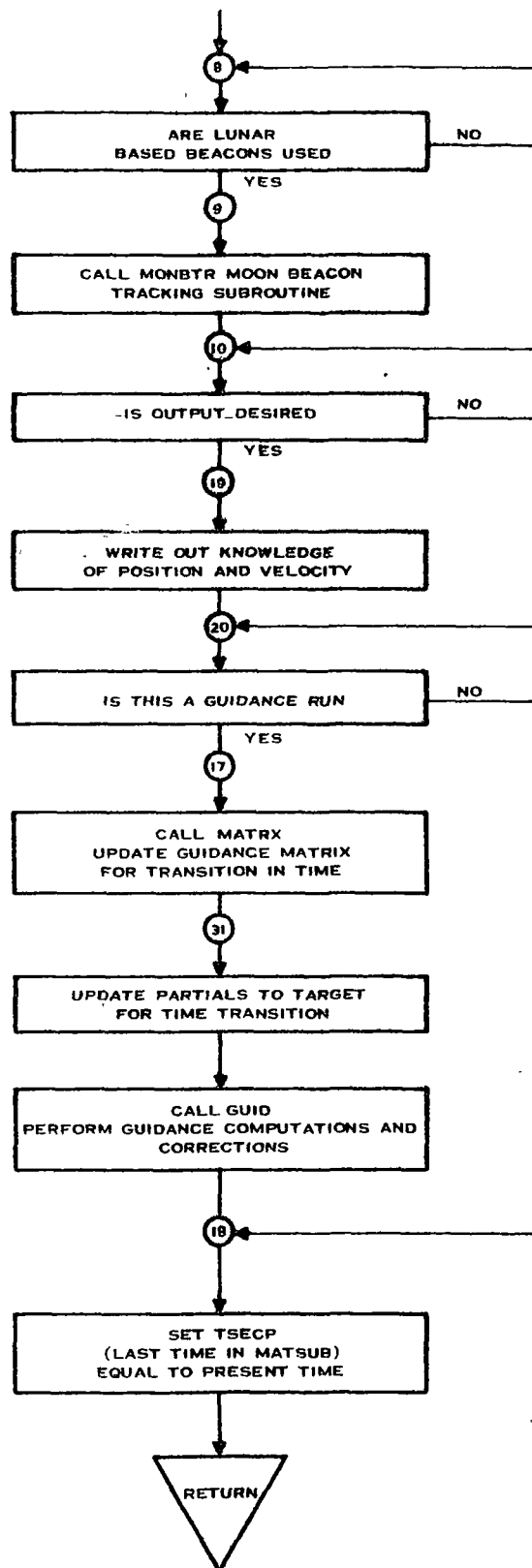
SQRT (FIL) (STH)

Approximate number of storages required:

346 DEC



MATSUB -2



* LABEL	MATS
* SYMBOL TABLE	MATS
CEC2006 SUBROUTINE MATSUB	MATS
SUBROUTINE MATSUB	MATS0000
COMMON T,S,C,IC	MATS0010
DIMENSION T(1360),S(1000),C(1000),IC(1),AN(3,3),PO(22),VE(22),	MATS0020
1EM(3,3),XP(3),VXP(3),EA(3,3),XED(3),VED(3),AO(6,6),P(6,6),	MATS0030
2TFTA(3,6),PFTA(6,6),AOS(6,6),AOI(6,6)	MATS0040
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),	MATS0050
1(C(138),AN),(C(13),TP1),(C(14),TP2),(C(62),PO),(C(84),VE),	MATS0060
2(C(120),EM),(C(650),TPRINT),(C(651),TSTRT),(C(30),TSEC),	MATS0070
3(C(15),XP),(C(18),VXP),(C(10),TW),(C(11),TF),(C(129),EA),	MATS0080
4(C(652),P),(C(752),AOS),(C(850),AOI)	MATS0090
5,(C(460),PFTA),(C(568),TFTA),(C(647),TOUT)	MATS0100
EQUIVALENCE (IC(2),IOR),(IC(7),KOUT),(IC(6),ITARG),(IC(9),LPRINT),	MATS0110
1(IC(190),LSTAT),(IC(191),LONB),(IC(192),LMB),(IC(193),IGUID),	MATS0120
2(IC(214),NOUT),(C(649),TSECP)	MATS0130
CALL SETN(NIN,NUTS)	MATS0131
NOUT=1	MATS0140
CALL LOADU(AO)	MATS0145
CALL MATRX(AO,AOS,AOS,6,6,6,0)	MATS0150
CALL LOADT	MATS0155
CALL MATRX(AO,P,P,6,6,6,1)	MATS0160
DO 30 I=1,6	MATS0165
DO 30 J=I,6	MATS0170
P(I,J)=(P(I,J)+P(J,I))/2.	MATS0175
P(J,I)=P(I,J)	MATS0180
30 CONTINUE	MATS0185
IF(TOUT=TSEC) 3,3,4	MATS0220
3 CONTINUE	MATS0230
TOUT=TOUT+TPRINT	MATS0240
NOUT=2	MATS0250
C NOUT IS USED TO INDICATE OTHER OUTPUT WANTED WHEN = 2	MATS0260
CALL OUTC	MATS0270
CALL OUTP	MATS0280
4 CONTINUE	MATS0290
C LSTAT IS SET 2 BY INPUT CARDS IF ANY EARTH BASED TRACKING	MATS0300
LSTAT=LSTAT	MATS0310
GO TO (6,5),LSTAT	MATS0320
5 CONTINUE	MATS0330
CALL EARTH	MATS0340
C EARTH UDDATS COV MATRIX P FOR EARTH BASED TRACKING	MATS0350
6 CONTINUE	MATS0360
LONB=LONB	MATS0370
GO TO (8,7),LONB	MATS0380
C LONB IS SET 2 BY INPUT CARDS IF ANY ONBOARD MEASUREMENTS MADE	MATS0390
7 CONTINUE	MATS0400
C ONBTR UPDATES COV MATRIX P FOR THE ONBOARD MEASUREMENTS	MATS0410
CALL ONBTR	MATS0420
8 CONTINUE	MATS0430
LMB=LMB	MATS0440

MATSUB (Cont'd)

	GO TO (10,9),LMB	MATS045
C	LMB IS SET 2 BY INPUT CARDS IF MOON BASED BEACONS USED	MATS046
9	CONTINUE	MATS047
	CALL MONBTR	MATS048
C	MONBTR UPDATES COV MATRIX P FOR BEACONS ON MOON	MATS049
10	CONTINUE	MATS050
	GO TO (20,19), NOUT	MATS051
19	CONTINUE	MATS052
	RMSP=SQRTF (P (1,1)+P (2,2)+P (3,3))	MATS053
	RMSVP=SQRTF(P (4,4)+P (5,5)+P (6,6))	MATS054
	WRITE OUTPUT TAPE NUTS,700,RMSP,RMSVP	MATS055
700	FORMAT(42H KNOWLEDGE OF STATE AFTER ALL OBSERVATIONS,/ 124H RMS POSITION=,E15.8,25H RMS VELOCITY=, 2E15.8)	MATS056 MATS057 MATS058
20	CONTINUE	MATS059
C	NUMBERS 11-16 RESERVED FOR FUTURE MEASUREMENTS	MATS060
	IGUID=IGUID	MATS061
	GO TO (18,17),IGUID	MATS062
C	IGUID IS SET BY INPUT TO MAIN PROGRAM IF GUIDANCE CALCULATIONS ARE MADE	MATS063
17	CONTINUE	MATS064
	CALL MATRX(AO,PFTA,PFTA,6,6,6,1)	MATS065
	DO 31 I=1,6	MATS066
	DO 31 J=I,6	MATS066
	PFTA(I,J)=(PFTA(I,J)+PFTA(J,I))/2.	MATS067
	PFTA(J,I)=PFTA(I,J)	MATS067
31	CONTINUE	MATS068
	CALL INVAO(AO,AOI)	MATS068
	CALL MATRX(TFTA,AOI,TFTA,3,6,6,0)	MATS069
C	CALL GUID	MATS071
	GUID PERFORMS THE GUIDANCE CALCULATIONS	MATS072
18	CONTINUE	MATS073
	TSECP=TSEC	MATS074
	RETURN	MATS075
	END	MATS

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Subroutine: MNA

Purpose: To provide the rotation matrix EMN which transforms moon centered coordinates in the earth's true equator and equinox to moon centered coordinates in the moon's true equator.

Calling Sequence:

CALL MNA (TIME, OM, CR, DT, EPSIL, RO, G, GP, WW, EMN)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TIME	1	d	days	Days since 1950.0
I	OM	1	Ω		Output from NUTAIT: (Arg. De-
					cending node)
I	CR	1	\mathcal{C}	radians	Output from NATAIT: (mean long.
					of the moon)
I	DT	1	$\Delta\psi + d\psi$	radians	Output from NUTAIT: (nutaton in
					longitude)
I	EPSIL	1	$\bar{e} + \Delta e + de$	radians	Output from NUTAIT: (mean obliquity and nutation in obliquity)

(Cont'd)

Common storages used or required:

None.

Subroutines required:

System double precision routines.

Functions required:

INTF, SORT, SIN, COS, ACOS

Approximate number of storages required:

(Cont'd.)

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	RO	1	ρ		Libration term
O	G	1	g	radians	Mean anomaly of the moon
O	GP	1	g	radians	Mean anomaly of the sun
O	WW	1	ω	radians	Argument of the perigee of the
					moon
O	EMN	3,3			Rotation matrix

Transformation From Earth's True Equator to Moon's True Equator.

The two rectangular systems are related through Λ , Ω' , and i by the rotation:

$$\begin{pmatrix} x \\ y \\ z \end{pmatrix}_{\text{MOON}} = \begin{pmatrix} b_{11} & b_{12} & b_{13} \\ b_{21} & b_{22} & b_{23} \\ b_{31} & b_{32} & b_{33} \end{pmatrix} \begin{pmatrix} x' \\ y' \\ z' \end{pmatrix}_{\text{EARTH}}$$

where

$$b_{11} = \cos \Lambda \cos \Omega' - \sin \Lambda \sin \Omega' \cos i$$

$$b_{12} = \cos \Lambda \sin \Omega' + \sin \Lambda \cos \Omega' \cos i$$

$$b_{13} = \cos \Lambda \sin i$$

$$b_{21} = -\sin \Lambda \cos \Omega' - \cos \Lambda \sin \Omega' \cos i$$

$$b_{22} = -\sin \Lambda \sin \Omega' + \cos \Lambda \cos \Omega' \cos i$$

$$b_{23} = \cos \Lambda \sin i$$

$$b_{31} = \sin \Omega' \sin i$$

$$b_{32} = -\cos \Omega' \sin i$$

$$b_{33} = \cos i$$

i is the inclination of the moon's true equator to the earth's equator

Ω' is the right ascension of the ascending node of the moon's true equator

Λ is the anomaly from the node to the X axis

$$\Lambda = \Delta + (\mathcal{C} + \Upsilon) - (\Omega + \sigma)$$

Δ is the anomaly from the node to the ascending node of the moon's true equator on the ecliptic

Ω is the mean longitude of the descending node of the moon's mean equator on the ecliptic

\mathcal{C} is the mean longitude of the moon

σ is the libration in the node

Υ is the libration in the mean longitude

ρ is the libration in the inclination.

$\delta\psi$, ϵ , Ω , and \mathcal{C} are input quantities obtained from NUTAIT. The remainder are computed from the following equations.

I = inclination of moon's equator to ecliptic

$$I = 1.535^\circ$$

g = mean anomaly of moon

$$g = 215.54013 + 13.064992 d$$

g' = mean anomaly of sun

g' = $358.009067 + .9856005 d$

ω = argument of perigee of moon

ω = $196.745632 + .1643586 d$

where d = days from 1950.

$$\sigma \sin I = -.0302777 \sin g + .0102777 \sin (g + 2\omega) - .00305555 \sin (2g + 2\omega)$$

$$\tau = -.003333 \sin g + .0163888 \sin g' + .005 \sin 2\omega$$

$$\rho = -.0297222 \cos g + .0102777 \cos (g + 2\omega) - .00305555 \cos (2g + 2\omega)$$

$$\cos i = \cos (\Omega + \sigma + \delta\psi) \sin \epsilon \sin (I + \rho)$$

$$+ \cos \epsilon \cos (I + \rho)$$

$$0 < i < 90^\circ$$

$$\sin \Omega' = -\sin (\Omega + \sigma + \delta\psi) \sin (I + \rho) \csc i$$

$$-90^\circ < \Omega' < 90^\circ$$

$$\sin \Delta = -\sin (\Omega + \sigma + \delta\psi) \sin \epsilon \csc i$$

$$\cos \Delta = -\sin (\Omega + \sigma + \delta\psi) \sin \Omega' \cos \epsilon$$

$$-\cos (\Omega + \sigma + \delta\psi) \cos \Omega'$$

$$0^\circ \leq \Delta < 360^\circ$$

Reference: JPL Technical Report No. 32-223

MNA

* LABEL
* SYMBOL TABLE

CEC20AH

SUBROUTINE MNA(TIME, OM, CR, DT, EPSIL, RO, G, GP, WW, EM)

DIMENSION EM(3,3), DF(3)

D = TIME

T = D/36525.

T2 = T*T

T3 = T2*T

A=13.064992

DO 6 I=1,3

DD=D

D - DD=DD*(A/360.)

D DD=DD-INTF(DD)

DF(I)=DD

GO TO (4,5,6), I

4 A=.9856005

GO TO 6

5 A=.1643586

6 CONTINUE

G=215.54013*360.*DF(1)

GP=358.009067*360.*DF(2)

WW=196.745632*360.*DF(3)

G = G*.017453296

GP = GP*.017453296

WW = WW*.017453296

YN = 1.535*.017453296

RO = -.0297222*COSF(G) + .01020777*COSF(G+2.*WW)

1 -.00305555*COSF(2.*G+2.*WW)

TA = -.003333*SINF(G) + .0163888*SINF(GP)

1 +.005*SINF(2.*WW)

SG = -.0302777*SINF(G) + .0102777*SINF(G+2.*WW)

1 -.00305555*SINF(2.*G+2.*WW)

SG = (SG*.017453296)/SINF(YN)

RO = RO*.017453296

TA = TA*.017453296

YN = YN + RO

RO = OM + SG + DT

CI = COSF(RO)*SINF(EPSIL)*SINF(YN)

1 +COSF(EPSIL)*COSF(YN)

SI = 1. - CI**2

SI = SQRTF(SI)

SO = -SINF(RO)*SINF(YN)/SI

CO = 1. - SO**2

CO = SQRTF(CO)

SD = -SINF(RO)*SINF(EPSIL)/SI

CD = -SINF(RO)*SO*COSF(EPSIL) - COSF(RO)*CO

DL = ACOSF(CD)

IF(SD)1,3,3

1 DL = 6.283185306 - DL

3 CONTINUE

SMNA

SMNA

SMNA

SMNA000

SMNA001

SMNA002

SMNA003

SMNA004

SMNA005

SMNA006

SMNA007

SMNA008

SMNA009

SMNA010

SMNA011

SMNA012

SMNA013

SMNA014

SMNA015

SMNA016

SMNA017

SMNA018

SMNA019

SMNA020

SMNA021

SMNA022

SMNA023

SMNA024

SMNA025

SMNA026

SMNA027

SMNA028

SMNA029

SMNA030

SMNA031

SMNA032

SMNA033

SMNA034

SMNA035

SMNA036

SMNA037

SMNA038

SMNA039

SMNA040

SMNA041

SMNA042

SMNA043

SMNA044

SMNA045

SMNA046

SMNA047

MNA (Cont'd)

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CA = DL + (CR + TA) - (OM + SG)
SA = SINF(CA)
CA = COSF(CA)
RO = COSF(RO)*SINF(EPSIL)/(SI*CD)
EM(1,1) = CA*CO - SA*SO*CI
EM(1,2) = CA*SO + SA*CO*CI
EM(1,3) = SA*SI
EM(2,1) = -SA*CO - CA*SO*CI
EM(2,2) = -SA*SO + CA*CO*CI
EM(2,3) = CA*SI
EM(3,1) = SO*SI
EM(3,2) = -CO*SI
EM(3,3) = CI
RETURN
END
```

SMNA048
SMNA049
SMNA050
SMNA051
SMNA052
SMNA053
SMNA054
SMNA055
SMNA056
SMNA057
SMNA058
SMNA059
SMNA060
SMNA061
SMNA

Subroutine: MNAND

Purpose: To compute the matrix M used to perform the velocity transformation corresponding to the position transformation described in MNA.

Calling Sequence:

CALL MNAND (TIME, RO, G, GP, WW, EM, DM)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TIME	1	d	days	Days since 1950.0
I	RO	1	ρ	radians	Output from MNA; see description
I	G	1	g	radians	Output from MNA; see description
I	GP	1	g'	radians	Output from MNA; see description
I	WW	1	ω	radians	Output from MNA; see description
I	EM	3,3	M		Output from MNA; matrix M
O	DM	3,3	\dot{M}		Matrix \dot{M}

Common storages used or required:

None

Subroutines required:

None

Functions required:

COS

Approximate number of storages required:

Theory and Equations

In transforming lunacentric position coordinates relative to the earth's equator and equinox of 1950.0 to coordinates relative to the moon's true equator, three matrices are computed. Matrix A (from ROTEQ) rotates the coordinates to equinox of date, matrix N (from NUTAIT) accounts for the nutation of the earth about its precessing mean equator, and matrix M (from MNA) transforms to the position relative to the moon's true equator.

$$\text{Then } \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}_{\text{moon}} = MNA \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}_{\text{earth, 1950.0}}$$

Assuming that $\dot{N} = \dot{A} = 0$

$$\begin{pmatrix} \dot{X} \\ \dot{Y} \\ \dot{Z} \end{pmatrix}_{\text{moon}} = MNA \begin{pmatrix} \dot{X} \\ \dot{Y} \\ \dot{Z} \end{pmatrix}_{\text{earth, 1950}} + \dot{M}NA \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}_{\text{earth, 1950}}$$

The \dot{M} matrix is computed from the equations:

$$\dot{M} = \begin{pmatrix} M_{21}\dot{\Lambda} & M_{22}\dot{\Lambda} & M_{23}\dot{\Lambda} \\ -M_{11}\dot{\Lambda} & -M_{12}\dot{\Lambda} & -M_{13}\dot{\Lambda} \\ 0 & 0 & 0 \end{pmatrix}$$

where M_{ij} are the elements of M, and

$$\dot{\Lambda} = \dot{\Delta} + \dot{\zeta} + \dot{\epsilon} - \dot{\Omega} - \dot{\sigma}$$

$$\dot{\Delta} = -\rho (\dot{\Omega} + \dot{\sigma})$$

$$\dot{\Omega} = 0.266170762 \times 10^{-5} - 0.12499171 \times 10^{-13} T \text{ rad/sec; } T = d/36525$$

$$\dot{\sigma} = -0.1069698435 \times 10^{-7} + 0.23015329 \times 10^{-3} T \text{ rad/sec}$$

$$\begin{aligned} \dot{t} = & -0.1535272946 \times 10^{-9} \cos g \\ & +0.569494067 \times 10^{-10} \cos g \\ & +0.579473484 \times 10^{-11} \cos 2g \text{ rad/sec} \end{aligned}$$

$$\begin{aligned} \dot{\sigma} = & -0.520642191 \times 10^{-7} \cos g \\ & +0.1811774451 \times 10^{-7} \cos (g+2g) \\ & -0.1064057858 \times 10^{-7} \cos (2g+2g) \text{ rad/sec} \end{aligned}$$

Reference: JPL Technical Report No. 32-223

MNAND

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* LABEL
* SYMBOL TABLE
SUBROUTINE MNAND(TIME,RO,G,GP,WW,EM,DM)
DIMENSION DM(3,3),EM(3,3)
T = TIME/36525.
CRD = .266170762E-5 * .12499171E-13*T
OMD = -.1069698435E-7 + .23015329E-13*T
TAD = -1.535272946*COSF(G) + .569494067*COSF(GP)
1 + .0579473484*COSF(2.*WW)
TAD = .1E-9*TAD
SGD = -.520642191*COSF(G) + .1811774451*COSF(G+2.*WW)
1 -.1064057858*COSF(2.*WW+2.*G)
SGD = .1E-6*SGD
DLD = -RO*(OMD + SGD)
CAD = DLD + CRD + TAD - OMD - SGD
DM(1,1) = EM(2,1)*CAD
DM(1,2) = EM(2,2)*CAD
DM(1,3) = EM(2,3)*CAD
DM(2,1) = -EM(1,1)*CAD
DM(2,2) = -EM(1,2)*CAD
DM(2,3) = -EM(1,3)*CAD
DM(3,1) = 0.0
DM(3,2) = 0.0
DM(3,3) = 0.0
RETURN
END

```

```

MNAN
MNAN
MNAN0000
MNAN0010
MNAN0020
MNAN0030
MNAN0040
MNAN0050
MNAN0060
MNAN0070
MNAN0080
MNAN0090
MNAN0100
MNAN0110
MNAN0120
MNAN0130
MNAN0140
MNAN0150
MNAN0160
MNAN0170
MNAN0180
MNAN0190
MNAN0200
MNAN0210
MNAN0220
MNAN

```

Subroutine: MONBTR

Purpose: To obtain the position and velocity vectors of the vehicle relative to the beacon and determine if the beacon is in view of the vehicle. The station location partials are computed and subroutine COMPHQ called to update the state covariance matrix for the measurements being made. The types of measurements possible are range, range rate, right ascension, and declination.

Calling Sequence:

CALL MONBTR

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities placed in common

Common storages used or required:

T, S, C, IC

Subroutines required:

COMPHQ, DOT, INTRI, MATRX, MNAND, MNA, NUTAIT, TRAC

Functions required:

ASIN, ATAN, FNORM, SQRT
(FIL)(SLO)(STH)

Approximate number of storages required:

495 DEC

MONBTR Partial Derivatives

MONBTR computes two partial matrices which are used in COMPHQ to evaluate station location errors. The matrices are the following:

$$\text{STPARS} = \begin{pmatrix} \frac{\partial x_1}{\partial \text{LAT}} & \frac{\partial x_1}{\partial \text{LON}} & \frac{\partial x_1}{\partial \text{ALT}} \\ \frac{\partial x_2}{\partial \text{LAT}} & \frac{\partial x_2}{\partial \text{LON}} & \frac{\partial x_2}{\partial \text{ALT}} \\ \frac{\partial x_3}{\partial \text{LAT}} & \frac{\partial x_3}{\partial \text{LON}} & \frac{\partial x_3}{\partial \text{ALT}} \end{pmatrix}$$

$$\text{STPARD} = \begin{pmatrix} \frac{\partial \dot{x}_1}{\partial \text{LAT}} & \frac{\partial \dot{x}_1}{\partial \text{LON}} & \frac{\partial \dot{x}_1}{\partial \text{ALT}} \\ \frac{\partial \dot{x}_2}{\partial \text{LAT}} & \frac{\partial \dot{x}_2}{\partial \text{LON}} & \frac{\partial \dot{x}_2}{\partial \text{ALT}} \\ \frac{\partial \dot{x}_3}{\partial \text{LAT}} & \frac{\partial \dot{x}_3}{\partial \text{LON}} & \frac{\partial \dot{x}_3}{\partial \text{ALT}} \end{pmatrix}$$

$$\text{where } \vec{X} = \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} = -\vec{X}_V + \vec{X}_B \quad \equiv \text{XREL (FORTRAN)}$$

$$\vec{\dot{X}} = \begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix} = -\vec{\dot{X}}_V + \vec{\dot{X}}_B \quad \equiv \text{VREL (FORTRAN)}$$

$$\frac{\partial x_i}{\partial \text{LAT}} = \frac{\partial x_{B1}}{\partial \text{LAT}} \quad \frac{\partial \dot{x}_i}{\partial \text{LAT}} = \frac{\partial \dot{x}_{B1}}{\partial \text{LAT}} \quad i = 1, 2, 3$$

$$\vec{X}_B = (MNA)^T \vec{X}_{BM}$$

$$\dot{\vec{X}}_B = (MNAND)^T \dot{\vec{X}}_{BM} + (MNA)^T \dot{\vec{X}}_{BM} \quad (=0)$$

where subscripts BM indicate beacon moon-fixed coordinates.

The transformations MNA and MNAND are obtained by calling the sub-routines MNA and MNAND.

$$\vec{X}_{BM} = (R + ALT) \begin{pmatrix} \cos LAT \cos LON \\ \cos LAT \sin LON \\ \sin LAT \end{pmatrix}$$

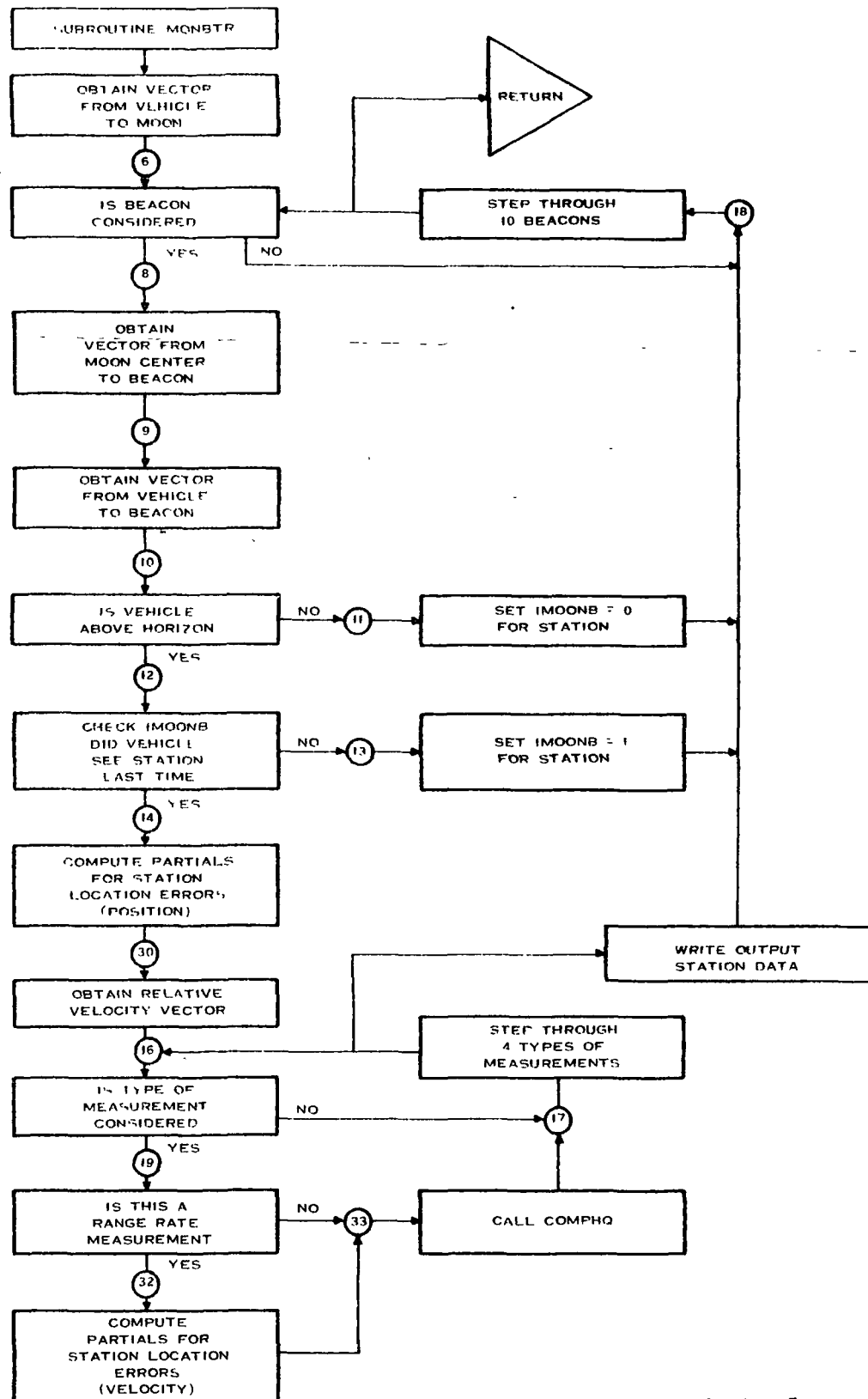
 3×1
 3×3
 3×1

$$\begin{pmatrix} \frac{\partial X_1}{\partial PAR} \\ \frac{\partial X_2}{\partial PAR} \\ \frac{\partial X_3}{\partial PAR} \end{pmatrix} = (MNA)^T \begin{pmatrix} \frac{\partial X_{BM}}{\partial PAR} \\ \frac{\partial Y_{BM}}{\partial PAR} \\ \frac{\partial Z_{BM}}{\partial PAR} \end{pmatrix}$$

$$\begin{pmatrix} \frac{\partial \dot{X}_1}{\partial PAR} \\ \frac{\partial \dot{X}_2}{\partial PAR} \\ \frac{\partial \dot{X}_3}{\partial PAR} \end{pmatrix} = (MNAND)^T \begin{pmatrix} \frac{\partial X_{BM}}{\partial PAR} \\ \frac{\partial Y_{BM}}{\partial PAR} \\ \frac{\partial Z_{BM}}{\partial PAR} \end{pmatrix}$$

S-279

MONBTR-3



S-281

MONSTR-5

MONBTR

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*      LABEL
*      SYMBOL TABLE
CEC2012 SUBROUTINE MONBTR
      SUBROUTINE MONBTR
      COMMON T,S,C,IC
      DIMENSION
1T(1360),S(1000),C(1000),IC(1),XREL(3),VREL(3)
1,PO(22),VE(22),AN(3,3),EM(3,3),ISBCON(10),U(3),EN(3)
2,RT(3),E(3),ETM(3,3),IMOONB(10),DM(3,3),DUM(3,3)
3,RMB(3),TYMEAS(4,10),X(3),VX(3),OUTPUT(6)
      DIMENSION STPARS(3,3),DUD(3,3),STPARD(3,3)
      EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),(IC,ICDUM)
1,(C(895),XREL),(C(898),VREL),(C(894),OBNO),(C(893),XMAG),
2(C(892),DEX),(C(891),DEN1),(C(890),DEN2)
3,(C(889),DEX2),(C(888),DEX3),(C(652),P),(C(973),OUTPUT)
1,(C(13),TW),(C(14),TF),(C(62),PO),(IC(3),NOR)
2,(IC(190),LSTAT),(C(138),AN),(S(24),A),(C(120),EM)
3,(IC(140),ISBCON),(S(72),DR),(IC(220),IMOONB),(C(649),TSECP)
4,(C(30),TSEC),(IC(140),TYMEAS),(C(15),X),(C(18),VX)
      EQUIVALENCE (C(800),STPARD),(C(788),STPARS)
      CALL SETN(NIN,NUTS)
      DELTT=TSEC-TSECP
      LSTAT=LSTAT
      GO TO(1,2),LSTAT
1  CONTINUE
   NB=NOR-1
   DIS=1.E10
   CALL INTR1(TW,TF,NB,PO,1,VE,DIS)
2  CONTINUE
   TIME=TW+TF
   CALL NUTAIT(TIME,OM,CR,DT,EM,EPSIL)
   CALL MNA(TIME,OM,CR,DT,EPSIL,RO,G,GP,WW,ETM)
   CALL MNAND(TIME,RO,G,GP,WW,ETM,DM)
   IF(NOR-2)3,5,3
3  CONTINUE
   DO 4 I=1,3
   J=20-I
   XREL(I)=PO(J)-X(I)
   VREL(I)=VE(J)-VX(I)
4  CONTINUE
   GO TO 7
5  CONTINUE
   DO 6 I=1,3
   XREL(I)=-X(I)
   VREL(I)=-VX(I)
6  CONTINUE
C   XREL POSITION VECTOR FROM VEHICLE TO MOON CENTER 1950
C   VREL RELATIVE VELOCITY OF MOON CENTER 1950
7  CONTINUE
   NN=485
   DO 18 III=1,10

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MONB
MONB
MONB
MONB0000
MONB0010
MONB0020
MONB0030
MONB0040
MONB0050
MONB0060
MONB0065
MONB0070
MONB0080
MONB0090
MONB0100
MONB0110
MONB0120
MONB0130
MONB0140
MONB0145
MONB0147
MONB0150
MONB0160
MONB0170
MONB0180
MONB0190
MONB0200
MONB0210
MONB0220
MONB0230
MONB0240
MONB0250
MONB0260
MONB0270
MONB0280
MONB0290
MONB0300
MONB0310
MONB0320
MONB0330
MONB0340
MONB0350
MONB0360
MONB0370
MONB0380
MONB0390
MONB0400
MONB0410
MONB0420
MONB0430
MONB0440

```


INTR, INTRI(Cont'd)

SUB TARGO
TNZ NEU
CLA TARG+1
SUB TARGO+1
TZE FLEE+6

TIME HAS CHANGED

REM
REM
REM
REM

ANALYZE TABLE
NEEDS AS A
FUNCTION OF
CENTRAL BODY

NEU

CLA TARG
FSB TABLE
TMI LOOKUP
STO COM+19
SUB 20.

POSITION EPHEMERIS TAPE
T-TO

TPL LOOKUP
CLA COM+19
FDH 4.

STQ COM+18
CLA COM+18
CALL FIX
CALL FLOAT
STO COM+17

 $(T-TO)/4.$

CHS
FAD COM+18
STO COM+1
CLA TARG+1
FDH 4.

STQ COM
CLA COM
FAD COM+1
STO TARG+2
LDQ COM+19

FMP =9,
CALL FIX
ADD KERN0+1
STA GG
LDQ COM+17

FMP =54,
CALL FIX
ADD KERN0+2
STA HH

AXT 2*SEP,4
STZ XN+2*SEP,4
TIX *-1,4,1
AXT BSEP,4
STZ KBO+BSEP,4

MUST INTERPOLATE
SO CLEAR STORAGE

TIX *-1,4,1
LXA CENTER,4
PXD ,4
COM
PDX ,2

SET GRAVITATIONAL
COEFFICIENTS
TO ZERO

INTR050
INTR051
INTR052
INTR053
INTR054
INTR055
INTR056
INTR057
INTR058
INTR059
INTR060
INTR061
INTR062
INTR063
INTR064
INTR065
INTR066
INTR067
INTR068
INTR069
INTR070
INTR071
INTR072
INTR073
INTR074
INTR075
INTR076
INTR077
INTR078
INTR079
INTR080
INTR081
INTR082
INTR083
INTR084
INTR085
INTR086
INTR087
INTR088
INTR089
INTR090
INTR091
INTR092
INTR093
INTR094
INTR095
INTR096
INTR097
INTR098
INTR099
INTR100

INTR, INTRI (Cont'd)

GEO	TXH	HELIO,4,1		INTR1010
	AXT	3,1		INTR1020
	CLA	GRAV+3,1		INTR1030
	STO	KBO+3,1		INTR1040
	TIX	*-2,1,1		INTR1050
	STZ	KBO-1,2		INTR1060
	CLA	EWORTO		INTR1070
	STO	EWORT		INTR1080
	CLA	HWORTE		INTR1090
	STO	HWORT		INTR1100
	TXH	GG12,4,0		INTR1110
	CLA	RJ	TEST FOR	INTR1120
	SUB	R	INCLUSION OF.	INTR1130
	TPL	GG12	JUPITER IF	INTR1140
	CLA	HWORTJ	EARTH IS	INTR1150
	STO	HWORT	CENTRAL BODY	INTR1160
	CLA	GRAV+6		INTR1170
	STO	KB6		INTR1180
	TXL	GG12,,**		INTR1190
HELIO	AXT	BSEP,1		INTR1200
	CLA	GRAV+BSEP,1		INTR1210
	STO	KBO+BSEP,1		INTR1220
	TIX	*-2,1,1		INTR1230
	STZ	KB2-3,2		INTR1240
ORTHO	CLA	EWORTO		INTR1250
	STO	EWORT		INTR1260
	CLA	HWORTO		INTR1270
	STO	HWORT		INTR1280
GG12	CLA	VEL	CHECK	INTR1290
	TZE	GG6	FOR VELOCITY	INTR1300
	CLA	EWORTO	OPTIONS	INTR1310
	STO	EWORT		INTR1320
	CLA	HWORTV		INTR1330
	STO	HWORT		INTR1340
GG6	CLA	EWORT		INTR1350
	TZE	GG+2		INTR1360
	CLA	EVEL		INTR1370
	STO	VEL+1		INTR1380
	CLA	TARG+1	GEOCENTRIC	INTR1390
	TSX	TAB,4	INTERPOLATION	INTR1400
GG	PZE	*,*,9		INTR1410
	PZE	XN,,EWORT+1		INTR1420
	CLA	HWORT		INTR1430
	TZE	HH+2		INTR1440
	CLA	HVEL		INTR1450
	STO	VEL+1		INTR1460
	CLA	TARG+2	HELIOCENTRIC	INTR1470
	TSX	TAB,4	INTERPOLATION	INTR1480
HH	PZE	*,*,54		INTR1490
	PZE	XN+3,,HWORT+1		INTR1500
RESET	AXT	3,4	PLACE	INTR1510

INTR, INTRI (Cont'd)

CLA XN+6,4
 FDH EVEL
 STQ XN,+18,4
 CLA XN+9,4
 FDH EVEL
 STQ XN,+12,4
 LDQ XN+3,4
 STQ XN+6,4
 FMP MU
 FSB XN+18,4
 STO XN+9,4
 STZ XN+3,4
 LDQ XN,+3,4
 STQ XN,+6,4
 FMP MU
 FSB XN,+18,4
 STO XN,+9,4
 STZ XN,+3,4
 TIX RESET+1,4,1
 LXA CENTER,4
 LXD VEL,2
 TXH RVPRT,2,0
 TXH TESTM,4,0
 NZT KB6
 TRA FLEE
 AXT 3,1
 CLA XN+21,1
 FAD XN+9,1
 STO XN+21,1
 TIX *-3,1,1
 TXL FLEE
 TESTM TXH RVPRT,4,1
 AXT 3,1
 CLS XN+6,1
 STO XN+3,1
 CLA XN+9,1
 FSB XN+6,1
 STO XN+9,1
 STZ XN+6,1
 TIX *-6,1,1
 FLEE CLA CENTER
 STO KERNO
 CLA TARG
 STO TARGO
 CLA TARG+1
 STO TARGO+1
 AXT 21,1
 CLA XN+21,1
 OUP STO **,1
 TIX OUP-1,1,1
 CLA VEL

COORDINATES
 IN OLD
 FORMAT

POSITION OF SUN

VELOCITY OF SUN

IX2 NOT ZERO IF VELOCITY OPTION
 GET COORDINATES FOR PRINTING

EARTH-CENTERED

MOON-CENTERED

TRANSFER POSITIONS

INTR152
 INTR153
 INTR154
 INTR155
 INTR156
 INTR157
 INTR158
 INTR159
 INTR160
 INTR161
 INTR162
 INTR163
 INTR164
 INTR165
 INTR166
 INTR167
 INTR168
 INTR169
 INTR170
 INTR171
 INTR172
 INTR173
 INTR174
 INTR175
 INTR176
 INTR177
 INTR178
 INTR179
 INTR180
 INTR181
 INTR182
 INTR183
 INTR184
 INTR185
 INTR186
 INTR187
 INTR188
 INTR189
 INTR190
 INTR191
 INTR192
 INTR193
 INTR194
 INTR195
 INTR196
 INTR197
 INTR198
 INTR199
 INTR200
 INTR201
 INTR202

INTR, INTRI (Cont'd)

	TZE	OUT
	AXT	21,1
	CLA	XN,+21,1
(N,V)	STO	++,1
	TIX	XN,V-1,1,1
OUT	LXD	HELIO-1,1
	LXD	TRAP+1,2
	LXD	TRAP,4
	TRA	8,4
	REM	TSX TAB,4
	REM	PZE B,,K
	REM	PZE A,,C
	REM	
	REM	
	REM	
	REM	
AB	SXD	COM+9,4
	SXD	COM+8,2
	SXD	COM+7,1
	STO	ARG
	CLA	1,4
	STA	TAB18
	LRS	18
	ADD	1,4
	STA	TAB21
	CLA	2,4
	PAX	,1
	TXI	++1,1,SEP
	SXA	TAB29,1
	ARS	18
	STA	VELOP
	AXT	2,1
	CLA	VEL
	TNZ	VELOP
	TXI	VELOP,1,-1
ELOP	CLA	++,1
	STO	VEL+2
	TXL	POSOP,1,1
	REM	
	CLA	ARG
	TSX	COEFF.,4
	AXT	3,4
	CLS	COM+13,4
	STO	COM+16,4
	TIX	*-2,4,1
	CLA	1.
	FSB	ARG
	TSX	COEFF.,4
	TRA	TAB1-1
	REM	
OSOP	CLA	ARG

DO NOT TRANSFER VELOCITY

TRANSFER VELOCITIES

(AC)=INTERPOLATIVE ARGUMENT

B=START OF DATA BLOCK

K=WORDS PER SUB BLOCK

A=START OF RESULT BLOCK

C=SKIP CODE WORD LOCATION

PICK UP SKIP
CODE WORD

VELOCITY OPTION

FORM THE
E1(2J).FORM THE
E0(2J).

POSITION OPTION

INTR2030
INTR2040
INTR2050
INTR2060
INTR2070
INTR2080
INTR2090
INTR2100
INTR2110
INTR2120
INTR2130
INTR2140
INTR2150
INTR2160
INTR2170
INTR2180
INTR2190
INTR2200
INTR2210
INTR2220
INTR2230
INTR2240
INTR2250
INTR2260
INTR2270
INTR2280
INTR2290
INTR2300
INTR2310
INTR2320
INTR2330
INTR2340
INTR2350
INTR2360
INTR2370
INTR2380
INTR2390
INTR2400
INTR2410
INTR2420
INTR2430
INTR2440
INTR2450
INTR2460
INTR2470
INTR2480
INTR2490
INTR2500
INTR2510
INTR2520
INTR2530

INTR, INTRI (Cont'd)

TSX COEFF,4
 AXT 3,4
 CLA COM+13,4
 STO COM+16,4
 TIX *-2,4,1
 CLA 1.
 FSB ARG
 TSX COEFF,4
 LXA TAB29,4
 TXI **1,4,-SEP
 SXA TAB29,4
 SXD COM+4,1
 TAB1 AXT 0,3
 LDQ VEL+2

PXD
 LGL 2
 PAX ,4
 STQ VEL+2
 CAL =03
 ORS VEL+2
 TXH END,4,2
 TXH FORT,4,0
 TXI **1,1,-3
 TXI TAB1+1,2,-1

FORT AXT 3,4
 TAB18 LDQ **,1
 FMP COM+13,4
 STO COM

TAB21 LDQ **,1
 FMP COM+16,4
 FAD COM
 STO COM+4,4
 TXI **1,1,-1
 TIX *-8,4,1
 FAD COM+2
 FAD COM+1

TAB29 STO **,2
 TXI TAB1+1,2,-1
 END LXD COM+4,1
 TIX VELOP,1,1
 LXD COM+9,4
 LXD COM+8,2
 LXD COM+7,1

COEFF TRA 3,4
 STO COM+10
 LDQ COM+10
 FMP COM+10
 STO COM+12
 FSB 1.
 FDH 6.
 FMP COM+10

FORM THE
 E1(2J)

FORM THE
 E0(2J)

X(0)

X(1)

X(T)

CALCULATE
 POSITION
 COEFFICIENTS
 FOR EVERETT,S
 INTERPOLATION
 FORMULA

INTR254
 INTR255
 INTR256
 INTR257
 INTR258
 INTR259
 INTR260
 INTR261
 INTR262
 INTR263
 INTR264
 INTR265
 INTR266
 INTR267
 INTR268
 INTR269
 INTR270
 INTR271
 INTR272
 INTR273
 INTR274
 INTR275
 INTR276
 INTR277
 INTR278
 INTR279
 INTR280
 INTR281
 INTR282
 INTR283
 INTR284
 INTR285
 INTR286
 INTR287
 INTR288
 INTR289
 INTR290
 INTR291
 INTR292
 INTR293
 INTR294
 INTR295
 INTR296
 INTR297
 INTR298
 INTR299
 INTR300
 INTR301
 INTR302
 INTR303
 INTR304

INTR, INTRI (Cont'd)

STO	COM+11		INTR3050
CLA	COM+12		INTR3060
FSB	4.		INTR3070
FDH	20.		INTR3080
FMP	COM+11		INTR3090
STO	COM+12		INTR3100
TRA	1,4		INTR3110
COEFF, STO	COM	CALCULATE	INTR3120
CLS	1.	VELOCITY	INTR3130
FDH	VEL+1	COEFFICIENTS	INTR3140
STO	COM+10	FOR EVERETT,S	INTR3150
LDQ	COM	INTERPOLATION	INTR3160
FMP	COM	FORMULA	INTR3170
STO	COM+12		INTR3180
XCA			INTR3190
FMP	3.		INTR3200
FSB	1.		INTR3210
FDH	6.		INTR3220
FMP	COM+10		INTR3230
STO	COM+11		INTR3240
CLA	COM+12		INTR3250
FSB	3.		INTR3260
XCA			INTR3270
FMP	5.		INTR3280
XCA			INTR3290
FMP	COM+12		INTR3300
FAD	4.		INTR3310
FDH	120.		INTR3320
FMP	COM+10		INTR3330
STO	COM+12		INTR3340
TRA	1,4		INTR3350
RVPRT AXT	0,2	EXPRESS ALL	INTR3360
AXT	3,5	BODIES GEOCENTRICALLY	INTR3370
CLA	XN+9,2		INTR3380
FAD	XN+9,4		INTR3390
STO	XN+9,2		INTR3400
CLA	VEL		INTR3410
TZE	++4		INTR3420
CLA	XN,+9,2		INTR3430
FAD	XN,+9,4		INTR3440
STO	XN,+9,2		INTR3450
TXI	++1,2,-1		INTR3460
TIX	RVPRT+2,4,1		INTR3470
TXH	RVPRT+1,2,9-SEP		INTR3480
CLA	CENTER	BUFFER	INTR3490
ALS	1	CENTRAL	INTR3500
ADD	CENTER	BODY	INTR3510
PAC	,4		INTR3520
CLA	XN,4		INTR3530
STO	COM+3,1		INTR3540
CLA	XN,,4		INTR3550

INTR, INTRI (Cont'd)

	STO	COM+6,1
	TXI	++1,4,-1
	TIX	*-5,1,1
RVPRT1	AXT	0,2
	AXT	3,4
	CLA	XN,2
	FSB	COM+3,4
	STO	XN,2
	CLA	VEL
	TZE	++4
	CLA	XN,,2
	FSB	COM+6,4
	STO	XN,,2
	TXI	++1,2,-1
	TIX	RVPRT1+2,4,1
	TXH	RVPRT1+1,2,-SEP
	TXL	FLEE
LOOKUP	CLA	TLAST
	FSB	TARG
	TNZ	++2
	TRA	ERR1
	TMI	*-1
	CLA	TARG
	FSB	TFIRST
	TPL	++2
	TRA	ERR1
	FDH	20,
	XCA	
	CALL	FIX
	CALL	FLOAT
	XCA	
	FMP	20,
	FAD	TFIRST
	STO	COM+1
	CLA	TABLE
	FSB	COM+1
	TMI	FINDIT
	FDH	20,
	XCA	
	CALL	FIX
	ADD	1F
	PAX	,4
	TEFA	++1
	TXL	++3,4,20
	REWA	6
	TRA	FINDIT
	BSRA	6
	TIX	*-1,4,1
FINDIT	AXT	10,2
	SDHA	6
	RTBA	6

EXPRESS ALL
BODIES IN TERMS
OF THE CENTRAL
BODY

TIME ON RECORD

RECORDS TO
BE BACKED

OVER

INTR3560
INTR3570
INTR3580
INTR3590
INTR3600
INTR3610
INTR3620
INTR3630
INTR3640
INTR3650
INTR3660
INTR3670
INTR3680
INTR3690
INTR3700
INTR3710
INTR3720
INTR3730
INTR3740
INTR3750
INTR3760
INTR3770
INTR3780
INTR3790
INTR3800
INTR3810
INTR3820
INTR3830
INTR3840
INTR3850
INTR3860
INTR3870
INTR3880
INTR3890
INTR3900
INTR3910
INTR3920
INTR3930
INTR3940
INTR3950
INTR3960
INTR3970
INTR3980
INTR3990
INTR4000
INTR4010
INTR4020
INTR4030
INTR4040
INTR4050
INTR4060

INTR, INTRI (Cont'd)

	RCHA	IO		INTR4070
	TCOA	*		INTR4080
	TEFA	ERR1		INTR4090
	CLA	TABLE		INTR4100
	SUB	COM+1		INTR4110
	TMI	**2		INTR4120
	TNZ	LOOKUP	TAPE NOT POSITIONED PROPERLY	INTR4130
	TNZ	FINDIT		INTR4140
	AXT	513,4		INTR4150
	CAL	TABLE	CHECK	INTR4160
	ACL	A+513,4	SUM	INTR4170
	TIX	*-1,4,1		INTR4180
	TRCA	BSRA		INTR4190
	LAS	C		INTR4200
	TRA	**2		INTR4210
	TRA	SCALE		INTR4220
BSRA	BSRA	6		INTR4230
	TIX	FINDIT+1,2,1		INTR4240
	CALL	ERP		INTR4250
IO	IOCD	TABLE,,515		INTR4260
ERR1	CALL	ERPT		INTR4270
	PZE	TARG		INTR4280
	REM		SCALING	INTR4290
	REM		LOOP	INTR4300
SCALE	AXT	189,4		INTR4310
	LDQ	A+189,4	SCALE	INTR4320
	FMP	SCALE1	GEOCENTRIC	INTR4330
	STO	A+189,4	EPHEMERIS	INTR4340
	TIX	*-3,4,1		INTR4350
	AXT	324,4		INTR4360
	LDQ	B+324,4	SCALE	INTR4370
	FMP	SCALE2	HELIOCENTRIC	INTR4380
	STO	B+324,4	EPHEMERIS	INTR4390
	TIX	*-3,4,1		INTR4400
	CLA	GRAV	COMPUTE	INTR4410
	FAD	GRAV+1	MASS RATIO	INTR4420
	STO	COM	OF MOON	INTR4430
	CLA	GRAV+1	TO EARTH-MOON	INTR4440
	FDH	COM	BARYCENTER	INTR4450
	STQ	MU	FOR POSITION OF EARTH	INTR4460
	TRA	NEU		INTR4470
SCALE1	DEC	6378.150	EARTH RADIUS	INTR4480
SCALE2	DEC	149598500.	ASTRONOMICAL UNIT (JPL, JULY 1961	INTR4490
FFIRST	DEC	3892.0	0 HR AUG 28, 1960 JD = 2437174.5	INTR4500
FLAST	DEC	7292.0	0 HR DEC 19, 1969 JD = 2440554.5	INTR4510
FRAP	PZE			INTR4520
	PZE			INTR4530
RJ	DEC	1E6	JUPITER TEST DISTANCE	INTR4540
TEMPDT	DEC	34.	E.T.=U.T.	INTR4550
	PZE			INTR4560
GRAV	DEC	3.98602E5	EARTH	INTR4570

INTR, INTRI (Cont'd)

DEC 4.8983349E3
 DEC 1.3252312E11
 DEC 3.2429889E5
 DEC 4.2915518E4
 DEC 0
 DEC 1.2652701E8
 DEC 86400.
 DEC 345600.

MU PZE
 OCT 000000520052
 HWORT OCT 0
 OCT 527777777777

EWORT OCT 0
 HWORTJ OCT 000000005252
 HWORTE OCT 000000005200
 EWORTO OCT 527777777777
 HWORTO OCT 000052525252
 HWORTV OCT 525252525252
 TARGO DEC 20.,0

KERNO PZE
 PZE A
 PZE B

ARG PZE 0
 1F DEC 1
 1. DEC 1.
 3. DEC 3.
 4. DEC 4.
 5. DEC 5.
 6. DEC 6.
 20. DEC 20.
 120. DEC 120.
 86400. DEC 86400.

VEL BSS 3
 *
 TABLE DEC 0
 A BSS 189
 B BSS 324
 C BSS 1

*
 TARG PZE
 PZE
 PZE
 CENTER PZE
 COM BSS 21
 VAFLG PZE
 FQFLG BSS 3
 KBO PZE
 KB1 PZE
 KB2 PZE
 KB3 PZE
 KB4 PZE

MOON INTR458
 SUN INTR459
 VENUS INTR460
 MARS INTR461
 REMOVE BARYCENTER INTR462
 JUPITER INTR463
 INTR464
 INTR465

MASS RATIO OF MOON TO BARYCENTER INTR466
 MARS, JUPITER VELOCITY INTR467
 INTR468
 MOON VELOCITY INTR469
 INTR470

BARYCENTER, JUPITER INTR471
 BARYCENTER INTR472

FORMER TIME INTR473
 FORMER CENTER INTR474
 GEOCENTRIC REFERENCE INTR475
 HELIOCENTRIC REFERENCE INTR476

INTR477
 INTR478
 INTR479
 INTR480
 INTR481
 INTR482
 INTR483
 INTR484
 INTR485
 INTR486
 INTR487
 INTR488
 INTR489

VELOCITY OPTION,H,SKIP CODE INTR490
 INTR491
 RESERVE INTR492
 FOR INTR493
 WORKING INTR494
 EPHEMERIS INTR495
 INTR496
 INTR497
 INTR498
 INTR499
 INTR500
 INTR501
 INTR502
 INTR503
 INTR504
 INTR505
 INTR506
 INTR507
 INTR508

INTR, INTRI (Cont'd)

KB5	PZE	
KB6	PZE	
XN	BSS	21
XN.	BSS	21
T	PZE	
	PZE	
R	PZE	
BSEP	SYN	7
SEP	SYN	XN, -XN
	END	

INTR5090
INTR5100
INTR5110
INTR5120
INTR5130
INTR5140
INTR5150
INTR5160
INTR5170
INTR

Subroutine: INV3

Purpose: To invert a matrix of any dimension up to a 6 by 6.

Calling Sequence:

CALL INV3 (A, N, DETERM)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
IO	A	6,6			A(I) Matrix to be inverted
					A(O) Inverse of input matrix
I	N	1			Dimension of input matrix
O	DETERM	1			Matrix determinant

Common storages used or required:

None

Subroutines required:

None

Functions required:

ABS

Approximate number of storages required:

INV3

*	LABEL	INV3
C	SUBROUTINE FOR INVERTING SQUARE MATRICES WHICH ARE 6 BY 6 OR LESS	INV30000
C	(TO INVERT LARGER MATRICES, SAY M BY M, DIMENSION IPIVOT(M), A(M*M),	INV30010
C	INDEX(M,2), PIVOT(M) AND RECOMPILE)	INV30020
C	A IS THE SQUARE MATRIX TO BE INVERTED	INV30030
C	N IS THE SIZE OF A (A IS AN N BY N MATRIX)	INV30040
C	THE SUBROUTINE RETURNS A INVERSE IN PLACE OF A AND THE DETERMINANT	INV30050
C	IN DETERM.	INV30060
	SUBROUTINE INV3(A,N,DETERM)	INV30070
	DIMENSION IPIVOT(6), A(36), INDEX(6,2), PIVOT(6)	INV30080
	EQUIVALENCE (IROW,JROW), (ICOLUM,JCOLUM), (AMAX,T,SWAP)	INV30090
	DETERM=1.0	INV30100
	DO 20 J=1,N	INV30110
20	IPIVOT(J)=0	INV30120
	DO 550 I=1,N	INV30130
	AMAX=0.0	INV30140
	DO 105 J=1,N	INV30150
	IF(IPIVOT(J)-1) 60,105,60	INV30160
60	DO 100 K=1,N	INV30170
	IF(IPIVOT(K)-1) 80,100,740	INV30180
80	M = N*(K-1)+J	INV30190
	IF (ABSF(AMAX)-ABSF(A(M))) 85,100,100	INV30200
85	IROW=J	INV30210
	ICOLUM=K	INV30220
	AMAX = A(M)	INV30230
100	CONTINUE	INV30240
105	CONTINUE	INV30250
	IPIVOT(ICOLUM)=IPIVOT(ICOLUM)+1	INV30260
	IF(IROW-ICOLUM) 140,260,140	INV30270
140	DETERM=-DETERM	INV30280
	DO 200 L=1,N	INV30290
	M = N*(L-1)	INV30300
	M1 = M+ICOLUM	INV30310
	M = M+IROW	INV30320
	SWAP = A(M)	INV30330
	A(M) = A(M1)	INV30340
200	A(M1) = SWAP	INV30350
260	INDEX(I,1)=IROW	INV30360
	INDEX(I,2)=ICOLUM	INV30370
	M = N*(ICOLUM-1)+ICOLUM	INV30380
	PIVOT(I) = A(M)	INV30390
	DETERM=DETERM*PIVOT(I)	INV30400
	A(M) = 1.0	INV30410
	DO 350 L=1,N	INV30420
	M = N*(L-1)+ICOLUM	INV30430
350	A(M) = A(M)/PIVOT(I)	INV30440
	DO 550 L1=1,N	INV30450
	IF(L1-ICOLUM) 400,550,400	INV30460
400	M = N*(ICOLUM-1)+L1	INV30470
	T = A(M)	INV30480
	A(M) = 0.	INV30490

INV3 (Cont'd)

```

      DO 450 L=1,N
      M = N*(L-1)
      M1 = M+ICOLUM
      M = M+L1
450  A(M) = A(M)-A(M1)+T
550  CONTINUE
      DO 710 I=1,N
      L=N+1-I
      IF (INDEX(L,1)=INDEX(L,2)) 630,710,630
630  JROW=INDEX(L,1)
      JCOLUM=INDEX(L,2)
      M = N*(JROW-1)
      M1 = N*(JCOLUM-1)
      DO 705 K=1,N
      M = M+1
      M1 = M1+1
      SWAP = A(M)
      A(M) = A(M1)
      A(M1) = SWAP
705  OONTINUE
710  OONTINUE
740  RETURN
      END

```

```

INV3051
INV3052
INV3053
INV3054
INV3055
INV3056
INV3057
INV3058
INV3059
INV3060
INV3061
INV3062
INV3063
INV3064
INV3065
INV3066
INV3067
INV3068
INV3069
INV3070
INV3071
INV3

```

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Subroutine: INVAO

Purpose: To form the inverse of a transition matrix for a linear, conservative dynamic system. If Φ is a partitioned matrix such as

$$\Phi = \begin{pmatrix} \Phi_1 & \Phi_2 \\ \Phi_3 & \Phi_4 \end{pmatrix} \text{ then INVAO computes } \Phi^{-1} = \begin{pmatrix} \Phi_4^T & -\Phi_2^T \\ -\Phi_3^T & \Phi_1^T \end{pmatrix}$$

Calling Sequence:

CALL INVAO (AO, AOI)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	AO	6,6	$\Phi(t_2, t_1)$		Transition Matrix
O	AOI	6,6	$\Phi^{-1}(t_2, t_1)$		Inverse Transition Matrix

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

INVAO

```

* LABEL
* SYMBOL TABLE
SUBROUTINE INVAO(AO,AOI)
DIMENSION AO(6,6),AOI(6,6)
DO 1 I=1,3
  II=I+3
  DO 1 J=1,3
    JJ=J+3
    AOI(I,J)=AO(JJ,II)
    AOI(II,J)=-AO(JJ,I)
    AOI(II,JJ)=AO(J,I)
1  AOI(I,JJ)=-AO(J,II)
RETURN
END

```

```

INVA
INVA
INVA0000
INVA0010
INVA0020
INVA0030
INVA0040
INVA0050
INVA0060
INVA0070
INVA0080
INVA0090
INVA0100
INVA

```


Subroutine: LOADO

Purpose: To transfer the transition matrix from its storage in the integration package's T block to the matrix in the call list.

Calling Sequence:

CALL LOADO (AO)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
0	AO	(6,6)	$\Phi(t_2 t_1)$		Transition Matrix

Common storages used or required:

T

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

LOADO

```

* LABEL
* SYMBOL TABLE
SUBROUTINE LOADO(AC)
COMMON T
DIMENSION T(1360),AO(6,6)
K=6
JJ=27
DO1 I=1,6
DO 1 J=1,3
K=K+1
KK=J+3
JJ=JJ+1
AO(KK,I)=T(JJ)
AO(J,I)=T(K)
1 CONTINUE
RETURN
END

```

```

LOAD
LOAD
LOAD0000
LOAD0010
LOAD0020
LOAD0030
LOAD0040
LOAD0050
LOAD0060
LOAD0070
LOAD0080
LOAD0090
LOAD0100
LOAD0110
LOAD0120
LOAD0130
LOAD

```

Subroutine: LOADT

Purpose: To place unit initial conditions in the T block for the
variational equations which are being used to generate the transition matrix.

Calling Sequence:

CALL LOADT

Input and Output

Common storages used or required:

T

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

LOAT
 LOAT
 LOAT0000
 LOAT0010
 LOAT0020
 LOAT0030
 LOAT0040
 LOAT0050
 LOAT0060
 LOAT0070
 LOAT0080
 LOAT0090
 LOAT0100
 LOAT0110
 LOAT0120
 LOAT0130
 LOAT0140
 LOAT0150
 LOAT0160
 LOAT0170
 LOAT

LOADT

```

* LABEL
* SYMBOL TABLE
SUBROUTINE LOADT
C SUBROUTINE LOADT PLTS UNIT ICS ON PERTURBATION EQUATIONS
COMMON T
DIMENSION T(1360),X(3,6),V(3,6)
EQUIVALENCE (T(7), X),(T(28),V)
DO 2 I=1,3
  L=I+3
  DO 1 J=1,3
    K=J+3
    X(I,J)=0.
    V(I,K)=0.
    X(I,K)=0.
    V(I,J)=0.
1 CONTINUE
    X(I,I)=1.
    V(I,L)=1.
2 CONTINUE
  RETURN
  END
  
```

Subroutine: MASS

Purpose: To find the relevant gravitational constants to be used in computing planetary perturbations for a given central body. MASS also chooses the initial integration step size as a function of central body.

Calling Sequence:

CALL MASS (NOR, UM, VKB, X, ACCP)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	NOR	1			Central Body Indicator.
					1=Earth; 2, Moon; 3, Sun; 4,
					Venus; 5, Mars; 6, Jupiter
I	UM	6	μ_i	Km^3/sec^2	Gravitational constants, arranged
					as above
O	VKB	6	μ_i	Km^3/sec^2	μ_i for bodies
I	X	3	X, Y, Z	Km	Position coordinates
O	ACCP	1		seconds	Initial integration step size

Common storages used or required:

None

Subroutines required:

None

Functions required:

FNORM

Approximate number of storages required:

Method of Establishing Integration Step Size and Perturbing Bodies

Central Body	Integration Step Size	Other Bodies to be Considered
Earth	60.0	Moon, Sun. If $ X \geq 10^6$ Km, Jupiter.
Moon	60.0	Earth, Sun.
Sun	43200.0	All
Venus, Mars, Jupiter	60.0	All

The bodies which are not to be used in calculation of perturbation accelerations are eliminated from consideration by placing zeros in array VKB(6). For the bodies which are being considered, the appropriate gravitational constant is placed in VKB(6).

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Subroutine: MATRX

Purpose: To perform matrix multiplications of matrices with any dimensions up to maximum dimensions of 10 by 10. A zero in the call sequence (J) yields an output matrix $C = A \cdot B$. A one in the call sequence (J) yields an output matrix $C = A \cdot B \cdot A^T$. The matrix products are obtained in double precision.

Calling Sequence:

CALL MATRX (A, B, C, NRA, NCA, NCB, J)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	A	(10,10)			Input Matrix
I	B	(10,10)			Input Matrix
O	C	(10,10)			Output Matrix
I	NRA	1			Number of Rows of A
I	NCA	1			Number of Columns of A
I	NCB	1			Number of Columns of B
I	J	1			Type of multiplication desired

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

MATRIX

```

* LABEL
* SYMBOL TABLE
CEC2000 SUBROUTINE MATRX
SUBROUTINE MATRX(A,B,C,NRA,NCA,NCB,J)
C J=0 A*B=C
C J=1 A*B*AT=C T MEANS TRANSPOSE
C NRA=NUMBER OF ROWS OF A
C NCA=COLUMNS OF A
C NCB=COLUMNS OF B
C ACCUMULATION OF PRODUCTS IN DOUBLE PRECISION
DIMENSION A(100),B(100),C(100),D(100)
D DUD=0.
D DUM=0.
DO 1 I=1,NRA
DO 1 K=1,NCB
NC=I+(K-1)*NRA
D CRUD=0.
DO 2 L=1,NCA
NA=I+(L-1)*NRA
NB=L+(K-1)*NCA
DUD=A(NA)
DUM=B(NB)
D CRUD=CRUD+DUD*DUM
2 CONTINUE
D(NC)=CRUD
1 CONTINUE
IF(J)3,3,4
3 CONTINUE
KK=NCB*NRA
DO 5 I=1,KK
5 C(I)=D(I)
GO TO 10
4 CONTINUE
DO 6 I=1,NRA
DO 6 K=1,NRA
NC=I+(K-1)*NRA
D CRUD=0.
DO 7 L=1,NCA
NA=I+(L-1)*NRA
NB=K+(L-1)*NRA
DUM=D(NA)
DUD=A(NB)
D CRUD=CRUD+DUM*DUD
7 CONTINUE
C(NC)=CRUD
6 CONTINUE
10 CONTINUE
RETURN
END

```

```

MATX
MATX
MATX
MATX0000
MATX0010
MATX0020
MATX0030
MATX0040
MATX0050
MATX0060
MATX0080
MATX0090
MATX0100
MATX0110
MATX0120
MATX0130
MATX0140
MATX0150
MATX0160
MATX0170
MATX0180
MATX0190
MATX0200
MATX0210
MATX0220
MATX0230
MATX0240
MATX0250
MATX0260
MATX0270
MATX0280
MATX0290
MATX0300
MATX0310
MATX0320
MATX0340
MATX0350
MATX0360
MATX0370
MATX0380
MATX0390
MATX0400
MATX0410
MATX0420
MATX0430
MATX0440
MATX0510
MATX0520
MATX

```

Subroutine: MATSUB

Purpose: The subroutine is primarily logic which controls (1) trajectory and data printout, (2) updating of the state covariance matrix for observations by calling subroutines EARTR, ONBTR, and MONBTR, and (3) updating of the guidance covariance matrix by calling subroutine GUID.

Calling Sequence:

CALL MATSUB

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities returned to common

Common storages used or required:

T, S, C, IC

Subroutines required:

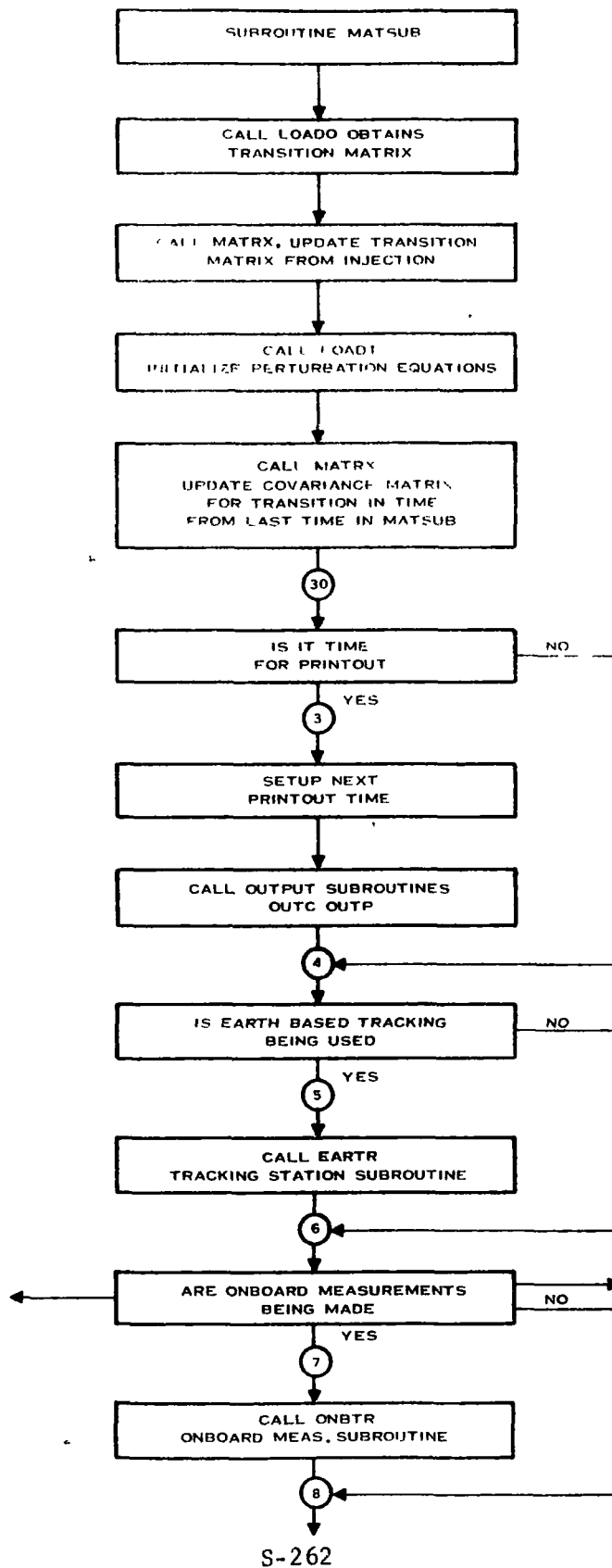
EARTR, GUID, INVAO, LOADO, LOADT, MATRX, MONBTR, ONBTR, OUTC, OUTP

Functions required:

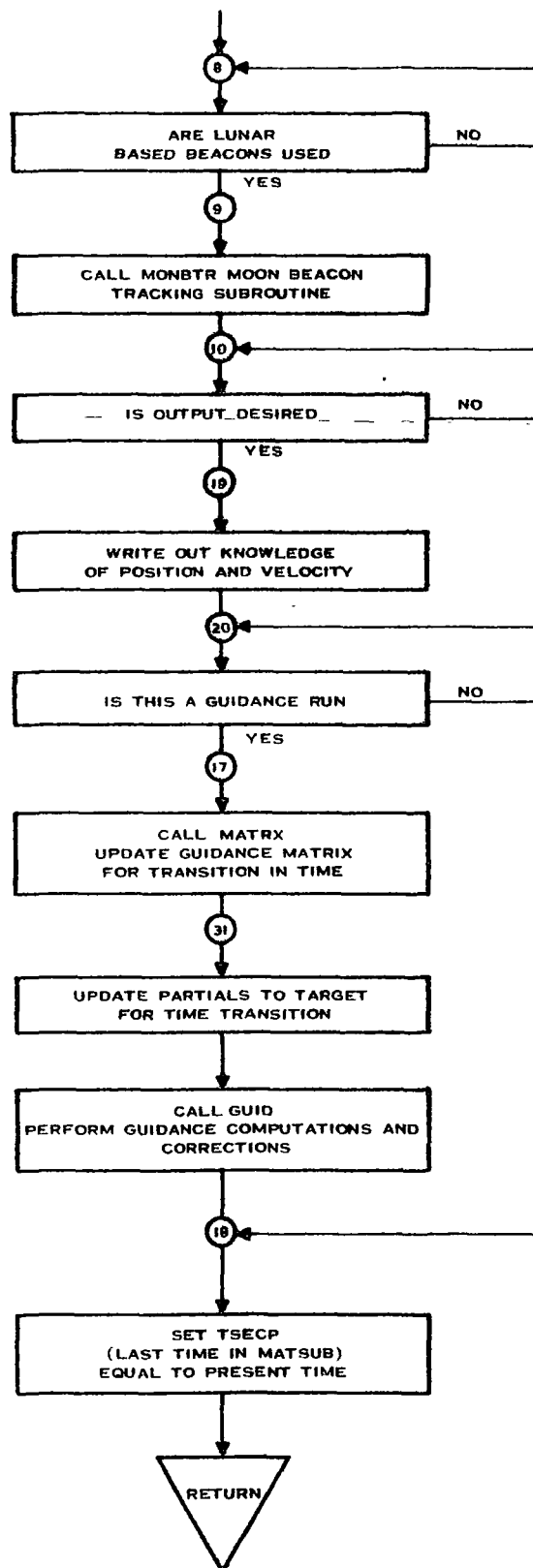
SQRT (FIL) (STH)

Approximate number of storages required:

346 DEC



MATSUB -2



<pre> * LABEL * SYMBOL TABLE CEC2006 SUBROUTINE MATSUB SUBROUTINE MATSUB COMMON T,S,C,IC DIMENSION T(1360),S(1000),C(1000),IC(1),AN(3,3),PO(22),VE(22), 1EM(3,3),XP(3),VXP(3),EA(3,3),XED(3),VED(3),AO(6,6),P(6,6), 2TFTA(3,6),PFTA(6,6),AOS(6,6),AOI(6,6) EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM), 1(C(138),AN),(C(13),TP1),(C(14),TP2),(C(62),PO),(C(84),VE), 2(C(120),EM),(C(650),TPRINT),(C(651),TSTRT),(C(30),TSEC), 3(C(15),XP),(C(18),VXP),(C(10),TW),(C(11),TF),(C(129),EA), 4(C(652),P),(C(752),AOS),(C(850),AOI) 5,(C(460),PFTA),(C(568),TFTA),(C(647),TOUT) EQUIVALENCE (IC(2),IOR),(IC(7),KOUT),(IC(6),ITARG),(IC(9),LPRINT), 1(IC(190),LSTAT),(IC(191),LONB),(IC(192),LMB),(IC(193),IGUID), 2(IC(214),NOUT),(C(649),TSECP) CALL SETN(NIN,NUTS) NOUT=1 CALL LOADU(AO) CALL MATRX(AO,AOS,AOS,6,6,6,0) CALL LOADT CALL MATRX(AO,P,P,6,6,6,1) DO 30 I=1,6 DO 30 J=I,6 P(I,J)=(P(I,J)+P(J,I))/2. P(J,I)=P(I,J) 30 CONTINUE IF(TOUT=TSEC) 3,3,4 3 CONTINUE TOUT=TOUT+TPRINT NOUT=2 C NOUT IS USED TO INDICATE OTHER OUTPUT WANTED WHEN = 2 CALL OUTC CALL OUTP 4 CONTINUE C LSTAT IS SET 2 BY INPUT CARDS IF ANY EARTH BASED TRACKING LSTAT=LSTAT GO TO (6,5),LSTAT 5 CONTINUE CALL EATR C EATR UDDATS COV MATRIX P FOR EARTH BASED TRACKING 6 CONTINUE LONB=LONB GO TO (8,7),LONB C LONB IS SET 2 BY INPUT CARDS IF ANY ONBOARD MEASUREMENTS MADE 7 CONTINUE C ONBTR UPDATES COV MATRIX P FOR THE ONBOARD MEASUREMENTS CALL ONBTR 8 CONTINUE LMB=LMB </pre>	<pre> MATS MATS MATS MATS0000 MATS0010 MATS0020 MATS0030 MATS0040 MATS0050 MATS0060 MATS0070 MATS0080 MATS0090 MATS0100 MATS0110 MATS0120 MATS0130 MATS0131 MATS0140 MATS0145 MATS0150 MATS0155 MATS0160 MATS0165 MATS0170 MATS0175 MATS0180 MATS0185 MATS0220 MATS0230 MATS0240 MATS0250 MATS0260 MATS0270 MATS0280 MATS0290 MATS0300 MATS0310 MATS0320 MATS0330 MATS0340 MATS0350 MATS0360 MATS0370 MATS0380 MATS0390 MATS0400 MATS0410 MATS0420 MATS0430 MATS0440 </pre>
--	---

MATSUB (Cont'd)

	GO TO (10,9),LMB	MATS0450
	LMB IS SET 2 BY INPUT CARDS IF MOON BASED BEACONS USED	MATS0460
C	9 CONTINUE	MATS0470
	CALL MONBTR	MATS0480
C	MONBTR UPDATES COV MATRIX P FOR BEACONS ON MOON	MATS0490
	10 CONTINUE	MATS0500
	GO TO (20,19), NOUT	MATS0510
	19 CONTINUE	MATS0520
	RMSP=SQRTF (P (1,1)+P (2,2)+P (3,3))	MATS0530
	RMSVP=SQRTF(P (4,4)+P (5,5)+P (6,6))	MATS0540
	WRITE OUTPUT TAPE NUTS,700,RMSP,RMSVP	MATS0550
700	FORMAT(42H KNOWLEDGE OF STATE AFTER ALL OBSERVATIONS,/ 124H RMS POSITION=,E15.8,25H RMS VELOCITY=, 2E15.8)	MATS0560 MATS0570 MATS0580
	20 CONTINUE	MATS0590
	NUMBERS 11-16 RESERVED FOR FUTURE MEASUREMENTS	MATS0600
	IGUID=IGUID	MATS0610
	GO TO (18,17),IGUID	MATS0620
C	IGUID IS SET BY INPUT TO MAIN PROGRAM IF GUIDANCE CALCULATIONS ARE MADE	MATS0630
	17 CONTINUE	MATS0640
	CALL MATRX(AO,PFTA,PFTA,6,6,6,1)	MATS0650
	DO 31 I=1,6	MATS0655
	DO 31 J=I,6	MATS0660
	PFTA(I,J)=(PFTA(I,J)+PFTA(J,I))/2.	MATS0665
	PFTA(J,I)=PFTA(I,J)	MATS0670
	31 CONTINUE	MATS0675
	CALL INVAO(AO,AOI)	MATS0680
	CALL MATRX(TFTA,AOI,TFTA,3,6,6,0)	MATS0685
	CALL GUID	MATS0690
C	GUID PERFORMS THE GUIDANCE CALCULATIONS	MATS0710
	18 CONTINUE	MATS0720
	TSECP=TSEC	MATS0730
	RETURN	MATS0740
	END	MATS0750
		MATS

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Subroutine: MNA

Purpose: To provide the rotation matrix EMN which transforms moon centered coordinates in the earth's true equator and equinox to moon centered coordinates in the moon's true equator.

Calling Sequence:

CALL MNA (TIME, OM, CR, DT, EPSIL, RO, G, GP, WW, EMN)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TIME	1	d	days	Days since 1950.0
I	OM	1	Ω		Output from NUTAIT: (Arg. De-
					cending node)
I	CR	1	ζ	radians	Output from NATAIT: (mean long.
					of the moon)
I	DT	1	$\Delta\psi + d\psi$	radians	Output from NUTAIT: (nutaton in
					longitude)
I	EPSIL	1	$\bar{e} + \Delta e + de$	radians	Output from NUTAIT: (mean obliquity and nutation in obliquity)

(Cont'd)

Common storages used or required:

None.

Subroutines required:

System double precision routines.

Functions required:

INTF, SORT, SIN, COS, ACOS

Approximate number of storages required:

(Cont'd.)

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
0	RO	1	ρ		Libration term
0	G	1	g	radians	Mean anomaly of the moon
0	GP	1	g	radians	Mean anomaly of the sun
0	WW	1	ω	radians	Argument of the perigee of the
					moon
0	EMN	3,3			Rotation matrix

Transformation From Earth's True Equator to Moon's True Equator.

The two rectangular systems are related through Λ , Ω' , and i by the rotation:

$$\begin{pmatrix} x \\ y \\ z \end{pmatrix}_{\text{MOON}} = \begin{pmatrix} b_{11} & b_{12} & b_{13} \\ b_{21} & b_{22} & b_{23} \\ b_{31} & b_{32} & b_{33} \end{pmatrix} \begin{pmatrix} x' \\ y' \\ z' \end{pmatrix}_{\text{EARTH}}$$

where

$$b_{11} = \cos \Lambda \cos \Omega' - \sin \Lambda \sin \Omega' \cos i$$

$$b_{12} = \cos \Lambda \sin \Omega' + \sin \Lambda \cos \Omega' \cos i$$

$$b_{13} = \cos \Lambda \sin i$$

$$b_{21} = -\sin \Lambda \cos \Omega' - \cos \Lambda \sin \Omega' \cos i$$

$$b_{22} = -\sin \Lambda \sin \Omega' + \cos \Lambda \cos \Omega' \cos i$$

$$b_{23} = \cos \Lambda \sin i$$

$$b_{31} = \sin \Omega' \sin i$$

$$b_{32} = -\cos \Omega' \sin i$$

$$b_{33} = \cos i$$

i is the inclination of the moon's true equator to the earth's equator

Ω' is the right ascension of the ascending node of the moon's true equator

Λ is the anomaly from the node to the X axis

$$\Lambda = \Delta + (\mathcal{C} + \Upsilon) - (\Omega + \sigma)$$

Δ is the anomaly from the node to the ascending node of the moon's true equator on the ecliptic

Ω is the mean longitude of the descending node of the moon's mean equator on the ecliptic

\mathcal{C} is the mean longitude of the moon

σ is the libration in the node

Υ is the libration in the mean longitude

ρ is the libration in the inclination.

$\delta\psi$, ϵ , Ω , and \mathcal{C} are input quantities obtained from NUTAIT. The remainder are computed from the following equations.

I = inclination of moon's equator to ecliptic

$$I = 1.535^\circ$$

g = mean anomaly of moon

$$g = 215.54013 + 13.064992 d$$

g' = mean anomaly of sun

g' = $358.009067 + .9856005 d$

ω = argument of perigee of moon

ω = $196.745632 + .1643586 d$

where d = days from 1950.

$$\sigma \sin I = -.0302777 \sin g + .0102777 \sin (g + 2\omega) - .00305555 \sin (2g + 2\omega)$$

$$\tau = -.003333 \sin g + .0163888 \sin g' + .005 \sin 2\omega$$

$$\rho = -.0297222 \cos g + .0102777 \cos (g + 2\omega) - .00305555 \cos (2g + 2\omega)$$

$$\cos i = \cos (\Omega + \sigma + \delta\psi) \sin \epsilon \sin (I + \rho)$$

$$+ \cos \epsilon \cos (I + \rho)$$

$$0 < i < 90^\circ$$

$$\sin \Omega' = -\sin (\Omega + \sigma + \delta\psi) \sin (I + \rho) \csc i$$

$$-90^\circ < \Omega' < 90^\circ$$

$$\sin \Delta = -\sin (\Omega + \sigma + \delta\psi) \sin \epsilon \csc i$$

$$\cos \Delta = -\sin (\Omega + \sigma + \delta\psi) \sin \Omega' \cos \epsilon$$

$$-\cos (\Omega + \sigma + \delta\psi) \cos \Omega'$$

$$0^\circ \leq \Delta < 360^\circ$$

Reference: JPL Technical Report No. 32-223

MNA

* LABEL
* SYMBOL TABLE

CEC20AH

SUBROUTINE MNA(TIME,OM,CR,DT,EPSIL,RO,G,GP,WW,EM)

DIMENSION EM(3,3),DF(3)

D = TIME

T = D/36525,

T2 = T*T

T3 = T2*T

A=13.064992

DO 6 I=1,3

DD=D

DD=DD*(A/360.)

DD=DD-INTF(DD)

DF(I)=DD

GO TO (4,5,6),I

4 A=.9856005

GO TO 6

5 A=.1643586

6 CONTINUE

G=215.54013*360.*DF(1)

GP=358.009067*360.*DF(2)

WW=196.745632*360.*DF(3)

G = G*.017453296

GP = GP*.017453296

WW = WW*.017453296

YN = 1.535*.017453296

RO = -.0297222*COSF(G) + .01020777*COSF(G+2.*WW)

1 -.00305555*COSF(2.*G+2.*WW)

TA = -.003333*SINF(G) + .0163888*SINF(GP)

1 +.005*SINF(2.*WW)

SG = -.0302777*SINF(G) + .0102777*SINF(G+2.*WW)

1 -.00305555*SINF(2.*G+2.*WW)

SG = (SG*.017453296)/SINF(YN)

RO = RO*.017453296

TA = TA*.017453296

YN = YN + RO

RO = OM + SG + DT

CI = COSF(RO)*SINF(EPSIL)*SINF(YN)

1 *COSF(EPSIL)*COSF(YN)

SI = 1. - CI**2

SI = SQRTF(SI)

SO = -SINF(RO)*SINF(YN)/SI

CO = 1. - SO**2

CO = SQRTF(CO)

SD = -SINF(RO)*SINF(EPSIL)/SI

CD = -SINF(RO)*SO*COSF(EPSIL) - COSF(RO)*CO

DL = ACOSF(CD)

IF(SD)1,3,3

1 DL = 6.283185306 - DL

3 CONTINUE

SMNA

SMNA

SMNA

SMNA000

SMNA001

SMNA002

SMNA003

SMNA004

SMNA005

SMNA006

SMNA007

SMNA008

SMNA009

SMNA010

SMNA011

SMNA012

SMNA013

SMNA014

SMNA015

SMNA016

SMNA017

SMNA018

SMNA019

SMNA020

SMNA021

SMNA022

SMNA023

SMNA024

SMNA025

SMNA026

SMNA027

SMNA028

SMNA029

SMNA030

SMNA031

SMNA032

SMNA033

SMNA034

SMNA035

SMNA036

SMNA037

SMNA038

SMNA039

SMNA040

SMNA041

SMNA042

SMNA043

SMNA044

SMNA045

SMNA046

SMNA047

MNA (Cont'd)

```
CA = DL + (CR + TA) - (OM + SG)
SA = SINF(CA)
CA = COSF(CA)
RO = COSF(RO)*SINF(EPSIL)/(SI*CD)
EM(1,1) = CA*CO - SA*SO*CI
EM(1,2) = CA*SO + SA*CO*CI
EM(1,3) = SA*SI
EM(2,1) = -SA*CO - CA*SO*CI
EM(2,2) = -SA*SO + CA*CO*CI
EM(2,3) = CA*SI
EM(3,1) = SO*SI
EM(3,2) = -CO*SI
EM(3,3) = CI
RETURN
END
```

```
SMNA048
SMNA049
SMNA050
SMNA051
SMNA052
SMNA053
SMNA054
SMNA055
SMNA056
SMNA057
SMNA058
SMNA059
SMNA060
SMNA061
SMNA
```

Subroutine: MNAND

Purpose: To compute the matrix M used to perform the velocity transformation corresponding to the position transformation described in MNA.

Calling Sequence:

CALL MNAND (TIME, RO, G, GP, WW, EM, DM)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TIME	1	d	days	Days since 1950.0
I	RO	1	ϕ	radians	Output from MNA; see description
I	G	1	g	radians	Output from MNA; see description
I	GP	1	g'	radians	Output from MNA; see description
I	WW	1	ω	radians	Output from MNA; see description
I	EM	3,3	M		Output from MNA; matrix M
O	DM	3,3	\dot{M}		Matrix \dot{M}

Common storages used or required:

None

Subroutines required:

None

Functions required:

COS

Approximate number of storages required:

Theory and Equations

In transforming lunacentric position coordinates relative to the earth's equator and equinox of 1950.0 to coordinates relative to the moon's true equator, three matrices are computed. Matrix A (from ROTEQ) rotates the coordinates to equinox of date, matrix N (from NUTAIT) accounts for the nutation of the earth about its precessing mean equator, and matrix M (from MNA) transforms to the position relative to the moon's true equator.

$$\text{Then } \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}_{\text{moon}} = MNA \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}_{\text{earth, 1950.0}}$$

Assuming that $\dot{N} = \dot{A} = 0$

$$\begin{pmatrix} \dot{X} \\ \dot{Y} \\ \dot{Z} \end{pmatrix}_{\text{moon}} = MNA \begin{pmatrix} \dot{X} \\ \dot{Y} \\ \dot{Z} \end{pmatrix}_{\text{earth, 1950}} + \dot{M}NA \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}_{\text{earth, 1950}}$$

The \dot{M} matrix is computed from the equations:

$$\dot{M} = \begin{pmatrix} M_{21}\dot{\Lambda} & M_{22}\dot{\Lambda} & M_{23}\dot{\Lambda} \\ -M_{11}\dot{\Lambda} & -M_{12}\dot{\Lambda} & -M_{13}\dot{\Lambda} \\ 0 & 0 & 0 \end{pmatrix}$$

where M_{ij} are the elements of M, and

$$\dot{\Lambda} = \dot{\Delta} + \dot{\zeta} + \dot{\epsilon} - \dot{\Omega} - \dot{\sigma}$$

$$\dot{\Delta} = -\rho (\dot{\Omega} + \dot{\sigma})$$

$$\dot{\Delta} = 0.266170762 \times 10^{-5} - 0.12499171 \times 10^{-13} T \text{ rad/sec; } T = d/36525$$

$$\dot{\Omega} = -0.1069698435 \times 10^{-7} + 0.23015329 \times 10^{-3} T \text{ rad/sec}$$

$$\begin{aligned} \dot{\sigma} = & -0.1535272946 \times 10^{-9} \cos g \\ & +0.569494067 \times 10^{-10} \cos g \\ & +0.579473484 \times 10^{-11} \cos 2\omega \text{ rad/sec} \end{aligned}$$

$$\begin{aligned} \dot{\sigma} = & -0.520642191 \times 10^{-7} \cos g \\ & +0.1811774451 \times 10^{-7} \cos (g+2\omega) \\ & -0.1064057858 \times 10^{-7} \cos (2\omega+2g) \text{ rad/sec} \end{aligned}$$

Reference: JPL Technical Report No. 32-223

MNAND

```

* LABEL
* SYMBOL TABLE
SUBROUTINE MNAND(TIME,RO,G,GP,WW,EM,DM)
DIMENSION DM(3,3),EM(3,3)
T = TIME/36525.
CRD = .266170762E-5 = .12499171E-13*T
OMD = -.1069698435E-7 + .23015329E-13*T
TAD = -1.535272946*COSF(G) + .569494067*COSF(GP)
1 + .0579473484*COSF(2.*WW)
TAD = .1E-9*TAD
SGD = -.520642191*COSF(G) + .1811774451*COSF(G+2.*WW)
1 -.1064057858*COSF(2.*WW+2.*G)
SGD = .1E-6*SGD
DLD = -RO*(OMD + SGD)
CAD = DLD + CRD + TAD - OMD - SGD
DM(1,1) = EM(2,1)*CAD
DM(1,2) = EM(2,2)*CAD
DM(1,3) = EM(2,3)*CAD
DM(2,1) = -EM(1,1)*CAD
DM(2,2) = -EM(1,2)*CAD
DM(2,3) = -EM(1,3)*CAD
DM(3,1) = 0.0
DM(3,2) = 0.0
DM(3,3) = 0.0
RETURN
END

```

```

MNAN
MNAN
MNAN0000
MNAN0010
MNAN0020
MNAN0030
MNAN0040
MNAN0050
MNAN0060
MNAN0070
MNAN0080
MNAN0090
MNAN0100
MNAN0110
MNAN0120
MNAN0130
MNAN0140
MNAN0150
MNAN0160
MNAN0170
MNAN0180
MNAN0190
MNAN0200
MNAN0210
MNAN0220
MNAN

```

Subroutine: MONBTR

Purpose: To obtain the position and velocity vectors of the vehicle relative to the beacon and determine if the beacon is in view of the vehicle. The station location partials are computed and subroutine COMPHQ called to update the state covariance matrix for the measurements being made. The types of measurements possible are range, range rate, right ascension, and declination.

Calling Sequence:

CALL MONBTR

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities placed in common

Common storages used or required:

T, S, C, IC

Subroutines required:

COMPHQ, DOT, INTRI, MATRX, MNAND, MNA, NUTAIT, TRAC

Functions required:

ASIN, ATAN, FNORM, SQRT
(FIL)(SLO)(STH)

Approximate number of storages required:

495 DEC

MONBTR Partial Derivatives

MONBTR computes two partial matrices which are used in COMPHQ to evaluate station location errors. The matrices are the following:

$$\text{STPARS} = \begin{pmatrix} \frac{\partial x_1}{\partial \text{LAT}} & \frac{\partial x_1}{\partial \text{LON}} & \frac{\partial x_1}{\partial \text{ALT}} \\ \frac{\partial x_2}{\partial \text{LAT}} & \frac{\partial x_2}{\partial \text{LON}} & \frac{\partial x_2}{\partial \text{ALT}} \\ \frac{\partial x_3}{\partial \text{LAT}} & \frac{\partial x_3}{\partial \text{LON}} & \frac{\partial x_3}{\partial \text{ALT}} \end{pmatrix}$$

$$\text{STPARD} = \begin{pmatrix} \frac{\partial \dot{x}_1}{\partial \text{LAT}} & \frac{\partial \dot{x}_1}{\partial \text{LON}} & \frac{\partial \dot{x}_1}{\partial \text{ALT}} \\ \frac{\partial \dot{x}_2}{\partial \text{LAT}} & \frac{\partial \dot{x}_2}{\partial \text{LON}} & \frac{\partial \dot{x}_2}{\partial \text{ALT}} \\ \frac{\partial \dot{x}_3}{\partial \text{LAT}} & \frac{\partial \dot{x}_3}{\partial \text{LON}} & \frac{\partial \dot{x}_3}{\partial \text{ALT}} \end{pmatrix}$$

$$\text{where } \vec{x} = \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} = -\vec{x}_V + \vec{x}_B \quad \equiv \text{XREL (FORTRAN)}$$

$$\vec{\dot{x}} = \begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix} = -\vec{\dot{x}}_V + \vec{\dot{x}}_B \quad \equiv \text{VREL (FORTRAN)}$$

$$\frac{\partial x_i}{\partial \text{LAT}} = \frac{\partial x_{Bi}}{\partial \text{LAT}} \quad \frac{\partial \dot{x}_i}{\partial \text{LAT}} = \frac{\partial \dot{x}_{Bi}}{\partial \text{LAT}} \quad i = 1, 2, 3$$

$$\vec{X}_B = (MNA)^T \vec{X}_{BM}$$

$$\vec{X}_B = (MNAND)^T \vec{X}_{BM} + \cancel{(MNA)^T \vec{X}_{BM}}^{(=0)}$$

where subscripts BM indicate beacon moon-fixed coordinates.

The transformations MNA and MNAND are obtained by calling the sub-routines MNA and MNAND.

$$\vec{X}_{BM} = (R + ALT) \begin{pmatrix} \cos LAT \cos LON \\ \cos LAT \sin LON \\ \sin LAT \end{pmatrix}$$

$3 \times 1 \quad 3 \times 3 \quad 3 \times 1$

$$\begin{pmatrix} \frac{\partial X_1}{\partial PAR} \\ \frac{\partial X_2}{\partial PAR} \\ \frac{\partial X_3}{\partial PAR} \end{pmatrix} = (MNA)^T \begin{pmatrix} \frac{\partial X_{BM}}{\partial PAR} \\ \frac{\partial Y_{BM}}{\partial PAR} \\ \frac{\partial Z_{BM}}{\partial PAR} \end{pmatrix}$$

$$\begin{pmatrix} \frac{\partial \dot{X}_1}{\partial PAR} \\ \frac{\partial \dot{X}_2}{\partial PAR} \\ \frac{\partial \dot{X}_3}{\partial PAR} \end{pmatrix} = (MNAND)^T \begin{pmatrix} \frac{\partial X_{BM}}{\partial PAR} \\ \frac{\partial Y_{BM}}{\partial PAR} \\ \frac{\partial Z_{BM}}{\partial PAR} \end{pmatrix}$$

$$\frac{\partial \bar{X}_{BM}}{\partial LAT} = (R + ALT) \begin{pmatrix} -\sin LAT \cos LON \\ -\sin LAT \sin LON \\ \cos LAT \end{pmatrix}$$

$$\frac{\partial \vec{X}_{BM}}{\partial LON} = (R + ALT) \begin{pmatrix} -\cos LAT \sin LON \\ \cos LAT \cos LON \\ 0 \end{pmatrix}$$

3 x 1 3 x 1

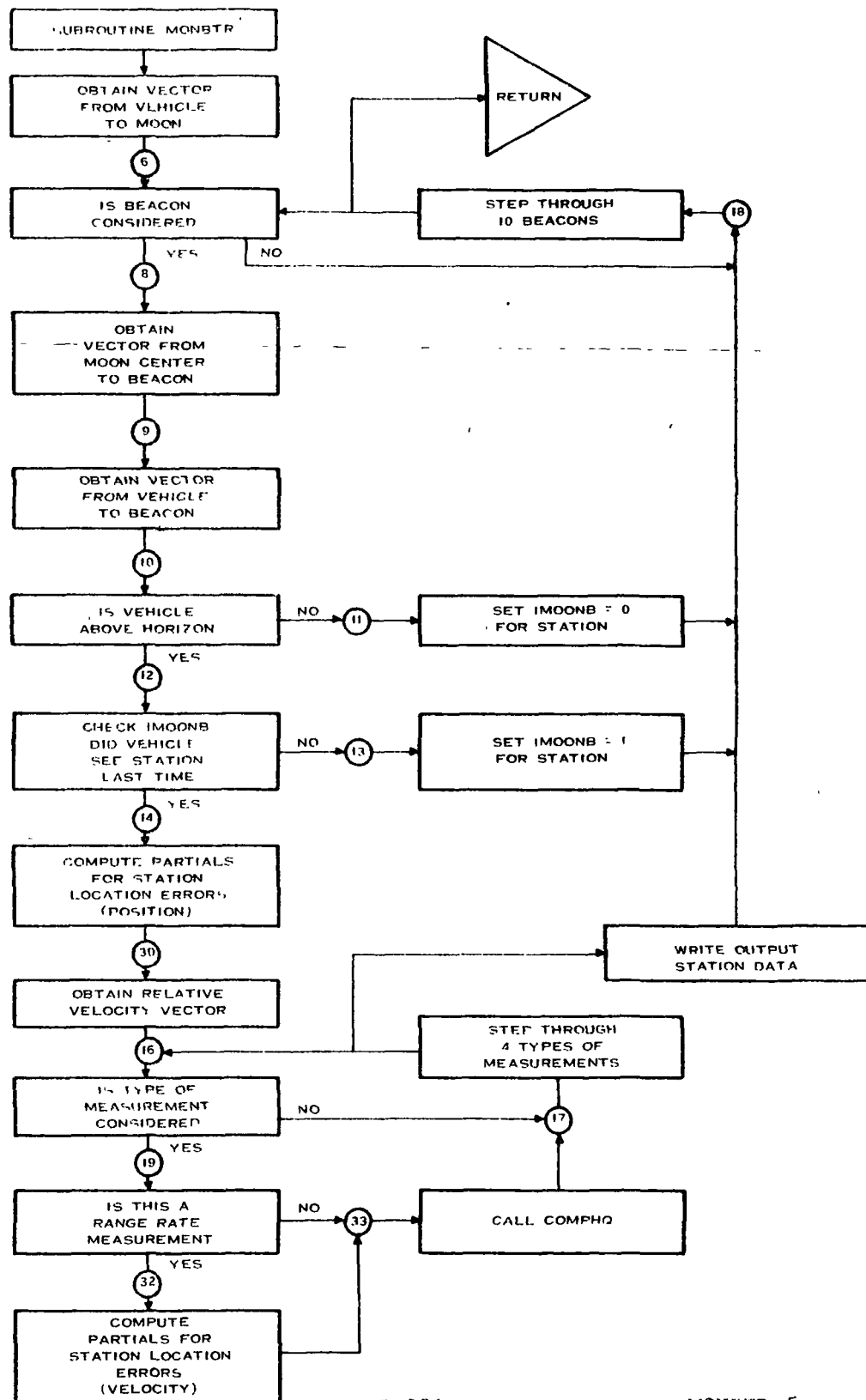
$$\frac{\partial \vec{X}_{BM}}{\partial ALT} = \begin{pmatrix} \cos LAT \cos LON \\ \cos LAT \sin LON \\ \sin LAT \end{pmatrix}$$

$$\text{STPARS} = (\text{MNA})^T \begin{pmatrix} \frac{\partial \vec{X}_{\text{BM}}}{\partial \text{LAT}} & \frac{\partial \vec{X}_{\text{BM}}}{\partial \text{LON}} & \frac{\partial \vec{X}_{\text{BM}}}{\partial \text{ALT}} \end{pmatrix}$$

$$\text{STPARD} = (\text{MNAND})^T \begin{pmatrix} \frac{\partial \vec{X}_{\text{BM}}}{\partial \text{LAT}} & \frac{\partial \vec{X}_{\text{BM}}}{\partial \text{LON}} & \frac{\partial \vec{X}_{\text{BM}}}{\partial \text{ALT}} \end{pmatrix}$$

3 x 3
3 x 3
3 x 3

Following computation of the matrices, subroutine COMPHQ is called to perform the updating of the state covariance matrix.



MONBTR

```

* LABEL
* SYMBOL TABLE
CEC2012 SUBROUTINE MONBTR
SUBROUTINE MONBTR
COMMON T,S,C,IC
DIMENSION
1T(1360),S(1000),C(1000),IC(1),XREL(3),VREL(3)
1,PO(22),VE(22),AN(3,3),EM(3,3),ISBOON(10),U(3),EN(3)
2,RT(3),E(3),ETM(3,3),IMOONB(10),DM(3,3),DUM(3,3)
3,RMB(3),TYMEAS(4,10),X(3),VX(3),OUTPUT(6)
DIMENSION STPARS(3,3),DUD(3,3),STPARD(3,3)
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),(IC,ICDUM)
1,(C(895),XREL),(C(898),VREL),(C(894),OBNO),(C(893),XMAG),
2(C(892),DEX),(C(891),DEN1),(C(890),DEN2)
3,(C(889),DEX2),(C(888),DEX3),(C(652),P),(C(973),OUTPUT)
1,(C(13),TW),(C(14),TF),(C(62),PO),(IC(3),NOR)
2,(IC(190),LSTAT),(C(138),AN),(S(24),A),(C(120),EM)
3,(IC(140),ISBCON),(S(72),DR),(IC(220),IMOONB),(C(649),TSECP)
4,(C(30),TSEC),(IC(140),TYMEAS),(C(15),X),(C(18),VX)
EQUIVALENCE (C(800),STPARD),(C(788),STPARS)
CALL SETN(NIN,NUTS)
DELT=TSEC-TSECP
LSTAT=LSTAT
GO TO(1,2),LSTAT
1 CONTINUE
NB=NOR-1
DIS=1.E10
CALL INTR1(TW,TF,NB,PO,1,VE,DIS)
2 CONTINUE
TIME=TW+TF
CALL NUTAIT(TIME,OM,CR,DT,EM,EPSIL)
CALL MNA(TIME,OM,CR,DT,EPSIL,RO,G,GP,WW,ETM)
CALL MNAND(TIME,RO,G,GP,WW,ETM,DM)
IF(NOR-2)3,5,3
3 CONTINUE
DO 4 I=1,3
J=20-I
XREL(I)=PO(J)-X(I)
VREL(I)=VE(J)-VX(I)
4 CONTINUE
GO TO 7
5 CONTINUE
DO 6 I=1,3
XREL(I)=-X(I)
VREL(I)=-VX(I)
6 CONTINUE
C XREL POSITION VECTOR FROM VEHICLE TO MOON CENTER 1950
C VREL RELATIVE VELOCITY OF MOON CENTER 1950
7 CONTINUE
NN=485
DO 18 III=1,10

```

```

MONB
MONB
MONB
MONB0000
MONB0010
MONB0020
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MONB0040
MONB0050
MONB0060
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MONB0070
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MONB0110
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MONB0145
MONB0147
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MONB0160
MONB0170
MONB0180
MONB0190
MONB0200
MONB0210
MONB0220
MONB0230
MONB0240
MONB0250
MONB0260
MONB0270
MONB0280
MONB0290
MONB0300
MONB0310
MONB0320
MONB0330
MONB0340
MONB0350
MONB0360
MONB0370
MONB0380
MONB0390
MONB0400
MONB0410
MONB0420
MONB0430
MONB0440

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```

      NN=NN+15
      IF (ISBCON(III)) 18,18,8
8     CONTINUE
      AT=S(NN+9)*DR
      ON=S(NN+10)*DR
      AL=S(NN+11)
      SNAME=S(NN+12)
      GH=0.
      CALL TRAC(ON,AT,AL,GH,U,E,EN,RT,AC,SL,CL,ST,CT,A,A)
      CALL MATRX(ETM,AN,DUM,3,3,3,0)
      DO 9 I=1,3
      RMB(I)=0.
      DO 9 J=1,3
      RMB(I)=RMB(I)+DUM(J,I)*RT(J)
9     CONTINUE
C    RMB-RADIUS VECTOR TO MOON BEACON 1950
      DO 10 I=1,3
      XREL(I)=XREL(I)+RMB(I)
C    XREL VECTOR FROM VEHICLE TO MOON BEACON 1950
10    CONTINUE
      TEST=DOT(RMB,XREL)
      IF(TEST) 12,12,11
11    IMOONB(III)=0
C    VEHICLE BELOW BEACON HORIZON
      GO TO 18
12    CONTINUE
      IF(IMOONB(III)) 13,13,14
13    CONTINUE
      IMOONB(III)=1
      GO TO 18
14    CONTINUE
      RADIUS=A+AL
      DUD(1,1)=-RADIUS*SL*CT
      DUD(2,1)=-RADIUS*SL*ST
      DUD(3,1)=RADIUS*CL
      DUD(1,2)=-RADIUS*CL*ST
      DUD(2,2)=RADIUS*CL*CT
      DUD(3,2)=0.
      DUD(1,3)=CL*CT
      DUD(2,3)=CL*ST
      DUD(3,3)=SL
      DO 30 I=1,3
      DO 30 J=1,3
      STPARS(I,J)=0.
      DO 30 K=1,3
30    STPARS(I,J)=STPARS(I,J)+DUM(K,I)*DUD(K,J)
      CALL MATRX(DM,AN,DUM,3,3,3,0)
      DO 15 I=1,3
      RMB(I)=0
      DO 15 J=1,3
      RMB(I)=RMB(I)+DUM(J,I)*RT(J)

```

MONB045
 MONB046
 MONB047
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MONETR (Cont'd)

15	CONTINUE	MONB0810
C	RMB ROTATIONAL VELOCITY OF MOON BEACON 1950	MONB0820
	DO 16 I=1,3	MONB0830
	VREL(I)=VREL(I)+RMB(I)	MONB0840
C	VREL RELATIVE VELOCITY OF MOON BEACON WRT THE VEHICLE	MONB0850
16	CONTINUE	MONB0860
	OBNO=DELTT/S(NN+13)	MONB0870
	XMAG=FNORM(XREL)	MONB0880
	DEX=XREL(1)**2+XREL(2)**2	MONB0890
	DEN1=1./SQRTF(DEX)/XMAG**2	MONB0900
	DEN2=1./DEX	MONB0910
	DEX2=XMAG*XMAG	MONB0920
	DEX3=1./XMAG	MONB0930
C	THE ABOVE QUANTITIES ARE USED IN COMPUTATIONS OF H MATRIX	MONB0940
	DEC=ASINF(DEX3*XREL(3))	MONB0942
	OUTPUT(5)=DEC/DR	MONB0944
	RA=ATANF(XREL(2)/XREL(1))	MONB0946
	OUTPUT(3)=RA/DR	MONB0948
	OUTPUT(1)=XMAG	MONB0949
	DO 17 JJJ=1,4	MONB0950
	IF(TYMEAS(JJJ,III))17,17,19	MONB0960
19	CONTINUE	MONB0962
	IF(JJJ=4)33,32,33	MONB0964
32	CONTINUE	MONB0966
	DO 34 I=1,3	MONB0968
	DO 34 J=1,3	MONB0970
	STPARD(I,J)=0.	MONB0972
	DO 34 K=1,3	MONB0974
34	STPARD(I,J)=STPARD(I,J)+DUM(K,I)*DUD(K,J)	MONB0975
33	CONTINUE	MONB0976
	CALL COMPHQ(JJJ,2,NN)	MONB0978
17	CONTINUE	MONB0980
	WRITE OUTPUT TAPE NUTS,700,III,OUTPUT	MONB0982
700	FORMAT(13H MOON BEACON ,I2,	MONB0983
	1/4H RNGE15.8,5H RGRE15.8,	MONB0984
	25H RAE15.8,5H RARE15.8,5H DECE15.8,5H DCRE15.8)	MONB0985
	DO 20 I=1,6	MONB0986
20	OUTPUT(I)=0.	MONB0987
18	CONTINUE	MONB0990
	RETURN	MONB1000
	END	MONB

Subroutine: MULT

Purpose: To find the product matrix of two 3 x 3 matrices.

Calling Sequence:

CALL MULT (A, B, C)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	A	3,3			First input matrix
I	B	3,3			Second input matrix
O	C	3,3			C = AB

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

MULT

```
* LABEL
* SYMBOL TABLE
SUBROUTINE MULT(A,B,C,N)
DIMENSION A(3,3),B(3,3),C(3,3)
DO 1 I=1,3
DO 1 J=1,3
C(I,J) = 0.
DO 1 K=1,3
1 C(I,J) = C(I,J) + A(I,K)*B(K,J)
3 RETURN
END
```

```
MULT
MULT
MULT0000
MULT0010
MULT0020
MULT0030
MULT0040
MULT0050
MULT0060
MULT0070
MULT
```

Subroutine: NUTAIT

Purpose: To evaluate the elements of the nutation matrix which relates the Cartesian coordinates expressed in the true equator and equinox to those in the mean equator and equinox.

Calling Sequence:

CALL NUTAIT (TIME, OM, CR, DT, EN, EPSIL)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TIME	1	T	days	Total number days from ref.epoch
O	OM	1	Ω	radians	Argument of moon's descending node
O	CR	1	CR	radians	Mean longitude of moon
O	DT	1	$\Delta\psi + d\psi$	radians	Nutation in longitude of equinox
O	EN	3,3	N	(-)	Nutation matrix
O	EPSIL	1	$\bar{\epsilon} + d\epsilon$	radians	True obliquity

Common storages used or required:

None

Subroutines required:

None

Functions required:

INTF, SINF, COSF

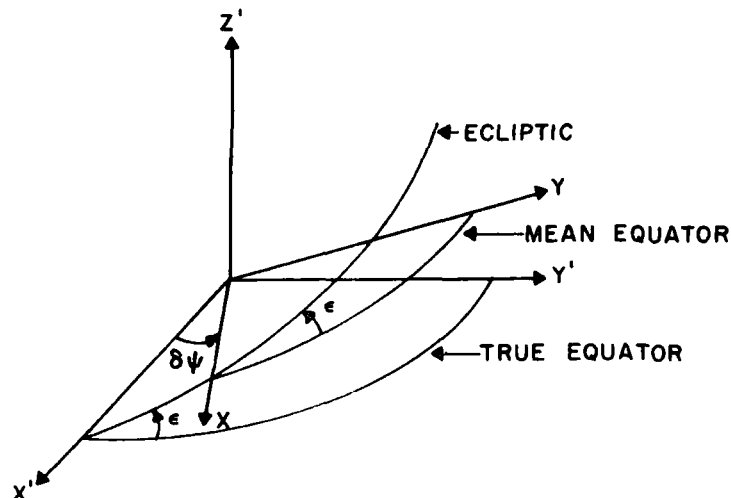
Approximate number of storages required:

NUTAIT

Method and Theory

The input time is converted to Julian centuries of 36525 days past the reference epoch (currently, 0^h January 1, 1950, E.T.). Where the computed angles are likely to be extremely large, the largest contributing term is reduced to the first revolution by the internal function DF(X). By using double precision arithmetic, this technique also helps to control round-off errors more closely as well as to keep the computed angles reasonable.

The relationship between the Cartesian coordinates expressed in the true equator and equinox and those expressed in the mean equator and equinox is shown in the following sketch:



The nutations are given by the following:

$$\text{For obliquity} \quad \delta\epsilon = \Delta\epsilon + d\epsilon$$

$$\text{For longitude} \quad \delta\Psi = \Delta\Psi + d\Psi$$

In the above equations, $\Delta\epsilon$, $\Delta\Psi$ express the long-period contributions and $d\epsilon$, $d\Psi$ the short-period contributions.

Both ϵ and Ψ are computed as functions of Ω , CR, Γ' , L, Γ where

$$\Omega = 12.112790 - 360*DF(1) + .0020795T + .002081T^2 + .000002T^3$$

$$CR = 64.375452 + 360*DF(2) - .001131575T - .00113015T^2 - .0000019T^3$$

$$\Gamma' = 208.84399 + 360*DF(3) - .010334T - .010343T^2 - .000012T^3$$

$$\Gamma = 282.08053 + .0000470684D + .00045525T + .0004575T^2 + .000003T^3$$

$$L = 280.08121 + 360*DF(4) + .000303 (T + T^2)$$

T in the above equations is the number of Julian years past the reference epoch and the function DF(X) is

$$DF(X) = d \frac{a}{360}$$

where $a = .052953922, 13.176397, .11140408, .98564734$

and d is the number of days past the reference epoch.

$$\begin{aligned} \text{Then } \Delta\epsilon \times 10^4 &= 25.5844 \cos \Omega - .2511 \cos 2\Omega \\ &+ 1.5336 \cos 2L + .0666 \cos (3L - \Gamma) \\ &- .0258 \cos (L + \Gamma) - .0183 \cos (2L - \Omega) \\ &- .0067 \cos (2\Gamma' - \Omega) \end{aligned}$$

$$\begin{aligned} d\epsilon \times 10^4 &= .2456 \cos 2CR + .0508 \cos (2CR - \Omega) \\ &+ .0369 \cos (3CR - \Gamma') - .0139 \cos (CR + \Gamma') \\ &- .0086 \cos (CR - \Gamma' + \Omega) + .0083 \cos (CR - \Gamma' - \Omega) \\ &+ .0061 \cos (3CR + \Gamma' - 2L) + .0064 \cos (3CR - \Gamma' - \Omega) \end{aligned}$$

$$\begin{aligned} \Delta\Psi \times 10^4 &= -(47.8927 + .0482T) \sin \Omega \\ &+ .5800 \sin 2\Omega - 3.5361 \sin 2L - .1378 \sin (3L - \Gamma) \\ &+ .0594 \sin (L + \Gamma) + .0344 \sin (2L - \Omega) + .0125 \sin (2\Gamma' - \Omega) \\ &+ .3500 \sin (L - \Gamma) + .0125 \sin (2L - 2\Gamma') \end{aligned}$$

$$\begin{aligned}
d\psi \times 10^4 = & -.5658 \sin 2CR - .0950 \sin (2CR - \Omega) \\
& - .0725 \sin (3CR - \Gamma') + .0317 \sin (CR + \Gamma') \\
& + .0161 \sin (CR - \Gamma' + \Omega) + .0158 \sin (CR - \Gamma' - \Omega) \\
& - .0144 \sin (3CR + \Gamma' - 2L) - .0122 \sin (3CR - \Gamma' - \Omega) \\
& + .1875 \sin (CR - \Gamma') + .0078 \sin (2CR - 2\Gamma') \\
& + .0414 \sin (CR + \Gamma' - 2L) + .0167 \sin (2CR - 2L) \\
& - .0089 \sin (4CR - 2L).
\end{aligned}$$

The mean obliquity is calculated by

$$\bar{\epsilon} = 23.4457587 - .01309404T - .00000088T^2 + .00000050T^3$$

and the true obliquity by

$$\epsilon = \bar{\epsilon} + \delta\epsilon$$

The nutation matrix N relates the Cartesian coordinates expressed in the true equator and equinox to those in the mean equator and equinox by

$$\begin{vmatrix} X' \\ Y' \\ Z' \end{vmatrix} = N \begin{vmatrix} X \\ Y \\ Z \end{vmatrix}$$

where the primed system is the true equator and equinox and the unprimed is the mean equator and equinox.

Thus

$$\begin{aligned}
N_{11} &= \cos \delta\psi \\
N_{12} &= -\sin \delta\psi \cos \bar{\epsilon} \\
N_{13} &= \sin \delta\psi \sin \bar{\epsilon} \\
N_{21} &= \sin \delta\psi \cos \epsilon
\end{aligned}$$

$$N_{22} = \cos \delta\psi \cos \epsilon \cos \bar{\epsilon} + \sin \epsilon \sin \bar{\epsilon}$$

$$N_{23} = \cos \delta\psi \cos \epsilon \sin \bar{\epsilon} - \sin \epsilon \cos \bar{\epsilon}$$

$$N_{31} = \sin \delta\psi \sin \epsilon$$

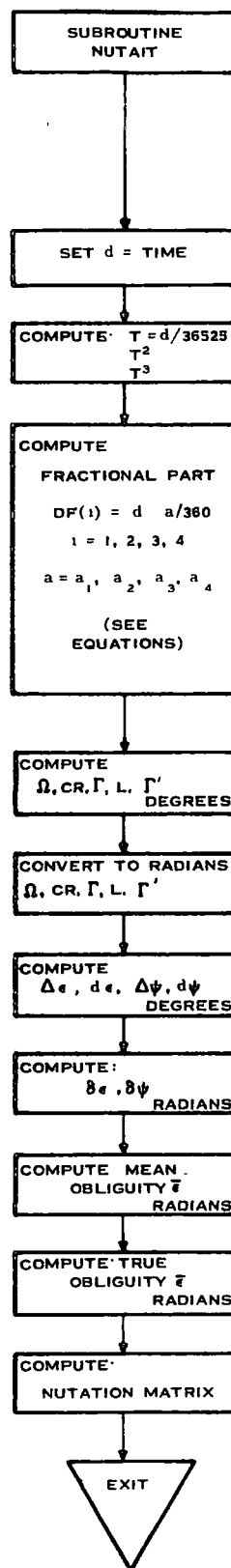
$$N_{32} = \cos \delta\psi \sin \epsilon \cos \bar{\epsilon} - \cos \epsilon \sin \bar{\epsilon}$$

$$N_{33} = \cos \delta\psi \sin \epsilon \sin \bar{\epsilon} + \cos \epsilon \cos \bar{\epsilon}$$

For numerical calculation, the above N matrix is expanded to the first order in $\delta\psi$ and $\delta\epsilon$:

$$N = \begin{vmatrix} 1 & -\delta\psi \cos \bar{\epsilon} & -\delta\psi \sin \bar{\epsilon} \\ \delta\psi \cos \bar{\epsilon} & 1 & -\delta\epsilon \\ \delta\psi \sin \bar{\epsilon} & \delta\epsilon & 1 \end{vmatrix}$$

Reference: JPL Technical Report No. 32-223



S-292

NUTAIT - 6

NUTAIT

WDL-TR2184

```

LABEL
SYMBOL TABLE
SUBROUTINE NUTAIT (TIME,OM,CR,DT,EN,ERSIL)
DIMENSION EN(3,3)
D = TIME
T = D/36525,
T2 = T*T
T3 = T2*T
OM = 12.112790-.052953922*D+.0020795*T+.002081*T2+.000002*T3
CR = 64.375452+13.176397*D-.001131575*T-.00113015*T2+.0000019*T3
GP = 208.84399+.11140408*D-.010334*T-.010343*T2-.000012*T3
VL = 280.08121+.98564734*D+.000303*(T+T2)
G = 282.08053+.0000470684*D+.00045525*T+.0004575*T2+.000003*T3
OM = OM*.017453296
CR = CR*.017453296
GP = GP*.017453296
VL = VL*.017453296
G = G*.017453296
DE = .255844*COSF(OM) -.2511*COSF(2.*OM)+.15336*COSF(2.*VL)
1 +.0666*COSF(3.*VL-G) -.0258*COSF(VL+G) -.0183*COSF(2.*VL-OM)
2 -.0067*COSF(2.*GP-OM)
DD = .2456*COSF(2.*CR) +.0508*COSF(2.*CR-OM) +.0369*COSF(3.*CR-GP)
1 -.0139*COSF(CR+GP) -.0086*COSF(CR-GP+OM) +.0083*COSF(CR-GP-OM)
2 -.0061*COSF(3.*CR+GP-2.*VL) +.0064*COSF(3.*CR-GP-OM)
DT = -(47.8927+.0482*T)*SINF(OM) +.58*SINF(2.*OM)
1 -.3.5361*SINF(2.*VL) -.1378*SINF(3.*VL-G) +.0594*SINF(VL+G)
2 +.0344*SINF(2.*VL-OM) +.0125*SINF(2.*GP-OM) +.35*SINF(VL-G)
3 +.0125*SINF(2.*VL-2.*GP)
DS = -.5658*SINF(2.*CR) -.095*SINF(2.*CR-OM) -.0725*SINF(3.*CR-GP)
1 +.0317*SINF(CR+GP) +.0161*SINF(CR-GP+OM) +.0158*SINF(CR-GP-OM)
2 -.0144*SINF(3.*CR+GP-2.*VL) -.0122*SINF(3.*CR-GP-OM)
3 +.1875*SINF(CR-GP) +.0078*SINF(2.*CR-2.*GP)
4 +.0414*SINF(CR+GP-2.*VL) +.0167*SINF(2.*CR-2.*VL)
5 -.0089*SINF(4.*CR-2.*VL)
DE = .17453296E-5*(DE+DD)
DT = .17453296E-5*(DT+DS)
EB = 23.4457587-.01309404*T+.00000088*T2+.0000005*T3
EB = EB*.017453296
ERSIL = EB+DE
EN(1,1) = 1,
EN(1,2) = -DT*COSF(EB)
EN(1,3) = -DT*SINF(EB)
EN(2,1) = -EN(1,2)
EN(2,2) = 1,
EN(2,3) = -DE
EN(3,1) = -EN(1,3)
EN(3,2) = DE
EN(3,3) = 1,
RETURN
END

```

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Subroutine: OBLN

Purpose: To compute the perturbing acceleration due to the earth's oblateness. The formula for the earth's potential includes the second, third and fourth spherical harmonics. Part of the input is a rotation matrix to equator and equinox of date, obtained by successive calls to ROTEQ, NUTAIT, and MULT. It also computes the first variation of the perturbing acceleration for the variational equations.

Calling Sequence:

CALL OBLN (XP, U, A, VJ, H, D, PO, AN, B, NEQ)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	XP	3	\bar{R}	Kilometers	Position vector
I	U	1	μ	Km ³ /sec ²	Gravitational constant
I	A	1	R_E	Kilometers	Equatorial radius of the earth
I	VJ	1	J		Coefficient of second harmonic
I	H	1	H		Coefficient of third harmonic
I	D	1	D		Coefficient of fourth harmonic
O	PO	3	∇U		Perturbing acceleration
I	AN	3,3			Rotation matrix to equator and equinox of date

(Cont'd.)

Common storages used or required:

None

Subroutines required:

None

Functions required:

SORT

Approximate number of storages required:

480 DEC

(Cont'd.)

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	B	3,3	$\partial \ddot{x}_i / \partial x_i$		Derivatives of ∇U
I	NEQ	1			Number of differential equations
					being integrated

OBLN computes the perturbing acceleration due to the earth's oblateness. The oblate potential of the earth is assumed to contain the second, third, and fourth spherical harmonics:

$$U = \frac{\mu}{R} \left\{ \frac{J R_E}{3R^2} (1 - 3 \sin^2 \phi) + \frac{H R_E^3}{5R^3} (3 \sin \phi - 5 \sin^3 \phi) + \frac{D R_E^4}{35R^4} (3 - 30 \sin^2 \phi + 35 \sin^4 \phi) \right\}$$

where R_E is the equatorial radius of the earth and ϕ is the geocentric latitude, $\bar{R} = (X_1, X_2, X_3)$ is expressed in the mean equator and equinox of 1950.

The position vector $\bar{r} = (X, Y, Z)$ expressed in the true equator and equinox of date must be obtained to determine $\sin \phi$. The proper rotation matrix AN has been computed. Then,

$$\bar{r} = AN \bar{R}$$

and

$$\sin \phi = \frac{Z}{R}.$$

The perturbing acceleration is equal to ∇U :

$$\frac{\partial U}{\partial X_j} = -J\mu \frac{R_E^2}{R^4} \left\{ \left(1 - \frac{5Z^2}{R^2}\right) \frac{X_j}{R} + 2 \frac{Z}{R} AN_{3j} \right\}$$

$$-H\mu \frac{R_E^3}{R^5} \left\{ \left(3 - \frac{7Z^2}{R^2}\right) \frac{Z}{R} \frac{X_j}{R} + \left(-\frac{3}{5} + \frac{3Z^2}{R^2}\right) AN_{3j} \right\}$$

$$-D\mu \frac{R_E^4}{R^6} \left\{ \left(\frac{3}{7} - \frac{6Z^2}{R^2} + \frac{9Z^4}{R^4}\right) \frac{X_j}{R} + \left(\frac{12}{7} - \frac{4Z^2}{R^2}\right) \frac{Z}{R} AN_{3j} \right\}$$

for $j = 1, 2, 3$.

If the number of second order differential equations is less than or equal to three, RETURN is called at this point.

OBLN also computes the derivatives of the perturbing acceleration for use in the integration package. For this purpose, only the term arising from the second harmonic is retained; also, the coordinates are regarded as being expressed in the reference system of the mean equator and equinox of 1950.

Starting with

$$\nabla U_a = \left(g_1 \frac{X_1}{R}, g_2 \frac{X_2}{R}, g_3 \frac{X_3}{R} \right)$$

where

$$g_1 = -J\mu \frac{R_E^2}{R^4} \left(1 - \frac{5Z^2}{R^2}\right)$$

$$g_2 = -J\mu \frac{R_E^2}{R^4} \left(3 - \frac{5Z^2}{R^2}\right)$$

yields

$$\frac{\partial \ddot{x}_1}{\partial x_j} = g_1 \frac{x_1}{R} \left(\frac{1}{x_1} \frac{\partial x_1}{\partial x_j} - \frac{3}{R^2} \bar{R} \cdot \frac{\partial \bar{R}}{\partial x_j} \right) \\ + J\mu R_E^2 \frac{x_1}{R^7} \left\{ 10x_3 \frac{\partial x_3}{\partial x_j} + 2 \left(1 - 10 \frac{x_3^2}{R^2} \right) \bar{R} \cdot \frac{\partial \bar{R}}{\partial x_j} \right\}$$

$$\frac{\partial \ddot{x}_2}{\partial x_j} = g_1 \frac{x_2}{R} \left(\frac{1}{x_2} \frac{\partial x_2}{\partial x_j} - \frac{3}{R^2} \bar{R} \cdot \frac{\partial \bar{R}}{\partial x_j} \right) \\ + J\mu R_E^2 \frac{x_2}{R^7} \left\{ 10x_3 \frac{\partial x_3}{\partial x_j} + 2 \left(1 - 10 \frac{x_3^2}{R^2} \right) R \cdot \frac{\partial R}{\partial x_j} \right\}$$

$$\frac{\partial \ddot{x}_3}{\partial x_j} = g_2 \frac{x_3}{R} \left(\frac{1}{x_3} \frac{\partial x_3}{\partial x_j} - \frac{3}{R^2} \bar{R} \cdot \frac{\partial \bar{R}}{\partial x_j} \right) \\ + J\mu R_E^2 \frac{x_3}{R^7} \left\{ 10x_3 \frac{\partial x_3}{\partial x_j} + 2 \left(3 - 10 \frac{x_3^2}{R^2} \right) R \cdot \frac{\partial R}{\partial x_j} \right\}$$

Expanding the dot products and collecting terms gives

$$B_{11} = g_1 \left(\frac{1}{R} - \frac{3x_1^2}{R^3} \right) + 2J\mu R_E^2 \frac{x_1^2}{R^7} \left(1 - 10 \frac{x_3^2}{R^2} \right)$$

$$B_{12} = g_1 \left(-\frac{3x_1 x_2}{R^3} \right) + 2 J\mu R_E^2 \frac{x_1 x_2}{R^7} \left(1 - 10 \frac{x_3^2}{R^2} \right)$$

$$B_{13} = g_1 \left(-\frac{3X_1X_3}{R^3} \right) + 2 J\mu R_E^2 \frac{X_1X_3}{R^7} \left(6 - 10 \frac{X_3^2}{R^2} \right)$$

$$B_{21} = B_{12}$$

$$B_{22} = g_1 \left(\frac{1}{R} - \frac{3X_2^2}{R^3} \right) + 2 J\mu R_E^2 \frac{X_2^2}{R^7} \left(1 - 10 \frac{X_3^2}{R^2} \right)$$

$$B_{23} = g_1 \left(-\frac{3X_2X_3}{R^3} \right) + 2 J\mu R_E^2 \frac{X_2X_3}{R^7} \left(6 - 10 \frac{X_3^2}{R^2} \right)$$

$$B_{31} = B_{13}$$

$$B_{32} = B_{23}$$

$$B_{33} = g_2 \left(\frac{1}{R} - \frac{3X_3^2}{R^3} \right) + 2 J\mu R_E^2 \frac{X_3^2}{R^7} \left(8 - 10 \frac{X_3^2}{R^2} \right)$$

where $B\lambda_j = \frac{\partial \ddot{X}_i}{\partial X_j}$

For $R > 3R_E$, B is set equal to zero.

```

* LABEL
* SYMBOL TABLE
CEC2031 SUBROUTINE OBLN
SUBROUTINE OBLN(XP,U,A,VJ,H,D,PO,AN,B,NEQ)
DIMENSION X(3),PO(3),AN(3,3),XP(3),B(3,3)
RE=6378.15
DO 2 I=1,3
X(I) = 0.
DO 2 J=1,3
2 X(I) = X(I) + AN(I,J)*XP(J)
R2 = X(1)**2+X(2)**2+X(3)**2
R = SQRTF(R2)
UR2 = U/R2
AR = A/R
AR2 = AR*AR
AR3 = AR*AR2
AR4 = AR*AR3
ZR = X(3)/R
ZR2 = ZR*ZR
ZR4 = ZR2*ZR2
TM1 = (1.-5.*ZR2)/R
TM2 = 2.*ZR
TM3 = (3.-7.*ZR2)*ZR/R
TM4 = -.6+3.*ZR2
TM5 = (.42857143-6.*ZR2+9.*ZR4)/R
TM6 = (1.7142857-4.*ZR2)*ZR
TO1 = -VJ*UR2*AR2
TO2 = -H*UR2*AR3
TO3 = -D*UR2*AR4
DO 1 I=1,3
1 PO(I) = TO1*(TM1*XP(I)+TM2*AN(3,I))
2      + TO2*(TM3*XP(I)+TM4*AN(3,I))
2      + TO3*(TM5*XP(I)+TM6*AN(3,I))
IF(NEQ=3)3,3,4
3 CONTINUE
RETURN
4 CONTINUE
IF(R=3.*RE)5,5,6
6 CONTINUE
DO 7 I=1,3
DO 7 J=1,3
B(I,J)=0.
7 CONTINUE
GO TO 3
5 CONTINUE
G5=-TO1/R
G6=5.*ZR2
G1=-G5*(1.-G6)
G2=-G5*(3.-G6)
G7=2.*G6
G8=X(1)/R

```

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OBLN
OBLN
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OBLN0000
OBLN0010
OBLN0020
OBLN0030
OBLN0040
OBLN0050
OBLN0060
OBLN0070
OBLN0080
OBLN0090
OBLN0100
OBLN0110
OBLN0120
OBLN0130
OBLN0140
OBLN0150
OBLN0160
OBLN0170
OBLN0180
OBLN0190
OBLN0200
OBLN0210
OBLN0220
OBLN0230
OBLN0240
OBLN0250
OBLN0260
OBLN0270
OBLN0280
OBLN0290
OBLN0300
OBLN0310
OBLN0320
OBLN0330
OBLN0340
OBLN0350
OBLN0360
OBLN0370
OBLN0380
OBLN0390
OBLN0400
OBLN0410
OBLN0420
OBLN0430
OBLN0440
OBLN0450
OBLN0460
OBLN0470

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G9=X(2)/R
G10=X(3)/R
B(1,1)=G1*(1,-3,*G8**2)*2.*G5*G8**2*(1,-G7)
B(1,2)=-3.*G1*G8*G9+2.*G5*G8*G9*(1,-G7)
B(1,3)=-3.*G1*G8*G10+2.*G5*G8*G10*(6,-G7)
B(2,1)=B(1,2)
B(2,2)=G1*(1,-3,*G9**2)+2.*G5*G9**2*(1,-G7)
B(2,3)=-3.*G1*G9*G10+2.*G5*G9*G10*(6,-G7)
B(3,1)=B(1,3)
B(3,2)=B(2,3)
B(3,3)=G2*(1,-3,*G10**2)+2.*G5*G10**2*(8,-G7)
GO TO 3
END

OBLN048
OBLN049
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OBLN051
OBLN052
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OBLN059
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OBLN -

S-301

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Subroutine: ONBTR

WDL-TR2184

Purpose: The subroutine obtains the relative position and velocity vectors from the vehicle to any of the six following bodies; Earth, Moon, Sun, Venus, Mars, and Jupiter. The bodies to be observed are established by input data. The types of observation which can be made on the body are range, range rate, right ascension, and declination. The selection of types of measurements to be made is also by input data. ONBTR calls subroutine COMPHO to perform the updating of the covariance matrix for observations being made.

Calling Sequence:

CALL ONBTR

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities placed in common

Common storages used or required:

T, S, C, IC

Subroutines required:

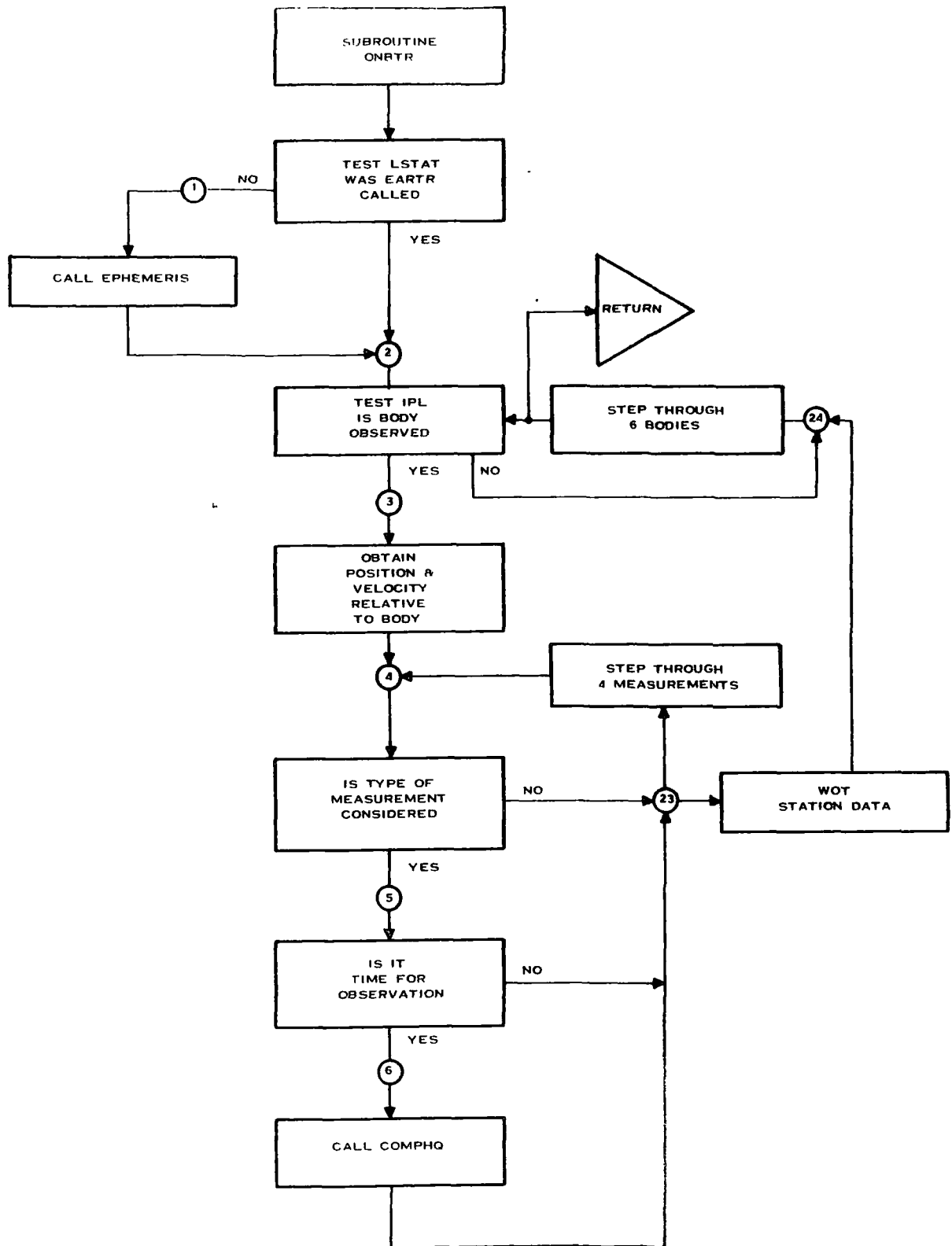
COMPHO, INTRI

Functions required:

ASIN, ATAN, FNORM, SQRT,
(FIL)(SLO)(STH)

Approximate number of storages required:

267 DEC



ONP

* LABEL
* SYMBOL TABLE

CEC2007

SUBROUTINE ONBTR

SUBROUTINE ONBTR UPDATES COVARIANCE MATRIX FOR ONBOARD
MEASUREMENTS OF RANGE, RIGHT ASCENSION, DECLINATION, AND
RANGE RATE RELATIVE TO THE 6 CELESTIAL BODIES

COMMON T,S,C,IC

DIMENSION PO(22),VE(22),IMPLAN(4,6),IPL(6),X(3),VX(3)

1,T(1360),S(1000),C(1000),IC(1),XREL(3),VREL(3)

2,TLAST(4,6),OBRATE(4,6),H(6),P(6,6),OUTPUT(6)

EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM)

1,(IC(110),IPL),(IC(116),IMPLAN),(C(15),X),(C(18),VX)

2,(IC(3),NOR),(C(13),TW),(C(14),TF),(IC(190),LSTAT)

3,(C(649),TSECP),(C(30),TSEC),(S(437),OBRATE),(C(652),P)

4,(C(622),TLAST),(C(62),PO),(C(84),VE)

1,(C(895),XREL),(C(898),VREL),(C(894),OBNO),(C(893),XMAG)

2(C(892),DEX),(C(891),DEN1),(C(890),DEN2),(S(72),DR)

3,(C(889),DEX2),(C(888),DEX3),(C(652),P),(C(973),OUTPUT)

CALL SETN(NIN,NUTS)

LSTAT=LSTAT

GO TO (1,2),LSTAT

1 CONTINUE

NB=NOR-1

DIS=1.E10

CALL INTR1(TW,TF,NB,PO,1,VE,DIS)

2 CONTINUE

DO 24 JJ=1,6

JJ DETERMINES BODY TO BE OBSERVED 1,EARTH 2,MOON 3,SUN

4,VENUS 5,MARS 6,JUPITER

IF(IPL(JJ))24,24,3

3 CONTINUE

LM=26-3*(JJ)

DO 4 I=1,3

MM=LM-I

XREL(I)=PO(MM)-X(I)

VREL(I)=VE(MM)-VX(I)

4 CONTINUE

XREL=VECTOR FROM VEHICLE TO JJ-TH PLANET,EQUINOX 1950

VREL=RELATIVE VELOCITY VECTOR

XMAG=FNORM(XREL)

DEX=XREL(1)**2+XREL(2)**2

DEN1=1./SQRTF(DEX)/XMAG**2

DEN2=1./DEX

DEX2=XMAG*XMAG

DEX3=1./XMAG

THE ABOVE QUANTITIES ARE USED IN COMPUTATIONS OF H MATRIX

DELTT=TSEC-TSECP

DEC=ASINF(DEX3*XREL(3))

OUTPUT(5)=DEC/DR

RA=ATANF(XREL(2)/XREL(1))

ONBT

ONBT

ONBT

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ONBT001

ONBT002

ONBT003

ONBT004

ONBT005

ONBT006

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ONBT036

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ONBT039

ONBT040

ONBT041

ONBT042

ONBT043

ONBT043

ONBT043

ONBT043

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      OUTPUT(3)=RA/DR
      OUTPUT(1)=XMAG
      DO 23 JJJ=1,4
      IF(IMPLAN(JJJ,JJ))23,23,5
5     CONTINUE
      TLAST(JJJ,JJ)=TLAST(JJJ,JJ)+DELTT
C     TLAST STORES TIME SINCE LAST JJJ TYPE OF OBSERVATION OF JJ BODY
C     JJJ DETERMINES TYPE OF OBS. 1-RANGE, 2-RIGHT ASCENSION,
C     3-DECLINATION, 4-RANGE RATE
      NOB=TLAST(JJJ,JJ)/OBRATE(JJJ,JJ)
      OBNO=NOB
      IF(NOB)23,23,6
6     CONTINUE
      JJJ=JJJ
      NN=426
      CALL COMPHQ(JJJ,1,NN)
      TLAST(JJJ,JJ)=TLAST(JJJ,JJ)+OBNO*OBRATE(JJJ,JJ)
23    CONTINUE
      WRITE OUTPUT TAPE NUTS,700,JJ,OUTPUT
700   FORMAT(16H CELESTIAL BODY ,I2,
1/4H RGE15.8,5H RGRE15.8,
25H RAE15.8,5H RARE15.8,5H DECE15.8,5H DCRE15.8)
      DO 20 I=1,6
20    OUTPUT(I)=0.
24    CONTINUE
      RETURN
      END

```

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ONBT0438
ONBT0439
ONBT0440
ONBT0450
ONBT0460
ONBT0470
ONBT0480
ONBT0490
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ONBT0590
ONBT0591
ONBT0592
ONBT0593
ONBT0594
ONBT0595
ONBT0596
ONBT0600
ONBT0610
ONBT

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Subroutine: ORTC

Purpose: To convert Cartesian coordinates to conic elements for the output subroutines and to provide other auxiliary results used in computations in the output subroutine.

Calling Sequence:

CALL ORTC (X, DX, U, SMA, ECC, RCA, OINC, OMG, BEP, B, B2,
R2, V2, A, C3, BET, THT)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	X	3	\vec{R}	Km	Position vector
I	VX	3	\vec{V}	Km/sec	Velocity vector
I	U	1	μ	Km ³ /sec ²	Central body gravitational constant
O	SMA	1	a	Km	Semi-Major Axis
O	ECC	1	e		Eccentricity
O	RCA	1	V_p	Km	Radius of closest approach
O	OINC	1	i	RAD	Orbital inclination

(Cont'd.)

Common storages used or required: _____

Subroutines required: _____

Functions required: _____

Approximate number of storages required: _____

(Cont'd.)

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	OMG	1	Ω	RAD	Argument of ascending node
O	BEP	1	ω	RAD	
O	B	3	$\vec{R} \times \vec{V}$		Quantities used in output
O	B2	1	$ \vec{R} \times \vec{V} ^2$		subroutine computations
O	R2	1	$ \vec{R} ^2$	Km ²	
O	V2	1	$ \vec{V} ^2$	(Km/sec) ²	
O	A	1	$\vec{R} \cdot \vec{V}$		
O	C3	1	$v^2 - \frac{2\mu}{R}$	(Km/sec) ²	
O	BET	1	η	RAD	
O	THT	1	θ	RAD	

The orbital elements determined by the subroutine are the following:

$$C3 = v^2 - \frac{2\mu}{R} \quad \vec{R} \times \vec{V} = \vec{h}$$

Semi-Major Axis

$$a = \text{SMA} = \frac{\mu}{|C3|}$$

Eccentricity

$$e = \text{ECC} = \sqrt{1 + \frac{C3}{\mu^2} |\vec{R} \times \vec{V}|^2} = \sqrt{1 + \frac{C3}{\mu^2} |\vec{h}|^2}$$

Radius of Closest Approach

$$v_p = RCA = \frac{|\vec{R} \times \vec{v}|^2}{\mu(1+e)} = \frac{|\vec{h}|^2}{\mu(1+e)}$$

Orbital Inclination

$$i = OINC = \tan^{-1} \frac{\sqrt{h^2(1) + h^2(2)}}{h(3)}$$

Argument of the Ascending node

$$\Omega = OMG = \tan^{-1} \frac{h(1)}{-h(2)}$$

True Anomaly

$$\theta = THT = \tan^{-1} \frac{(\vec{X} \cdot \vec{v}) |\vec{h}|}{|\vec{h}|^2 - \mu R}$$

Argument of Periapsis plus True Anomaly

$$n = BET = \frac{X(3) |\vec{h}|}{X(2) h(1) - X(1) h(2)}$$

Argument of Periapsis

$$\omega = BEP = BET - THT$$

```

* LABEL
* SYMBOL TABLE
SUBROUTINE ORTC(X,DX,U,SMA,ECC,RCA,OINC,OMG,BEP
1,B,B2,R2,V2,A,C3,BET,THT)
DIMENSION X(3),DX(3),B(3)
CALL CROSS(X,DX,B)
R2 = DOT(X,X)
V2 = DOT(DX,DX)
B2 = DOT(B,B)
A = DOT(X,DX)
BB = SQRTF(B2)
R = SQRTF(R2)
C3 = V2-2.*U/R
SMA = U/ABSF(C3)
ECC = SQRTF(1.+C3*B2/U**2)
OINC = ARKTNS(180,B(3),SQRTF(B(1)**2+B(2)**2))
OMG = ARKTNS(360,-B(2),B(1))
RCA = B2/(U*(1.+ECC))
P = B2/U
THT = ARKTNS(360,U*(P-R),BB*A)
BET = ARKTNS(360,X(2)*B(1)-X(1)*B(2),X(3)*BB)
BEP = BET-THT
IF(BEP) 2,3,3
2 BEP=BEP+6.2831853
3 CONTINUE
RETURN
END

```

```

ORTC
ORTC
ORTC0000
ORTC0010
ORTC0020
ORTC0030
ORTC0040
ORTC0050
ORTC0060
ORTC0070
ORTC0080
ORTC0090
ORTC0100
ORTC0110
ORTC0120
ORTC0130
ORTC0140
ORTC0150
ORTC0160
ORTC0170
ORTC0180
ORTC0190
ORTC0200
ORTC0210
ORTC0220
ORTC0230
ORTC

```

Subroutine: OUTC

Purpose: OUTC writes out the trajectory elements in a coordinate system and reference system specified by an input quantity (KOUT). OUTC also writes out the orbital parameters found in ORTC, and writes out the selenographic latitude and longitude if the system is moon-centered.

Calling Sequence:

CALL OUTC

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
KOUT	IC(7)				0 for output in date
					1 for output in 1950
					2 for output in ecliptic coord.

Common storages used or required:

T, S, C, IC

Subroutines required:

see next page

Functions required:

see next page

Approximate number of storages required:

decimal 940; octal 1654

Subroutines Required

ECLIP

GHA

INTRI

MNAND

NMA

MULT

NUTAIT

ORTC

OUTDAT

ROTATE

ROTEQ

RVOUT

SETN

Functions Required

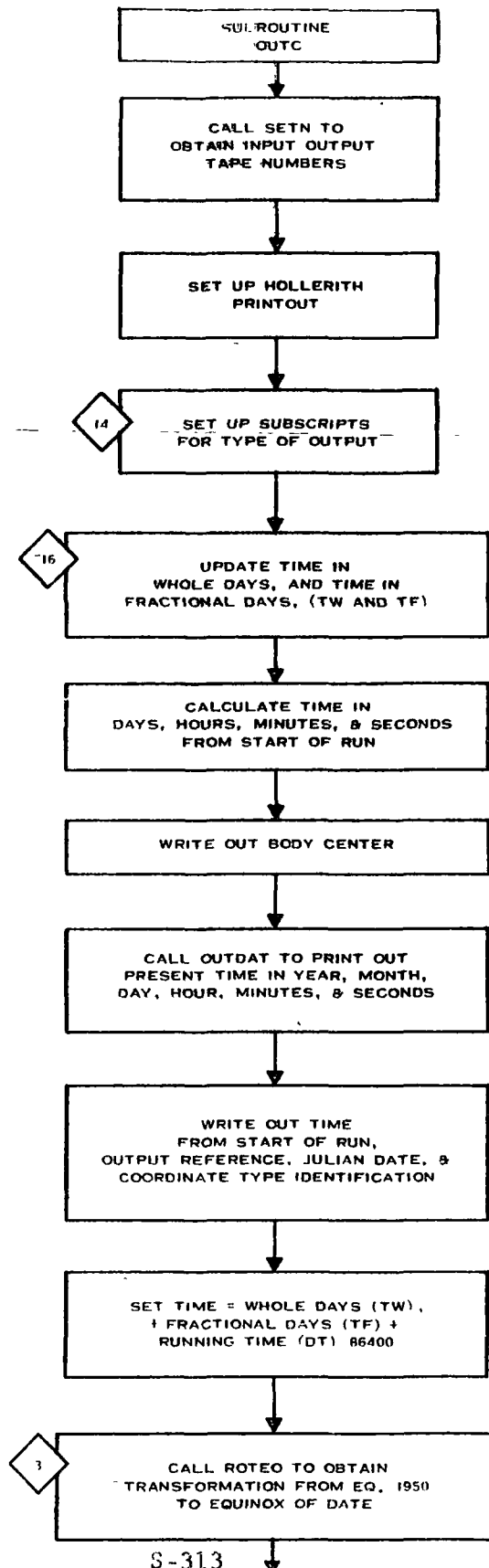
ARKTNS

ATAN

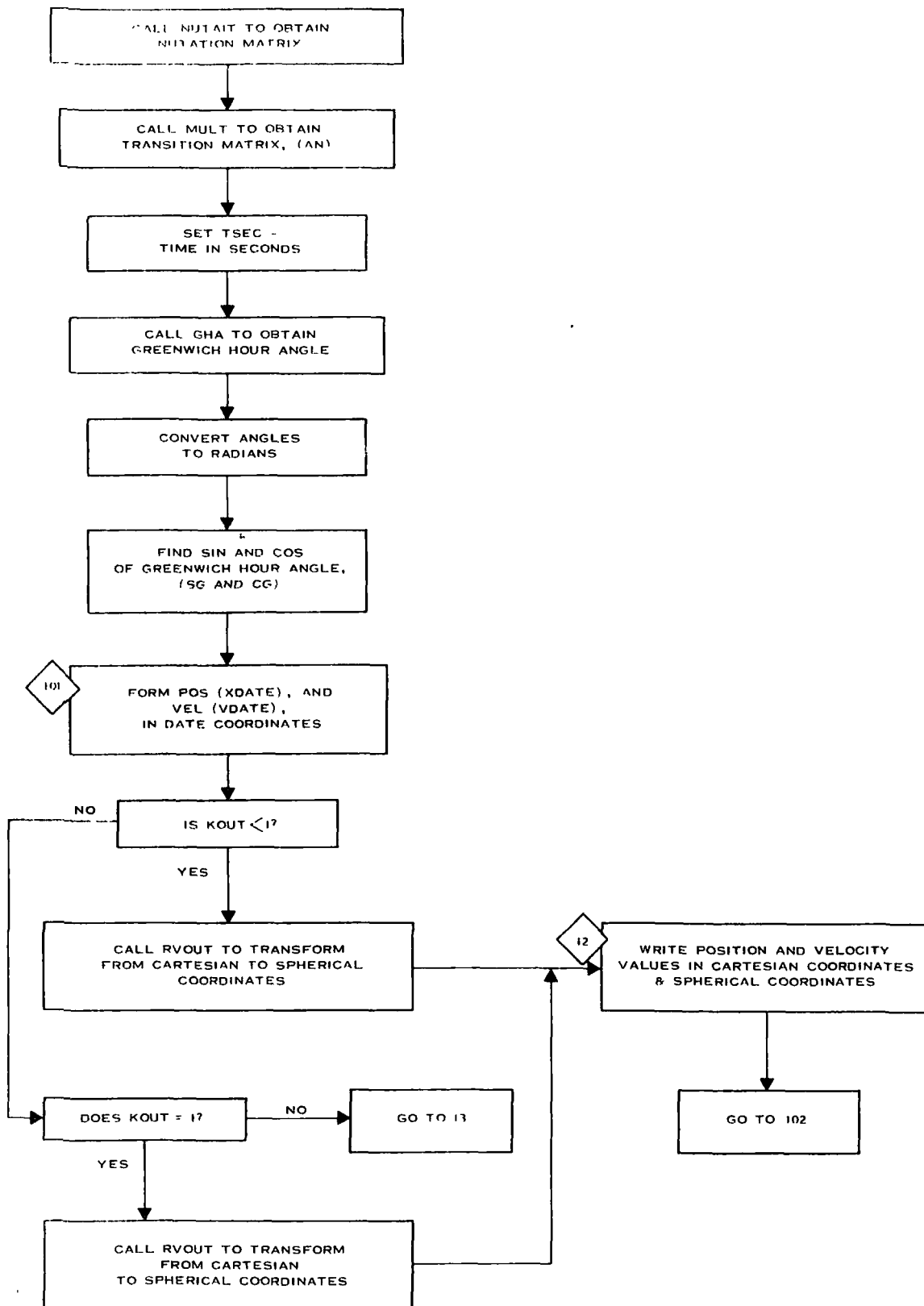
COS

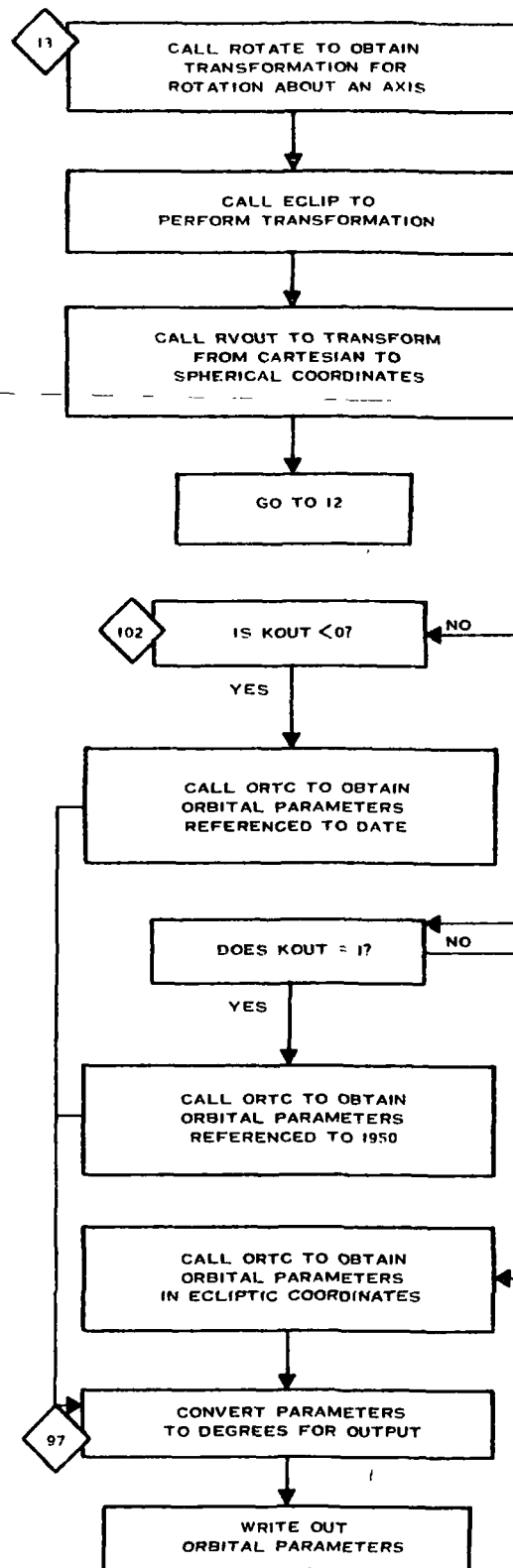
SIN

SORT



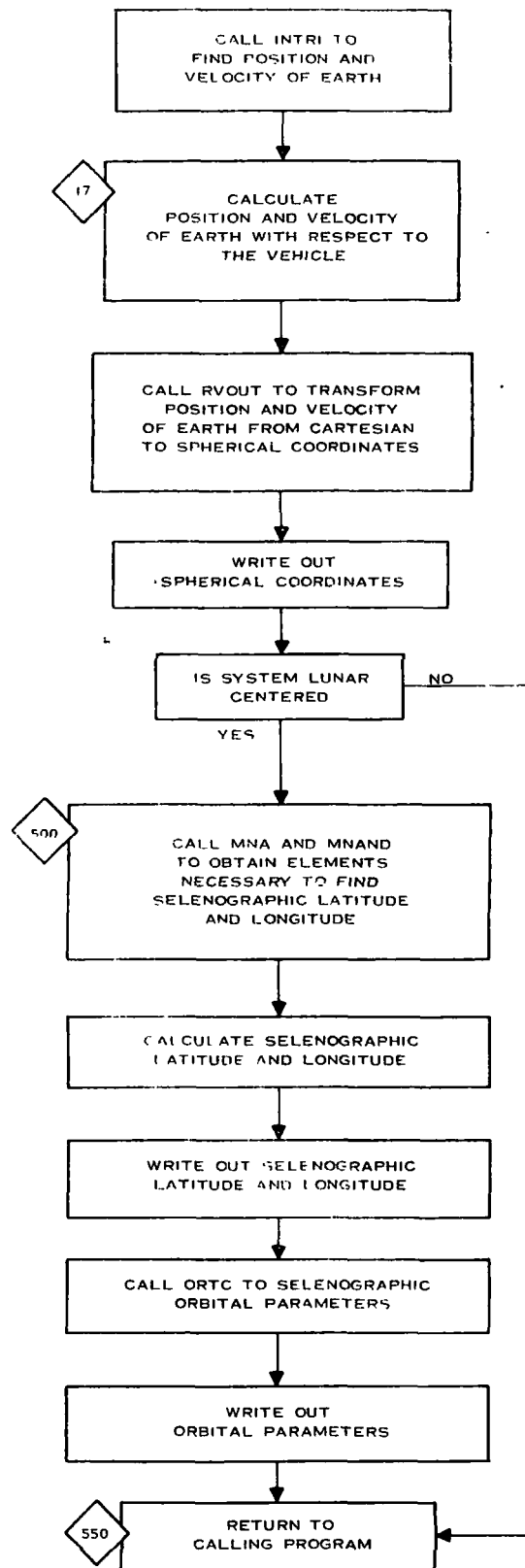
OUTC - 3





OUTC - 5

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```

* LABEL OUTC
* SYMBOL TABLE OUTC
CEC2015 SUBROUTINE OUTC OUTC
SUBROUTINE OUTC OUTC000
COMMON T,S,C,IC OUTC001
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),(IC,ICDUM) OUTC002
EQUIVALENCE (T(2),DT),(C(15),XP),(C(18),VXP),(C(129),EA) OUTC003
1,(C(120),EN),(C(138),AN),(C(62),PO),(C(84),VE),(C(10),TW) OUTC004
2,(C(11),TF),(IC(3),NOR),(IC(6),ITARG),(IC(7),KOUT),(C(55),U) OUTC005
3,(S(73),RTD),(C(180),SMA),(C(181),ECC),(C(182),RCA),(C(183),OINC) OUTC006
4,(C(184),OMG),(C(185),BEP),(C(186),XED),(C(189),VED) OUTC007
5,(C(156),ECX),(C(159),ECV),(C(147),ECL),(C(30),T2) OUTC008
6,(C(192),RCV),(C(195),RCV2),(C(196),R2),(C(197),V2),(C(198),RDV) OUTC009
7,(C(199),C3),(C(162),BET),(C(163),THT) OUTC010
DIMENSION T(1360),S(1000),C(1000),IC(1) OUTC011
DIMENSION XP(3),VXP(3),EA(3,3),EN(3,3),B(3,3),AN(3,3), OUTC012
1 BAN(3,3),PO(22),VE(22),XDATE(3),VDATE(3),XEARTH(3),VEARTH(3), OUTC013
2SPDATE(6),ECX(3),ECV(3),CNAME(6),VEV(3) OUTC014
DIMENSION XED(3),VED(3),PEV(3),RCV(3),RCVM(3) OUTC015
DIMENSION ANAME(2) OUTC016
DIMENSION BNAME(4) OUTC017
DIMENSION ECL(3,3) OUTC018
DIMENSION POS(3),VES(3),POM(3),VEM(3),POT(3),VET(3) OUTC019
CALL SETN(NIN,NOUT) OUTC019
ANAME(1) = 6H DATE OUTC020
ANAME(2) = 6H1950.0 OUTC021
BNAME(1) = 6H EC OUTC022
BNAME(2) = 6H LIPTIC OUTC023
BNAME(3) = 6H EQUA OUTC024
BNAME(4) = 6H TORIAL OUTC025
CNAME(1)=6H EARTH OUTC026
CNAME(2)=6H MOON OUTC027
CNAME(3)=6H SUN OUTC028
CNAME(4)=6H VENUS OUTC029
CNAME(5)=6H MARS OUTC030
CNAME(6)=6H JUPITR OUTC031
202 CONTINUE OUTC032
KO=KOUT OUTC033
NOR = NOR OUTC034
IF (KOUT-1) 14,14,15 OUTC035
14 KT = 3 OUTC036
GO TO 16 OUTC037
15 KT = 1 OUTC038
KO=0 OUTC039
16 CONTINUE OUTC040
TP2 = TF+DT/86400. OUTC041
TWGN=0. OUTC042
32 CONTINUE OUTC043
IF(TP2) 33,34,34 OUTC044
33 CONTINUE OUTC045
TP2=TP2+1. OUTC046

```

	TWGN=TWGN-1.	OUTC0470
	GO TO 32	OUTC0480
34	CONTINUE	OUTC0490
	TFP = INTF(TP2)	OUTC0500
	TP2 = TP2-TFP	OUTC0510
	TP1=TW+TFP+TWGN	OUTC0520
	IT1=T2/86400.	OUTC0530
	DT1=IT1	OUTC0540
	DT1=T2-DT1*86400.	OUTC0550
	IT2=DT1/3600.	OUTC0560
	DT2=IT2	OUTC0570
	DT2=DT1-DT2*3600.	OUTC0580
	IT3=DT2/60.	OUTC0590
	DT3=IT3	OUTC0600
	DT3=DT2-DT3*60.	OUTC0610
	TT = INTF(TP2+.5)	OUTC0620
	TP2P = TP2+.5-TT	OUTC0630
	TP1P = TP1 + TT + 2433282.	OUTC0640
	WRITE OUTPUT TAPE NOUT,702,CNAME(NOR)	OUTC0650
702	FORMAT (//1H0A6,10H CENTERED)	OUTC0660
	CALL OUTDAT(TP1,TP2)	OUTC0670
	WRITE OUTPUT TAPE NOUT,2,IT1,IT2,IT3,DT3,ANAME(KO +1),TP1P,TP2P	OUTC0680
	1 ,BNAME(KT),BNAME(KT+1)	OUTC0690
2	FORMAT(I4,5H DAYSI4,5H HRS.I4,5H MIN.F7.2,5H SEC.4XA6,3X12HJULIAN	OUTC0700
1	DATE F8.0,F8.8,10X2A6,12H COORDINATES)	OUTC0710
	N = NOR	OUTC0720
	TIME = TW+TF+DT/86400.	OUTC0730
	DIS = 1.E10	OUTC0740
	NR1 = N-1	OUTC0750
	NV = 1	OUTC0760
3	CALL ROTEQ(TIME,EA)	OUTC0770
	CALL NUTAIT(TIME,WM,CR,DA,EN,EPSIL)	OUTC0780
	CALL MULT(EN,EA,AN,0)	OUTC0790
	TSEC = 86400.*TP2	OUTC0800
	CALL GHA(TSEC,TP1,GHAN,EN(2,1),OMEGA)	OUTC0810
	GHAN = GHAN*.017453296	OUTC0820
	OMEGA = OMEGA*.017453296	OUTC0830
	SG = SIN(GHAN)	OUTC0840
	CG = COS(GHAN)	OUTC0850
	DO 1 I=1,3	OUTC0860
	XDATE(I) = 0.	OUTC0870
	VDATE(I) = 0.	OUTC0880
	DO 101 J=1,3	OUTC0890
	XDATE(I) = XDATE(I) + AN(I,J)*XP(J)	OUTC0900
	VDATE(I) = VDATE(I) + AN(I,J)*VXP(J)	OUTC0910
101	CONTINUE	OUTC0920
	XED(I)=XDATE(I)	OUTC0930
	VED(I)=VDATE(I)	OUTC0940
1	CONTINUE	OUTC0950
	IF (KOUT-1) 11,10,13	OUTC0960
10	CALL RVOUT(XP,VXP,SPDATE)	OUTC0970

```

WRITE OUTPUT TAPE NOUT,5,XP,VXP,SPDAT
GO TO 102
11 CALL RVOUT(XDATE,VDATE,SPDATE)
12 WRITE OUTPUT TAPE NOUT,5,XDATE,VDATE,SPDATE
GO TO 102
13 CALL ROTATE(1,EPSIL,ECL,1)
CALL ECLIP(XDATE,VDATE,ECL)
CALL RVOUT(XDATE,VDATE,SPDATE)
DO 103 I=1,3
  ECX(I)=XDATE(I)
103 ECV(I)=VDATE(I)
GO TO 12
102 CONTINUE
5 FORMAT(4H -- XE15.8,5H YE15.8,5H ZE15.8,5H DXE15.8,
1 5H DYE15.8,5H DZE15.8/4H RE15.8,5H DECE15.8,5H RAE15.8,
2 5H VE15.8,5H PTHE15.8,5H AZE15.8)
IF (KOUT-1) 105,106,107
105 CALL ORTC(XED,VED,U,SMA,ECC,RCA,OINC,OMG,BEP
1,RCV,RCV2,R2,V2,RDV,C3,BET,THT)
GO TO 97
106 CALL ORTC(XP,VXP,U,SMA,ECC,RCA,OINC,OMG,BEP
1,RCV,RCV2,R2,V2,RDV,C3,BET,THT)
GO TO 97
107 CALL ORTC(ECX,ECV,U,SMA,ECC,RCA,OINC,OMG,BEP
1,RCV,RCV2,R2,V2,RDV,C3,BET,THT)
97 CONTINUE
ORIN =OINC*RTD
OMEG =OMG*RTD
APF =BEP*RTD
WRITE OUTPUT TAPE NOUT,4,SMA,ECC,ORIN,OMEG,APF,RCA
CALL INTR1(TP1,TP2,NR1,PO,NV,VE,DIS)
DO 17 I=1,3
  I4=23-I
  PEV(I)=PO(I4)-XP(I)
  VEV(I)=VXP(I)-VE(I4)
17 CONTINUE
DO 108 I=1,3
  XDATE(I)=0.
  VDATE(I)=0.
DO 108 J=1,3.
  XDATE(I)=XDATE(I)-AN(I,J)*PEV(J)
108 VDATE(I)=VDATE(I)+AN(I,J)*VEV(J)
22 XEARTH(3) = XDATE(3)
VEARTH(3) = VDATE(3)
XEARTH(1) = XDATE(1)*CG + XDATE(2)*SG
XEARTH(2) = -XDATE(1)*SG + XDATE(2)*CG
VEARTH(1)=VDATE(1)*CG+VDATE(2)*SG
VEARTH(2)=-VDATE(1)*SG+VDATE(2)*CG
CALL RVOUT(XEARTH,VEARTH,SPDATE)
WRITE OUTPUT TAPE NOUT,31,SPDATE
31 FORMAT(4H RTEE15.8,5H LATE15.8,

```

3.5H	LONE15.8,5H	VEE15.8,5H	PTEE15.8,5H	AZEE15.8)	OUTC1490
29	CONTINUE.				OUTC1500
	IF(N-2)550,500,550				OUTC1510
500	CALL MNA(TIME,WM,CR,DA,EPSIL,RR,G,GP,WW,BAN)				OUTC1520
	DO 510 I=1,3				OUTC1540
	XDATE(I)=0.				OUTC1550
	VDATE(I)=0.				OUTC1560
	DO 510 J=1,3				OUTC1570
	XDATE(I)=XDATE(I)+BAN(I,J)*XED(J)				OUTC1580
510	VDATE(I)=VDATE(I)+BAN(I,J)*VED(J)				OUTC1590
	SLAT=XDATE(3)/SQRTF(XDATE(1)**2+XDATE(2)**2)				OUTC1600
	SLAT=ATANF(SLAT)*RTD				OUTC1610
	SLNG=ARKTNS(360,XDATE(1),XDATE(2))*RTD				OUTC1620
	WRITE OUTPUT TAPE NOUT,701,SLNG,SLAT				OUTC1630
701	FORMAT(19H SELENOGRAPHIC LON=,E17.8,5H LAT=,E17.8)				OUTC1640
	CALL ORTC(XDATE,VDATE,U,AMS,EPS,RP,ORIN,OMEG,APF				OUTC1650
	1,RCVM,RCVM2,R2M,V2M,RDVM,C3M,BETM,THTM)				OUTC1660
	OMEG= OMEG*RTD				OUTC1670
	ORIN = ORIN*RTD				OUTC1680
C	GIVES CALENDER DATE FROM T1(WHOLE DAYS FROM 1950)				OUTC1690
C	ANDT2(FRACT OF DAY)				OUTC1700
	APF = APF*RTD				OUTC1710
	WRITE OUTPUT TAPE NOUT,4,AMS,EPS,ORIN,OMEG,APF,RP				OUTC1720
4	FORMAT (4H SMAE15.8,5H ECCE15.8,5H INCE15.8,5H LANE15.8,				OUTC1730
1	5H APFE15.8,5H RCAE15.8)				OUTC1740
550	RETURN				OUTC1750
	END				OUTC

Subroutine: OUTDAT

Purpose: OUTDAT finds and outputs the calendar date and Julian date, given the number of days since 1950.0.

Calling Sequence:

CALL OUTDAT (T1, T2)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	T1	1		days	Integral number of days from 1950.0.
I	T2	1		days	Fraction of day past T1

Common storages used or required:

None

Subroutines required:

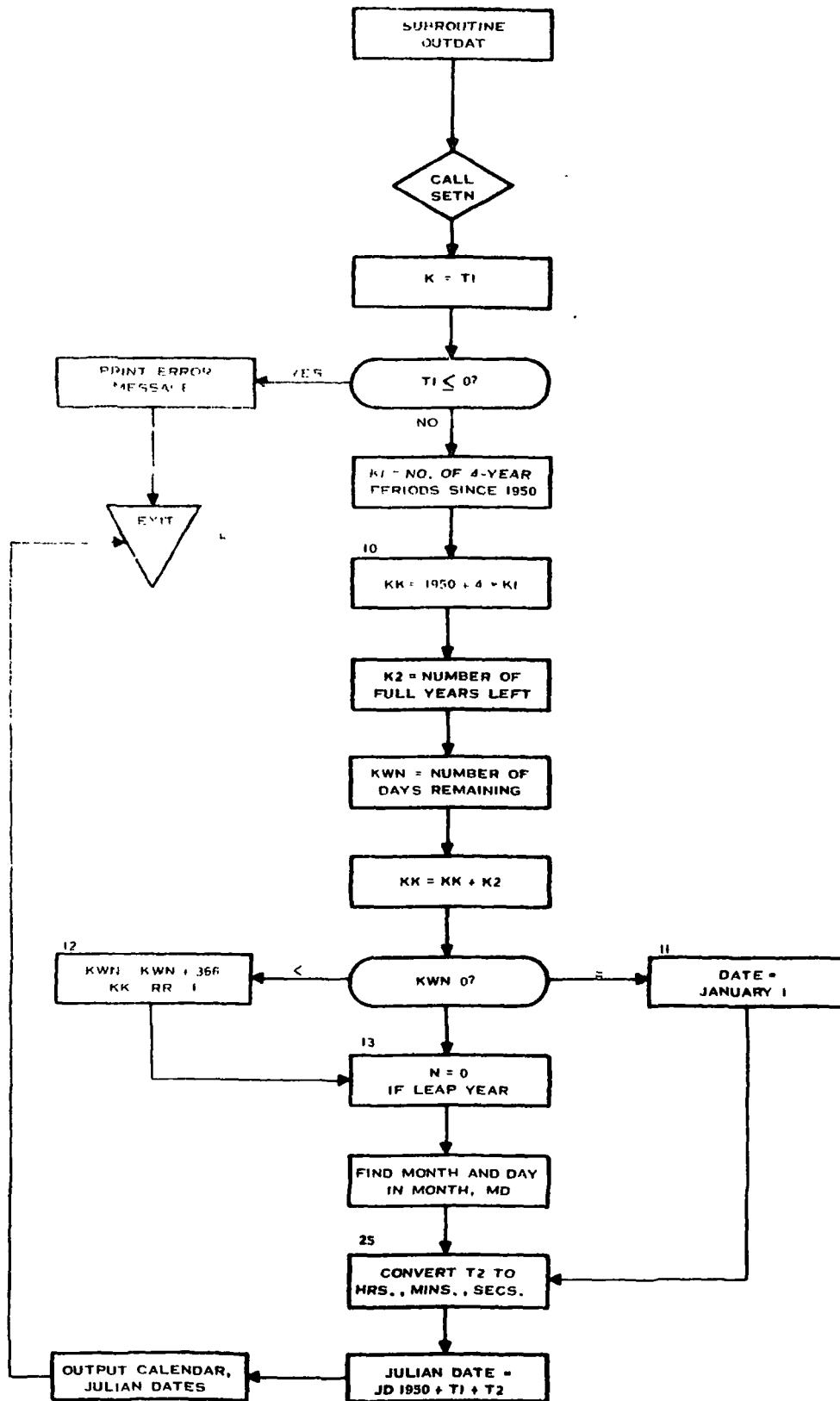
SETN

Functions required:

XMODF, INTF

Approximate number of storages required:

351 DEC



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OUTDAT - 2


```
* LABEL
* SYMBOL TABLE
CEC20DT
SUBROUTINE OUTDAT (T1,T2)
C GIVES CALENDER DATE FROM T1(WHOLE DAYS FROM 1950)
C ANDT2(FRACT OF DAY)
CALL SETN(NIN,NOUT)
MD=0
K=T1
IF(T1)6,6,7
6 WRITE OUTPUT TAPE NOUT,100
8 RETURN
100 FORMAT(23H DATE IS 1950 OR BEFORE)
7 K1=K/1461
10 KK=K1*4+1950
K1=XMODF(K,1461)
K2=K1/365
KWN=XMODF(K1,365)-K2/3
KK=KK+K2
IF(KWN)12,11,13
11 MONTH=1
MD=1
GO TO 25
12 KWN=KWN+366
KK=KK+1
13 N=XMODF(KK,4)
KNW=0
JJ=0
135 JJ=JJ+1
IF(12-JJ)23,23,137
C J,F,M,A,M,J,J,A,S,O,N,MONTHS FOR GO TO
137 GO TO (14,15,14,16,14,16,14,14,16,14,16,14),JJ
14 CONTINUE
KNW=KNW+31
GO TO 17
15 CONTINUE
IF(N)18,18,19
18 KNW=KNW+1
19 KNW=KNW+28
GO TO 17
16 KNW=KNW+30
17 CONTINUE
IF(KWN-KNW)20,21,22
22 CONTINUE
MD=KNW
GO TO 135
20 CONTINUE
MONTH=JJ
MD=KWN-MD+1
GO TO 25
```

OUTD
OUTD
OUTD
OUTD000
OUTD001
OUTD002
OUTD003
OUTD004
OUTD005
OUTD006
OUTD007
OUTD008
OUTD009
OUTD010
OUTD011
OUTD012
OUTD013
OUTD014
OUTD015
OUTD016
OUTD017
OUTD018
OUTD019
OUTD020
OUTD021
OUTD022
OUTD023
OUTD024
OUTD025
OUTD026
OUTD027
OUTD028
OUTD029
OUTD030
OUTD031
OUTD032
OUTD033
OUTD034
OUTD035
OUTD036
OUTD037
OUTD038
OUTD039
OUTD040
OUTD041
OUTD042
OUTD043
OUTD044
OUTD045
OUTD046
OUTD047
OUTD048

OUTDAT (cont'd)

WDL-TR2184

```

21 CONTINUE
   MONTH=JJ+1
   MD=1
   GO TO 25
23 MONTH =12
   MD=KWN-MD+1
25 CONTINUE
   TH=T2*24.
   THP=INTF(TH)
   NHOUR=THP
   THP=(TH-THP)*60.
   TH=INTF(THP)
   NMIN=TH
   THP=(THP-TH)*60.
   NSEC=THP
   TSEC=NSEC
   THP=(THP-TSEC)*1000.
   NFSEC=THP
   TT=INTF(T2+.5)
   TP2=T2+.5-TT
   TP1=T1+TT+2433282.
   WRITE OUTPUT TAPE NOUT,101, KK, MONTH, MD, NHOUR, NMIN, NSEC, NFSEC
   1, TP1, TP2
101 FORMAT(6H YEAR=,I4,8H MONTH=,I2, 6H DAY=,I2, 7H HOUR=,I2,
1 6H MIN=,I2,6H SEC=,I2,1H.,I3,10X,12HJULIAN DATE=,
2F8.0,F8.8)
   GO TO 8
   END

```

OUTD0480
 OUTD0490
 OUTD0500
 OUTD0510
 OUTD0520
 OUTD0530
 OUTD0540
 OUTD0550
 OUTD0560
 OUTD0570
 OUTD0580
 OUTD0590
 OUTD0600
 OUTD0610
 OUTD0620
 OUTD0630
 OUTD0640
 OUTD0650
 OUTD0660
 OUTD0670
 OUTD0680
 OUTD0690
 OUTD0700
 OUTD0710
 OUTD0720
 OUTD0730
 OUTD0740
 OUTD

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OUTDAT - 4

Subroutine: OUTP

Purpose: Obtain the error data in the desired coordinate system for output purposes. The three coordinate systems available are: (1) Equator of Date, (2) Equator of 1950, and (3) Ecliptic. The coordinate system is determined by an input quantity KOUT.

Calling Sequence:

CALL OUTP

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities printed out

Common storages used or required:

T, S, C, IC

Subroutines required:

CROSS, HPHT, INV3, MATRX,
PTRAN

Functions required:

COS, FNORM, SIN, SQRT

Approximate number of storages required:

1179 DEC

A. Derivation of Partial's Used in Subroutine

In order to determine the RMS error in knowledge of orbital elements, the partials which relate the elements and the vehicle state are required. The derivation of these partials follows. The angular elements are shown below in Fig. 1.

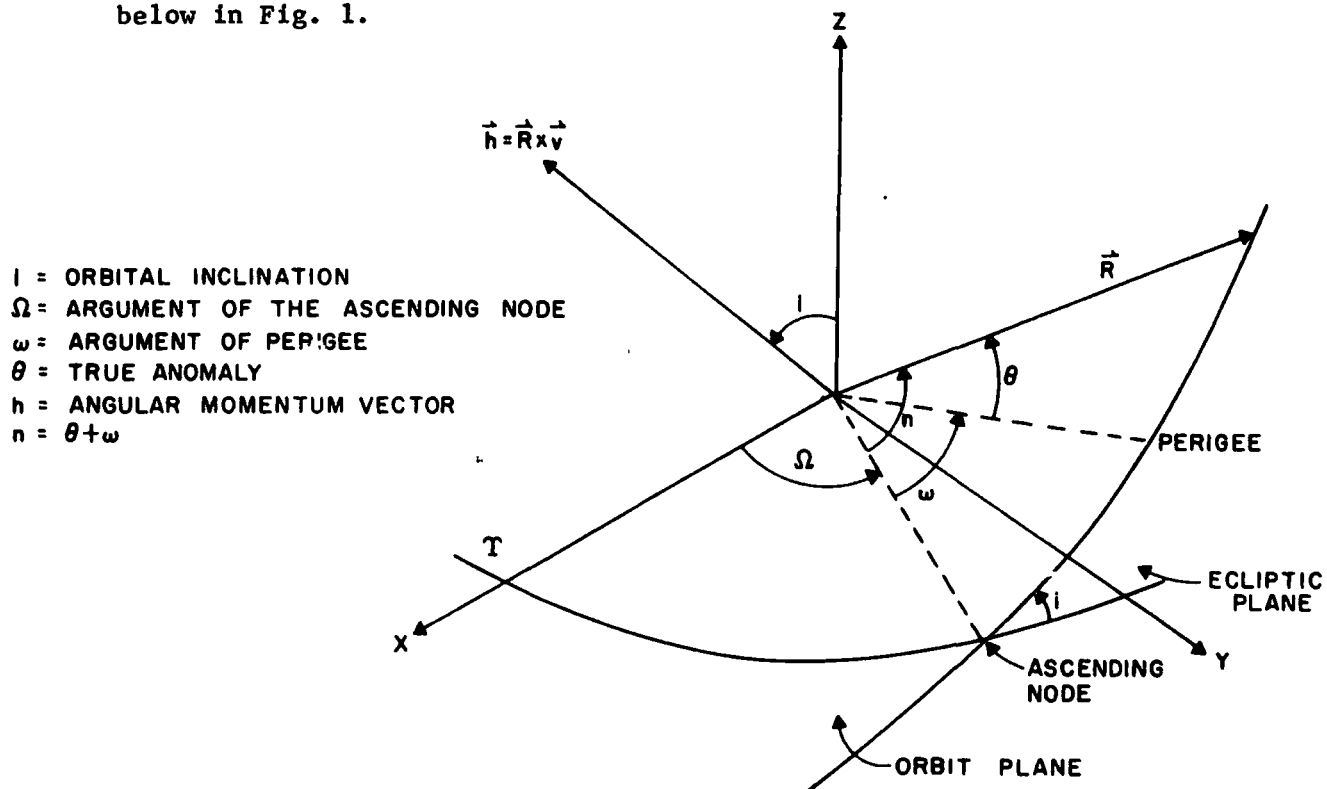


FIG. 1

1. Derivation of partial for eccentricity

$$e = \sqrt{1 + \frac{h^2 C3}{\mu^2}}$$

$$\nabla e = \frac{1}{\mu^2 e} \left\{ C3 [v^2 \vec{r} - (\vec{r} \cdot \vec{v}) \vec{v}] + h^2 \mu \frac{\vec{r}}{r^3} \right\}$$

$$\text{where } \nabla = \left(\frac{\partial}{\partial x} ; \frac{\partial}{\partial y} ; \frac{\partial}{\partial z} \right)$$

$$C3 = v^2 - \frac{2\mu}{r}$$

$$h^2 = |\vec{r} \times \vec{v}|^2$$

$$D\epsilon = \frac{1}{\mu^2 \epsilon} \left\{ h^2 \vec{v} + C3 [r^2 \vec{v} - (\vec{r} \cdot \vec{v}) \vec{r}] \right\}$$

$$\text{where } D = \left(\frac{\partial}{\partial \dot{x}} ; \frac{\partial}{\partial \dot{y}} ; \frac{\partial}{\partial \dot{z}} \right)$$

2. Derivation of partials for radius of closest approach

$$r_p = \frac{h^2}{\mu(1+\epsilon)}$$

$$\nabla r_p = \frac{1}{\mu \epsilon} \left\{ v^2 \vec{r} - (\vec{r} \cdot \vec{v}) \vec{v} - \mu r_p^2 \frac{\vec{r}}{r^3} \right\}$$

$$Dr_p = \frac{1}{\mu \epsilon} \left\{ (r^2 - r_p^2) \vec{v} - (\vec{r} \cdot \vec{v}) \vec{r} \right\}$$

3. Derivation of partials for semi-major axis

$$a = - \frac{\mu}{C3}$$

$$\frac{\partial a}{\partial x_k} = 2a^2 \frac{x_k}{r^3}$$

for $k = 1, 2, 3$

$$x_1 = X \quad x_2 = Y \quad x_3 = Z$$

$$\frac{\partial a}{\partial \dot{x}_k} = 2a^2 \frac{\dot{x}_k}{\mu}$$

$$\dot{x}_1 = \dot{X} \quad \dot{x}_2 = \dot{Y} \quad \dot{x}_3 = \dot{Z}$$

4. Derivation of partials for longitude of the ascending node

$$\Omega = \tan^{-1} \frac{h(1)}{-h(2)}$$

$$\frac{\partial \Omega}{\partial x} = - \sin \Omega \frac{\dot{z}}{h \sin i}$$

$$\frac{\partial \Omega}{\partial \dot{x}} = \sin \Omega \frac{z}{h \sin i}$$

$$\frac{\partial \Omega}{\partial y} = \cos \Omega \frac{z}{h \sin i}$$

$$\frac{\partial \Omega}{\partial \dot{y}} = - \cos \Omega \frac{z}{h \sin i}$$

$$\frac{\partial \Omega}{\partial z} = - \cos i \frac{\dot{z}}{h \sin i} \quad \frac{\partial \Omega}{\partial \dot{z}} = \cos i \frac{z}{h \sin i}$$

5. Derivation of partials for inclination

$$i = \tan^{-1} \frac{\sqrt{h(1)^2 + h(2)^2}}{h(3)}$$

$$\frac{\partial i}{\partial X_k} = \frac{\sin i \cos n}{\sin n} \frac{\partial \Omega}{\partial X_k} \quad \text{for } k = 1, 2, \dots, 6$$

$$X_1 = X \quad X_2 = Y \quad X_3 = Z$$

$$X_4 = \dot{X} \quad X_5 = \dot{Y} \quad X_6 = \dot{Z}$$

6. Derivation of partials for argument of periapsis

$$\omega = n - \theta = \tan^{-1} \frac{zh}{yh(1) - xh(2)} - \tan^{-1} \frac{(\hat{r} \cdot \hat{v}) h}{h^2 - \mu r}$$

$$\frac{\partial \omega}{\partial X_k} = - \frac{1}{e^2} (\alpha \cos n + \beta \sin n) \frac{\partial n}{\partial X_k} + \frac{1}{he^2} \left\{ (\alpha \sin n - \beta \cos n) \right\}$$

$$\left\{ \frac{\partial h}{\partial X_k} - (\alpha + \cos n) \frac{\cos i}{\sin n} h \frac{\partial \Omega}{\partial X_k} \right\}$$

for $k = 1, 2, 3$

$$\begin{aligned} \frac{\partial \omega}{\partial \dot{X}} = & - \frac{1}{e^2} (\alpha \cos n + \beta \sin n) \frac{\partial n}{\partial \dot{X}} + \frac{1}{he^2} (\alpha \sin n - \beta \cos n) \left\{ \frac{\partial h}{\partial \dot{X}} \right. \\ & \left. - (\alpha + \cos n) \frac{\cos i}{\sin n} h \frac{\partial \Omega}{\partial \dot{X}} \right\} - \frac{h}{e^2 \mu} \alpha \cos \Omega \end{aligned}$$

$$\frac{\partial n}{\partial y} = -\frac{1}{\epsilon^2} (\alpha \cos n + \beta \sin n) \frac{\partial n}{\partial y} + \frac{1}{h\epsilon^2} (\alpha \sin n - \beta \cos n) \left\{ \frac{\partial h}{\partial y} \right. \\ \left. - (\alpha + \cos n) \frac{\cos i}{\sin n} h \frac{\partial \Omega}{\partial y} \right\} - \frac{1}{\mu\epsilon^2} \alpha \sin \Omega$$

$$\frac{\partial n}{\partial z} = -\frac{1}{\epsilon^2} (\alpha \cos n + \beta \sin n) \frac{\partial n}{\partial z} + \frac{1}{h\epsilon^2} (\alpha \sin n - \beta \cos n) \left\{ \frac{\partial h}{\partial z} \right. \\ \left. - (\alpha + \cos n) \frac{\cos i}{\sin n} h \frac{\partial \Omega}{\partial z} \right\} - \frac{h}{\mu\epsilon^2} \frac{\beta}{\sin i}$$

where

$$\alpha = \epsilon \cos \omega$$

$$\beta = \epsilon \sin \omega$$

$$\frac{\partial h}{\partial x_k} = \frac{h \sin^2 i \cos n}{\cos i \sin n} \frac{\partial \Omega}{\partial x_k} \quad k = 1, 2, \dots, 6$$

$$\frac{\partial n}{\partial x} = -\cos i \frac{\partial \Omega}{\partial x} - \frac{1}{r} \sin n \cos \Omega$$

$$\frac{\partial n}{\partial x} = -\cos i \frac{\partial \Omega}{\partial x}$$

$$\frac{\partial n}{\partial y} = -\cos i \frac{\partial \Omega}{\partial y} - \frac{1}{r} \sin n \sin \Omega$$

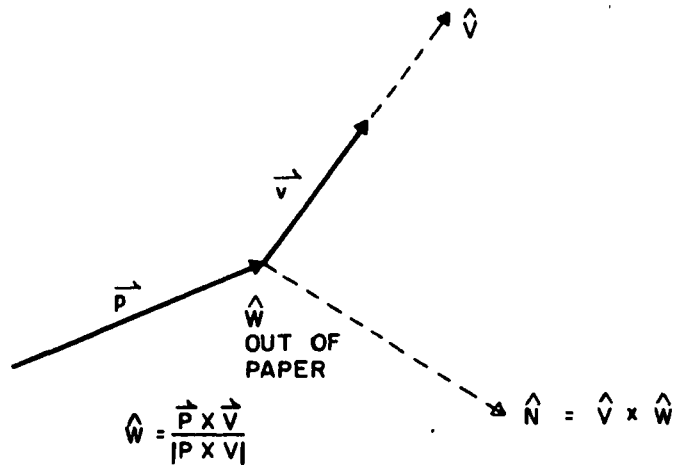
$$\frac{\partial n}{\partial y} = -\cos i \frac{\partial \Omega}{\partial y}$$

$$\frac{\partial n}{\partial z} = -\cos i \frac{\partial \Omega}{\partial z} + \frac{1}{r} \frac{\cos n}{\sin i}$$

$$\frac{\partial n}{\partial z} = -\cos i \frac{\partial \Omega}{\partial z}$$

B. Derivation of Transformation from Cartesian x, y, z to Cartesian N, V, W coordinates

The coordinates N, V, and W represent unit vectors shown in Fig. 2 following.



(PAPER IS ORBIT PLANE)

\vec{p} AND \vec{v} ARE POSITION AND
VELOCITY VECTORS

FIG. 2

\hat{w} is in the direction of the angular momentum vector, \hat{v} is along the velocity vector, and \hat{N} forms an orthogonal coordinate system in the sense of $\hat{N} = \hat{v} \times \hat{w}$. The three unit vectors may be written as follows:

$$\hat{w} = \frac{\vec{R} \times \vec{v}}{|\vec{R} \times \vec{v}|}$$

$$\hat{v} = \frac{\vec{v}}{|\vec{v}|}$$

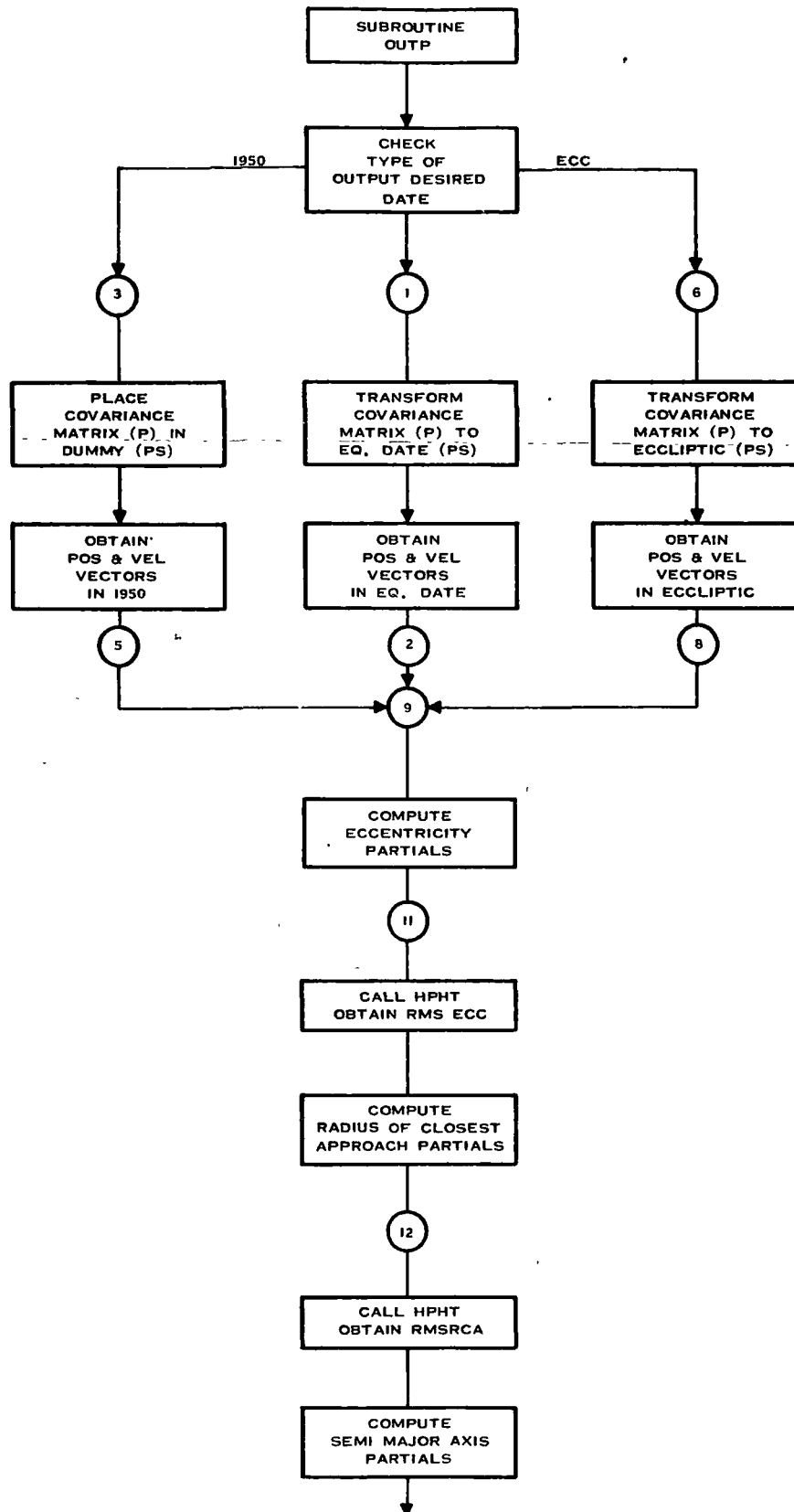
$$\hat{N} = \frac{\vec{v}}{|\vec{v}|} \times \frac{\vec{R} \times \vec{v}}{|\vec{R} \times \vec{v}|}$$

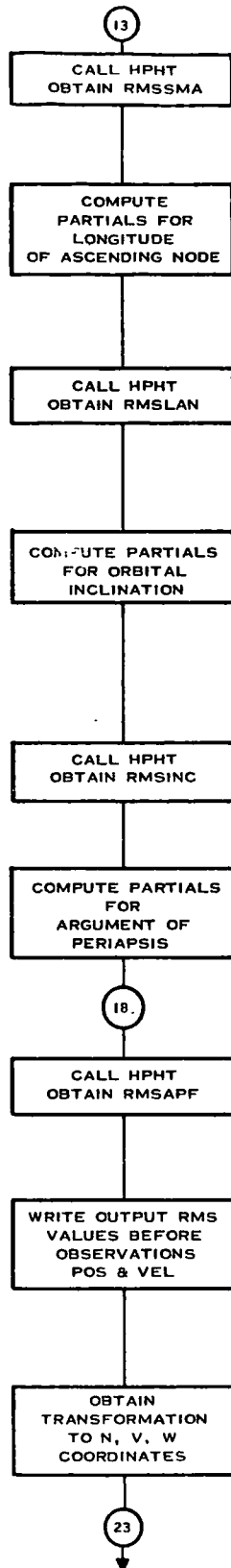
Writing the transposed vectors in matrix form yields the desired transformation from $\hat{i}, \hat{j}, \hat{k}$ to $\hat{N}, \hat{v}, \hat{w}$

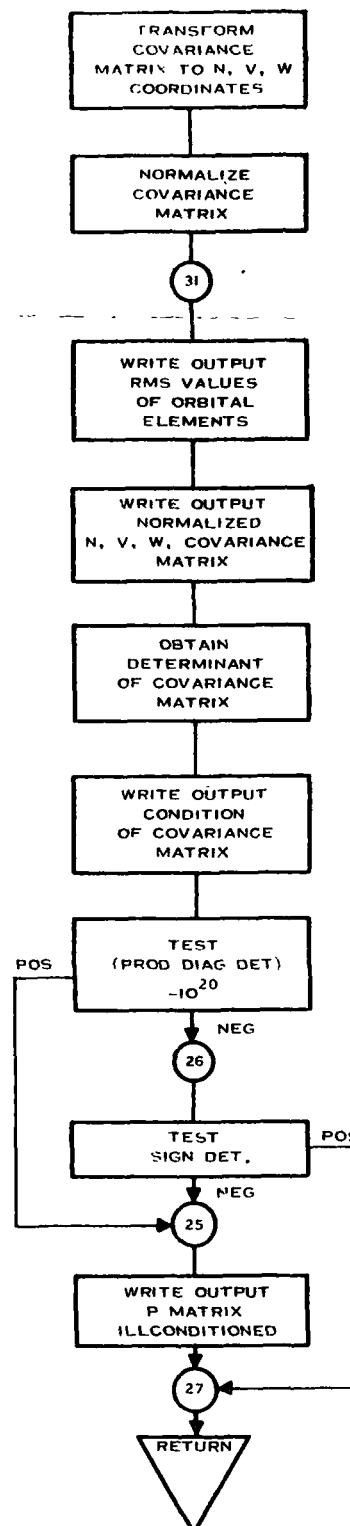
$$\begin{pmatrix} N \\ v \\ w \end{pmatrix}_{3 \times 1} = \begin{pmatrix} \hat{N}^T \\ \hat{v}^T \\ \hat{w}^T \end{pmatrix}_{3 \times 3} \begin{pmatrix} x \\ y \\ z \end{pmatrix}_{3 \times 1}$$

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OUPT - 6







S-333

OUP T - 9

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* LABEL
C C2016 SUBROUTINE OUTP
SUBROUTINE OUTP
COMMON T,S,C,IC
DIMENSION T(1360),S(1000),C(1000),IC(1),P(6,6),AN(3,3),ECL(3,3)
1,ECX(3),ECV(3),XED(3),VED(3),XP(3),VXP(3),PS(6,6),X(3),VX(3)
2,DUM(3,3), H (6),DUMC(3,3),DELH2(3),DELC3(3),DELECC(3),DELVH2(3)
3,DELVEC(3),DELRP(3),DELVVP(3),DELSMA(3),DELYSA(3),Q(6)
DIMENSION Q1(6),RCV(3),DAG(6)
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),(IC,ICDUM)
1,(C(652),P ),(C(138),AN),(C(147),ECL),(C(156),ECX),(C(159),ECV)
2,(C(180),SMA),(C(181),ECC),(C(182),RCA),(C(183),OINC),(C(184),OMG)
3,(C(185),APF),(C(186),XED),(C(189),VED),(C(192),RCV),(C(195),RCV2)
4,(C(196),R2),(C(197),V2) ,(C(198),RDV),(C(199),C3),(C(15),XP)
5,(C(18),VXP),(IC(7),KOUT),(C(55) ,U),(C(162),BET),(C(163),THT)
6,(S(73),RTD)
CALL SETN(NIN,NUTS)
C KOUT=TYPE OUTPUT DESIRED 0=EQ OF DATE 1= EQ OF 1950 2=ECCLIPTIC
IF(KOUT-1) 1,3,6
1 CONTINUE
CALL PTRAN(P,AN,PS,2)
DO 2 I=1,3
X(I)=XED(I)
2 VX(I)=VED(I)
GO TO 9
3 CONTINUE
DO 4 I=1,6
DO 4 J=1,6
4 PS(I,J)=P(I,J)
DO 5 I=1,3
X(I)=XP(I)
5 VX(I)=VXP(I)
GO TO 9
6 CONTINUE
DO 7 I=1,3
DO 7 J=1,3
DUM(I,J)=0.
DO 7 K=1,3
7 DUM(I,J)=DUM(I,J) + ECL(I,K)*AN(K,J)
CALL PTRAN( P,DUM,PS,2)
DO 8 I=1,3
X(I)=ECX(I)
8 VX(I)=ECV(I)
9 CONTINUE
R=SQRTF(R2)
CALL CROSS(VX,RCV,DELH2)
CALL CROSS(RCV,X,DELVH2)
DO 10 I=1,3
10 DELC3(I)=(U/R2/R)*X(I)
C FOLLOWING IS COMPUTATION OF ECCENTRICITY PARTIALS
CONST= 1./(ECC*U**2)

```

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OUTP
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OUTP0050
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OUTP0070
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OUTP0230
OUTP0240
OUTP0250
OUTP0260
OUTP0270
OUTP0280
OUTP0290
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OUTP0370
OUTP0380
OUTP0390
OUTP0400
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OUTP0420
OUTP0430
OUTP0440
OUTP0450
OUTP0460
OUTP0470

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DO 11 I=1,3
II=I+3
DELECC(I)=CONST*(C3*DELH2(I)+RCV2*DELVC3(I))
DELVEC(I)=CONST*(C3*DELVH2(I)+RCV2*VX(I))
H(I)=DELECC(I)
H(II)=DELVEC(I)
11 CONTINUE
CALL HPHT(H,PS,RMSECC)
FOLLOWING FOR PARTIALS OF RADIUS CLOSEST APPROACH =RCA
CON=1.+ECC
CONST=U*CON
CONS =RCV2/(CONST*CON)
CON=2./CONST
DO 12 I=1,3
II= I+3
DELRP(I)=CON*DELH2(I)-CONS*DELECC(I)
DELRP(I)=CON*DELVH2(I)-CONS*DELVEC(I)
H(I)=DELRP(I)
H(II)=DELRP(I)
12 CONTINUE
CALL HPHT(H,PS,RMSRCA)
FOLLOWING FOR PARTIALS OF SEMI MAJOR AXIS =SMA
CONST= 1./ ( ECC-1.)
CON= RCA*CONST**2
DO 13 I=1,3
II=I+3
DELSMA(I)=CONST*DELRP(I)-CON*DELECC(I)
DELVSA(I)=CONST*DELRP(I)-CON*DELVEC(I)
H(I)=DELSMA(I)
H(II)=DELVSA(I)
13 CONTINUE
CALL HPHT(H,PS,RMSSMA)
CI=COSF(0INC)
SI=SINF(0INC)
CW=COSF(OMG)
SW=SINF(OMG)
FOLLOWING FOR LINE OF MODES =LAN PARTIALS
CON =SQRTF(RCV2)
CONST=1./ (CON*SI)
CONS =VX(3)*CONST
G(1) =-SW*CONS
G(2) =CW *CONS
G(3) =-CI*CONS/SI
CONS =X(3)*CONST
G(4) =SW*CONS
G(5) =-CW*CONS
G(6) = CI*CONS/SI
CALL HPHT(0,PS,RMSLAN)
THE FOLLOWING FOR INCLINATION
CONS=1./CON
H(1)=CONS*(-VX(2)*SI + VX(3)*CW*CI)

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OUTP048
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 OUTP103

OUTP (cont'd)

WDL-TR

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H(2)=CONS*(VX(1)*SI + VX(3)*SW*CI)
H(3)=-CONS*CI*(VX(1)*CW+VX(2)*SW)
H(4)=CONS*(X(2)*SI-X(3)*CW*CI)
H(5)=-CONS*(X(1)*SI+X(3)*SW*CI)
H(6)= CONS*CI*(X(1)*CW + X(2)*SW)
CALL HPHT(H,PS,RMSINC)
C THE FOLLOWING ARE PARTIALS OF ARG. OF PERIAPSIS = APF
  SN =SINF(BET)
  CN = COSF(BET)
  DO 17 I=1,6
    Q1(I) = -CI*Q(I)
17 CONTINUE
  G1(1) = Q1(1)-SN*CW/R
  G1(2) = Q1(2)-SN*SW/R
  G1(3) = Q1(3)+CN/(R*SI)
  CP = COSF(APF)
  SP = SINF(APF)
  RAGHI = 1./SQRTF(RCV2)
  CON = ECC*CP
  CONST = ECC*SP
  CONS = -(CON*CN+CONST*SN)/(ECC**2)
  CONS1 = (CON*SN-CONST*CN)*RAGHI/(ECC**2)
  CONS2 = CON*CN
  CONS2 = CONS2*RAGHI*CI/SN
  DO 18 I=1,3
    II = I+3
    H(I) = CONS*Q1(I)+CONS1*(RAGHI*DELH2(I)-CONS2*Q(I))
    H(II) = CONS*Q1(II)+CONS1*(RAGHI*DELVH2(I)-CONS2*Q(II))
18 CONTINUE
  CONS = -1./((RAGHI*U)*(ECC**2))
  H(4)= H(4)+CONS*CW*CON
  H(5)= H(5)+CONS*SW*CON
  H(6) = H(6)+CONS*CONST/SI
  CALL HPHT(H,PS,RMSAPF)
  WRITE OUTPUT TAPE NUTS,700
700 FORMAT( 44X,31H RMS VALUES BEFORE OBSERVATIONS)
  DO 21 I=1,6
    H(I) =SQRTF(PS(I,I))
    WRITE OUTPUT TAPE NUTS,701,H
701 FORMAT(4H  XE15.8,5H  YE15.8,5H  ZE15.8,5H  DXE15.8,
15H  DYE15.8,5H  DZE15.8)
  R50=FNORM(VXP)
  CALL CROSS(XP,VXP,DUM(1,3))
  R51=FNORM(DUM(1,3))
  DO 22 I=1,3
    DUM(I,2)=VXP(I)/R50
22 DUM(I,3)= DUM(I,3)/R51
  CALL CROSS(DUM(1,2),DUM(1,3),DUM(1,1))
  DO 23 I=1,3
    DO 23 J=1,3
23 DUMC(I,J)=DUM(J,I)

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OUTP1040
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 OUTP1670

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CALL PTRAN(P,DUMC,PS,2)
DO 30 I=1,6
DAG(I)=SQRTF(PS(I,I))
30 CONTINUE
DO 31 I=1,6
DO 32 J=I,6
PS(I,J)=PS(I,J)/DAG(I)/DAG(J)
32 CONTINUE
PS(I,I)=1.
31 CONTINUE
RMSINC = RMSINC*RTD
RMSAPF = RMSAPF*RTD
RMSLAN = RMSLAN*RTD
WRITE OUTPUT TAPE NUTS,702,RMSSMA,RMSECC,RMSINC,RMSLAN,RMSAPF,
1RMSRCA
702 FORMAT(4H SMAE15.8,5H ECCE15.8,5H INCE15.8,5H LANE15.8,
15H APFE15.8,5H RCAE15.8)
WRITE OUTPUT TAPE NUTS,703,DAG
703 FORMAT(50X,22H RMS N,V,W COORDINATES,/21X,17H RMS POSITION, KM,
142X,20H RMS VELOCITY KM/SEC,/7X,7H NORMAL, 12X,9H VELOCITY,11X,
29H MOMENTUM,12X,7H NORVEL,14X,7H VELVEL,11X,9H MOMENVEL,/4H
3.8,(5E20.8))
WRITE OUTPUT TAPE NUTS,704,((PS(I,J),J=1,6),I=1,6)
704 FORMAT(30X,58H NORMALIZED STATE COVARIANCE MATRIX IN N,V,W COORD
1INATES,/4H E15.8,(5E20.8)/19X,(5E20.8)/39X,(4E20.8)/59X,
2(3E20.8)/79X,(2E20.8)/99X,E20.8)
CON = 1.
CALL INV3(PS,6,DETER)
CONST = CON/DETER
WRITE OUTPUT TAPE NUTS,705,DETER,CON,CONST
705 FORMAT(37H CONDITION OF STATE COVARIANCE MATRIX,/
124H DETERMINANT OF MATRIX =,E15.8,3X,
222H PRODUCT OF DIAGONAL =,E15.8,1X,
324H RATIO PROD.DIAG./DET. =,E15.8)
IF (ABSF(CONST)-1.E20) 26,25,25
26 IF (DETER) 25,25,27
WRITE OUTPUT TAPE NUTS,706
706 FORMAT(33H ***P MATRIX IS ILLCONDITIONED***)
27 CONTINUE
RETURN
END

```

OUTP168
 OUTP169
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Subroutine: PTRAN

Purpose: To compute the transformation of the state covariance matrix from one inertial coordinate system to another. The transformation which is obtained with $KK = 2$ is the following:

$$PS = \begin{pmatrix} B & 0 \\ 0 & B \end{pmatrix} \begin{pmatrix} P \end{pmatrix} \begin{pmatrix} B^T & 0 \\ 0 & B^T \end{pmatrix}$$

6x6 6x6 6x6 6x6

If KK is set 1 only, the diagonal 3x3's are computed.

Calling Sequence:

CALL PTRAN (P, B, PS, KK)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	P	(6,6)			Covariance Matrix
I	B	(3,3)			Transformation Matrix
O	PS	(6,6)			Transformed Matrix
I	KK	1			Logic Key

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

PTRAN

WDL-TR

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* LABEL
* SYMBOL TABLE
SUBROUTINE PTRAN( P,B,PS,KK)
DIMENSION P(6,6),B(3,3),PS(6,6),DUM(6,6)
C SUBROUTINE CALCULATES THE 6X6 MATRIX PS FROM
C P IS SYMMETRIC PS=( B 0 )( P )( BT 0 ) T=TRANPOSE
C ( 0 B )( ) ( 0 BT) K=1 OBTAINS ONLY DIAG 3X3
DO 1 I=1,6
DO 1 J=1,6
PS(I,J)=0.
1 DUM(I,J)=0.
DO 2 I=1,3
I3=I+3
DO 2 J=1,3
J3=J+3
DO 2 K=1,3
K3 = K+3
DUM(I,J)=DUM(I,J)+ B(I,K)*P(K,J)
DUM(I3,J3)=DUM(I3,J3)+ B(I,K)*P(K3,J3)
GO TO(2,3), KK
3 DUM(I,J3) =DUM(I,J3) + B(I,K)*P(K,J3)
2 CONTINUE
DO 5 I=1,3
I3=I+3
DO 5 J=1,3
J3=J+3
DO 4 K=1,3
K3=K+3
PS(I,J)=PS(I,J) + DUM(I,K)*B(J,K)
PS(I3,J3)=PS(I3,J3) +DUM(I3,K3)*B(J,K)
GO TO(4,6), KK
6 PS(I,J3) =PS(I,J3) +DUM(I ,K3)*B(J,K)
4 CONTINUE
GO TO(5,7),KK
7 PS(J3,I)=PS(I,J3)
5 CONTINUE
8 CONTINUE
RETURN
END

```

PTRN
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PTRN000
PTRN0010
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PTRN003
PTRN0035
PTRN0040
PTRN005
PTRN006
PTRN0070
PTRN008
PTRN009
PTRN0100
PTRN011
PTRN012
PTRN013
PTRN0140
PTRN015
PTRN016
PTRN0170
PTRN018
PTRN019
PTRN0200
PTRN0210
PTRN022
PTRN023
PTRN0240
PTRN025
PTRN026
PTRN0270
PTRN028
PTRN029
PTRN0300
PTRN0310
PTRN032
PTRN033
PTRN0340
PTRN

Subroutine: RETRO

Purpose: To take the P and PAR covariance matrices through a retro maneuver into a circular orbit.

Calling Sequence:

CALL RETRO

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities returned to common

Common storages used or required:

T, S, C, IC

Subroutines required:

MATRX, SETN

Functions required:

DOT, FNORM, SQRT

Approximate number of storages required:

779 DEC

Derivation of Guidance Law Through Retro Maneuver

The vehicle is assumed to be at periapsis at the time the subroutine is called. The maneuver is then carried out such that the vehicle is in circular orbit after retro fire.

The required velocity at periapsis for a circular orbit is:

$$v_p = \sqrt{\frac{\mu}{R_p}}$$

The required incremental velocity correction along the nominal trajectory is the following

$$\Delta \vec{v} = \left(\frac{v_p}{v_n} - 1 \right) \vec{v}_n \quad v_n = |\vec{v}_n| \quad (1)$$

where v_n is the nominal periapsis velocity vector for the incoming trajectory.

The guidance law which governs the deviations from the nominal is obtained in the following manner. The deviation from nominal periapsis velocity (assuming linear theory) may be written as:

$$\delta \vec{v}_p = \dot{\vec{x}} + A \vec{x} \quad (2)$$

$$3 \times 1 \quad 3 \times 1 (3 \times 3) (3 \times 1)$$

where

$$A = \begin{pmatrix} \frac{\partial v_p}{\partial x_1} & 0 & 0 \\ 0 & \frac{\partial v_p}{\partial x_2} & 0 \\ 0 & 0 & \frac{\partial v_p}{\partial x_3} \end{pmatrix}$$

and $\underline{\hat{x}}$ and $\dot{\underline{\hat{x}}}$ are the vehicle deviation state.

The partial derivatives in matrix A are the following:

$$\frac{\partial u_p}{\partial x_i} = - \frac{\mu x_i}{2u_p R^3} \quad i = 1, 2, 3$$

The estimate of periapsis velocity deviation from equation (2) is

$$\delta \underline{\hat{u}}_p = \underline{\hat{x}} + A \underline{\hat{x}} \quad (3)$$

and the guidance law is obtained as follows:

$$\delta \underline{\hat{u}}_p + \dot{\underline{\hat{x}}}_{g_t} = 0 = \underline{\hat{x}} + A \underline{\hat{x}} + \dot{\underline{\hat{x}}}_g$$

or

$$\dot{\underline{\hat{x}}}_g = - (A \ I) \begin{pmatrix} \underline{\hat{x}} \\ \dot{\underline{\hat{x}}} \end{pmatrix} \quad (4)$$

3x1 3x6 6x1

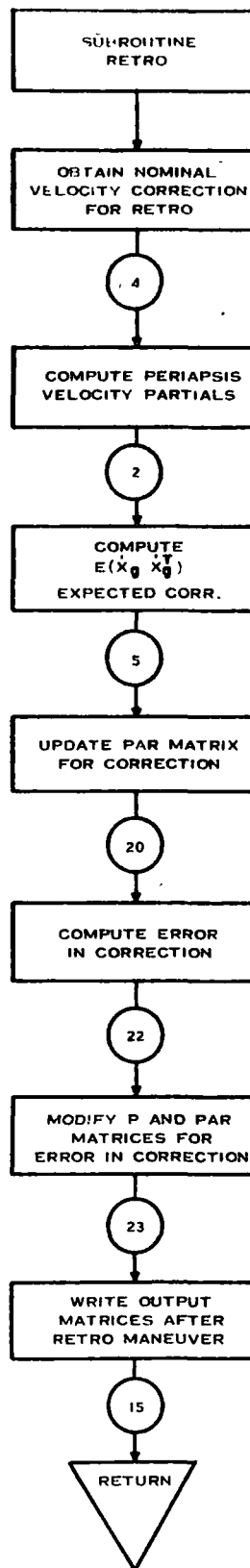
The total guidance correction is the sum of equations (1) and (4).

$$\dot{\underline{\hat{x}}}_{gt} = - (A \ I) \begin{pmatrix} \underline{\hat{x}} \\ \dot{\underline{\hat{x}}} \end{pmatrix} + \Delta \vec{V} \quad (5)$$

The guidance law expressed by equation (4) corresponds to equation (6) in the guidance correction derivation in subroutine GUID. The P and PAR covariance matrices are then updated as shown by the derivation in the GUID subroutine writeup. The additional term, $\Delta \vec{V}$, present in the total guidance correction required is treated as being independent of the deviation state. Therefore, the $E(\dot{\underline{\hat{x}}}_{gt} \dot{\underline{\hat{x}}}_{gt}^T)$ may be written as:

$$E(\dot{\underline{\hat{x}}}_{gt} \dot{\underline{\hat{x}}}_{gt}^T) = E(\dot{\underline{\hat{x}}}_g \dot{\underline{\hat{x}}}_g^T) + \Delta \vec{V} \Delta \vec{V}^T$$

since $E(\dot{\underline{\hat{x}}}_g \Delta \vec{V}^T) = 0$



S-344

RETRO - 4

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* LABEL
* SYMBOL TABLE
CEC2030 SUBROUTINE RETRO
SUBROUTINE RETRO
COMMON T,S,C,IC
DIMENSION T(1360),S(1000),C(1000),IC(1)
1,TPAR(3,6),PAR(6,6),P(6,6),DUP(3,3)
2,TGUID(6),DUM(3,3),DUN(3,3),DUMM(6,6)
DIMENSION XP(3),VXP(3),CV(3)
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM)
1,(IC,ICDUM),(C(568),TPAR),(C(460),PAR)
2,(C(652),P),(IC(218),N),(C(648),TGUIDE)
3,(IC(219),IGD),(IC(217),IGDTP),(IC(214),NOUT)
4,(C(30),TSEC),(S(476),TGUID),(S(483),RATIO)
5,(S(473),QQPT),(S(471),QQSO),(S(484),DMONIT)
EQUIVALENCE (C(15),XP),(C(18),VXP),(C(55),U)
CALL SETN(NIN,NUTS)
WRITE OUTPUT TAPE NUTS,701
701 FORMAT(94H THE DOLLOING DATA ARE CONDITIONS AFTER RETRO INTO CIRC
1ULAR ORBIT ASSUMING VEHICLE AT PERIGEE)
R2=DOT(XP,XP)
R=FNORM(XP)
VM=FNORM(VXP)
VP=SQRTF(U/R)
DELV=VP/VM
DO 1 I=1,3
1 CV(I)=DELV*VXP(I)
WRITE OUTPUT TAPE NUTS,700,CV
700 FORMAT(35H CIRCULAR VELOCITY COMPONENTS X,Y,Z/(3E17,8))
DO 4 I=1,3
4 CV(I)=(CV(I)-VXP(I))**2
CONS=-U/(2.*VP*R2*R)
DO 2 I=1,3
II=I+3
DO 3 J=1,3
JJ=J+3
TPAR(I,J)=0.
3 TPAR(I,JJ)=0.
TPAR(I,I)=CONS*XP(I)
2 TPAR(I,II)=-1.
CALL MATRX(TPAR,P,DUM,3,6,6,1)
CALL MATRX(TPAR,PAR,DUN,3,6,6,1)
DO 5 I=1,3
DO 6 J=1,3
6 DUM(I,J)=DUN(I,J)-DUM(I,J)
5 DUM(I,I)=DUM(I,I)+CV(I)
RMSV2=DUM(1,1)+DUM(2,2)+DUM(3,3)
RMSV=SQRTF(RMSV2)
C FOLLOWING IS UPDATING OF PAR MATRIX FOR GUIDANCE CORRECTION
DO 17 I=1,6
DO 17 J=I,6

```

RETR
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RETR029
RETR030
RETR031
RETR032
RETR033
RETR034
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RETR036
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RETR038
RETR039
RETR040
RETR041
RETR042
RETR043
RETR044
RETR045
RETR046
RETR047

RETRO (cont'd)

WDL-TR2

```

      PAR(I,J)=PAR(I,J)-P(I,J)
      PAR(J,I)=PAR(I,J)
17  CONTINUE
      DO 19 I=1,3
      II=I+3
      DO 18 J=1,3
      JJ=J+3
      DUMM(II,J)=TPAR(I,J)
      DUMM(I,JJ)=0.
      DUMM(II,JJ)=0.
18  DUMM(I,J)=0.
19  DUMM(I,I)=1.
      CALL MATRX(DUMM,PAR,PAR,6,6,6,1)
      DO 20 I=1,6
      DO 20 J=I,6
      PAR(I,J)=PAR(I,J)+P(I,J)
      PAR(J,I)=PAR(I,J)
20  CONTINUE
      CRUD=QQPT*RMSV2
      QQ=QQSO-QQPT
      DO 22 I=1,3
      DO 21 J=I,3
      DUN(I,J)=QQ*DUM(I,J)
      DUN(J,I)=DUN(I,J)
21  CONTINUE
      DUN(I,I)=DUN(I,I)+CRUD
22  CONTINUE
      RMSERR=SQRTF(DUN(1,1)+DUN(2,2)+DUN(3,3))
      DO 23 I=1,3
      II=I+3
      DO 23 J=I,3
      JJ=J+3
      PAR(II,JJ)=PAR(II,JJ)+DUN(I,J)
      PAR(JJ,II)=PAR(II,JJ)
      P(II,JJ)=P(II,JJ)+DMONIT*DUN(I,J)
      P(JJ,II)=P(II,JJ)
23  CONTINUE
      WRITE OUTPUT TAPE NUTS,702,RMSV,RMSERR
702  FORMAT(24H RETRO GUID DATA FOLLOWS/
115H  RMS VEL REQ=,E15.8,10X,18H  RMSERR IN CORR=,E15.8)
      WRITE OUTPUT TAPE NUTS,703,P
703  FORMAT(9H P MATRIX/(6E17.8))
      WRITE OUTPUT TAPE NUTS,704,PAR
704  FORMAT(11H PAR MATRIX/(6E17.8))
15  RETURN
      END

```

RETR048
 RETR049
 RETR050
 RETR051
 RETR052
 RETR053
 RETR054
 RETR055
 RETR056
 RETR057
 RETR058
 RETR059
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 RETR061
 RETR062
 RETR063
 RETR064
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 RETR066
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 RETR069
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 RETR076
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 RETR080
 RETR081
 RETR082
 RETR083
 RETR084
 RETR085
 RETR086
 RETR087
 RETR088
 RETR089
 RETR090
 RETR091
 RETR092
 RETR

Subroutine: ROTATE

Purpose: To compute a 3 x 3 rotation matrix for a transformation of coordinates about axis i ($i = 1, 2, 3$) through an angle $\pm \theta$.

[For example: rotation about axis 1, matrix =
$$\begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{pmatrix}$$

Calling Sequence:

CALL ROTATE (NCOORD, ANG, RMTRIX, IROT)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	NCOORD	1	$i, i = 1, 2, 3$		Axis of rotation
I	ANG	1	θ	radians	Angle for rotation
O	RMTRIX	3,3			Resulting rotation matrix
I	IROT	1			If IROT < 0, use $-\theta$.

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

ROTATE

WDL-TR21

```
* LABEL
* SYMBOL TABLE
SUBROUTINE ROTATE(NCOORD,ANG,RMTRIX,IROT)
DIMENSION RMTRIX(3,3)
SANG = SIN(ANG)
CANG = COS(ANG)
IF (IROT) 1,2,2
1 SANG = -SANG
2 DO 3 I=1,3
  DO 3 J=1,3
3 RMTRIX(I,J) = 0.
  GO TO (4,5,6), NCOORD
4 I = 2
  J = 3
  GO TO 7
5 I = 1
  J = 3
  GO TO 7
6 I = 1
  J = 2
7 RMTRIX(NCOORD,NCOORD) = 1.
  RMTRIX(I,I) = CANG
  RMTRIX(I,J) = SANG
  RMTRIX(J,I) = -SANG
  RMTRIX(J,J) = CANG
RETURN
END
```

```
ROTA
ROTA
ROTA0000
ROTA0010
ROTA0020
ROTA0030
ROTA0040
ROTA0050
ROTA0060
ROTA0070
ROTA0080
ROTA0090
ROTA0100
ROTA0110
ROTA0120
ROTA0130
ROTA0140
ROTA0150
ROTA0160
ROTA0170
ROTA0180
ROTA0190
ROTA0200
ROTA0210
ROTA0220
ROTA0230
ROTA
```

Subroutine: ROTEQ

Purpose: ROTEQ evaluates elements of the rotation matrix which relate the general precession of the earth's equator and the consequent retrograde motion of the equinox on the ecliptic. It is used to provide the transformation from mean equator and equinox of 1950.0 to mean equator and equinox of date.

Calling Sequence:

CALL ROTEQ (TIME, A)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TIME	1	T	days	Total number days from reference epoch (1950.0)
O	A	3,3	A		Rotation matrix

Common storages used or required:

None

Subroutines required:

None

Functions required:

None

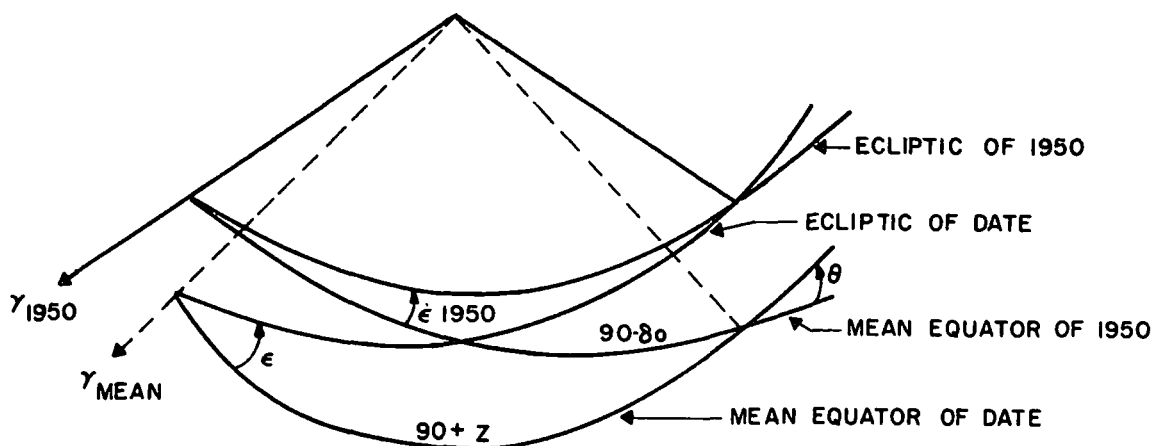
Approximate number of storages required:

Elements of Transformation

The rotation matrix may be represented as

$$\begin{pmatrix} x' \\ y' \\ z' \end{pmatrix} = \begin{pmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{pmatrix} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$$

where X, Y, Z are expressed in the mean equator and equinox of 1950.0 and x', y', z' are the coordinates in the mean equator and equinox of date.



The geometry of the precession has been represented by the three small parameters δ_0 , z , and θ . γ_{1950} is the mean equinox of 1950; ϵ_{1950} is the mean obliquity of 1950; γ_{mean} is the mean equinox of date; ϵ is the mean obliquity of date. Measured in the mean equator of 1950 from the mean equinox of 1950, $90^\circ - \delta_0$ is the right ascension of the ascending node of the mean equator of date on the mean equator of 1950.

$90^\circ + z$ is the right ascension of the node measured in the mean equator of date from the mean equinox of date. θ is the inclination of the mean equator of date to the mean equator of 1950.

In terms of δ_o , z , and θ , (a_{ij}) is given by:

$$a_{11} = -\sin \delta_o \sin z + \cos \delta_o \cos z \cos \theta$$

$$a_{12} = -\cos \delta_o \sin z - \sin \delta_o \cos z \cos \theta$$

$$a_{13} = -\cos z \sin \theta$$

$$a_{21} = \sin \delta_o \cos z + \cos \delta_o \sin z \cos \theta$$

$$a_{22} = \cos \delta_o \cos z - \sin \delta_o \sin z \cos \theta$$

$$a_{23} = -\sin z \sin \theta$$

$$a_{31} = \cos \delta_o \sin \theta$$

$$a_{32} = -\sin \delta_o \sin \theta$$

$$a_{33} = \cos \theta$$

$$\delta_o = 2304''.997T + ''302T^2 + ''0179T^3$$

$$z = 2304''.997T + 1''.093T^2 + ''0192T^3$$

$$\theta = 2004''.298T - ''426T^2 - ''0416T^3$$

with T the number of Julian centuries of 36,525 days past the epoch 1950.0.

The actual computational form of (a_{ij}) is obtained by expanding the a_{ij} in power series in δ_0 , z , θ and replacing the arguments by the above time series. The results are:

$$a_{11} = 1 - .00029697T^2 - .00000013T^3$$

$$a_{12} = -a_{21} = -.02234988T - .00000676T^2 + .00000221T^3$$

$$a_{13} = -a_{31} = -.00971711T + .00000207T^2 + .00000096T^3$$

$$a_{22} = 1 - .00024976T^2 - .00000015T^3$$

$$a_{23} = a_{32} = -.00010859T^2 - .00000003T^3$$

$$a_{33} = 1 - .00004721T^2 + .00000002T^3$$

```

* LABEL
* SYMBOL TABLE
SUBROUTINE ROTEQ(TIME,A)
DIMENSION A(3,3)
T = TIME/36525.
T2 = T*T
T3 = T2*T
A(1,1) = 1. - .00029697*T2 - .00000013*T3
A(1,2) = -.02234988*T - .00000676*T2 + .00000221*T3
A(2,1) = -A(1,2)
A(1,3) = -.00971711*T + .00000207*T2 + .00000096*T3
A(3,1) = -A(1,3)
A(2,2) = 1. - .00024976*T2 - .00000015*T3
A(2,3) = -.00010859*T2 - .00000003*T3
A(3,2) = A(2,3)
A(3,3) = 1. - .00004721*T2 + .00000002*T3
RETURN
END

```

```

ROTO
ROTO
ROTO000
ROTO001
ROTO002
ROTO003
ROTO004
ROTO005
ROTO006
ROTO007
ROTO008
ROTO009
ROTO010
ROTO011
ROTO012
ROTO013
ROTO014
ROTO

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Subroutine: RVIN

Purpose: To transform inertial equatorial spherical to Cartesian coordinates.

Calling Sequence:

CALL RVIN (A, B, C)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	A	5	$A(1) = R$		Magnitude of Position Vector
			$A(2) = \phi$	deg	Declination
			$A(3) = \theta$	deg	Right Ascension
			$A(4) = V$		Magnitude of Velocity Vector
			$A(5) = \Gamma$	deg	Flight Path Angle
			$A(6) = \Sigma$	deg	Azimuth
O	B	3			X, Y, Z
O	C	3			\dot{X} , \dot{Y} , \dot{Z}

Common storages used or required:

None

Subroutines required:

None

Functions required:

SIN, COS

Approximate number of storages required:

RVIN

The calling sequence consists of

CALL RVIN (XIN, XOUT, VOUT)

where: XIN is a vector with dimension six. The vector contains the spherical set in the following order

$$\text{XIN} = \begin{bmatrix} |R| \\ 0 \\ \theta \\ |V| \\ \gamma \\ \sigma \end{bmatrix} \quad \begin{array}{ll} |R| & = \text{Magnitude position vector} \\ 0 & = \text{Declination} \\ \theta & = \text{Right ascension} \\ |V| & = \text{Magnitude velocity vector} \\ \gamma & = \text{Flight path angle} \\ \sigma & = \text{Azimuth} \end{array}$$

6x1

XOUT is a vector with dimension three. The vector contains the Cartesian components of position

$$\text{XOUT} = \begin{bmatrix} x \\ y \\ z \end{bmatrix}$$

3x1

VOUT is a vector with dimension three. The vector contains the Cartesian components of velocity

$$\text{VOUT} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix}$$

3x1

RVIN TRANSFORMATIONS

The position transformation is obtained as follows (see Fig. 1 below).

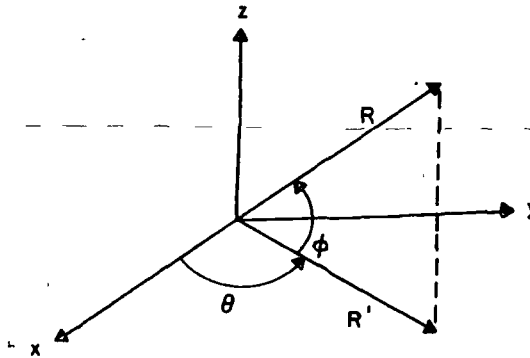


FIG 1

Projecting \vec{R} on the x-y plane, θ is the angle from the x axis to the projection measured counterclockwise. The elevation of \vec{R} above the x-y plane is the angle ϕ . The formulas are

$$\begin{matrix} \text{XOUT} = & \begin{pmatrix} x \\ y \\ z \end{pmatrix} & = & |R| & \begin{pmatrix} \cos \phi \cos \theta \\ \cos \phi \sin \theta \\ \sin \phi \end{pmatrix} & (1) \\ & 3 \times 1 & & & 3 \times 1 \end{matrix}$$

The velocity transformation is obtained as follows. The azimuth and flight path angles refer to the tangent plane which is normal to the \vec{R} vector (see Fig. 2).

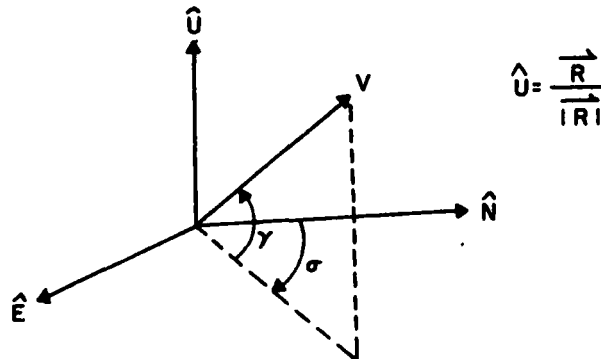


FIG. 2

The unit up, \hat{U} , east \hat{E} , and north, \hat{N} , vectors in terms of xyz are

$$\begin{matrix} \hat{U} & = & \frac{\vec{R}}{|\vec{R}|} & = & \begin{pmatrix} \cos \phi \cos \theta \\ \cos \phi \sin \theta \\ \sin \phi \end{pmatrix} & (2) \\ 3 \times 1 & & 3 \times 1 & & 3 \times 1 & \end{matrix}$$

$$\begin{matrix} \hat{E} & = & \frac{\hat{k} \times \hat{U}}{|\hat{k} \times \hat{U}|} & = & \begin{pmatrix} -\sin \theta \\ \cos \theta \\ \phi \end{pmatrix} & (3) \\ 3 \times 1 & & 3 \times 1 & & 3 \times 1 & \end{matrix}$$

$$\begin{matrix} \hat{N} & = & \hat{U} \times \hat{E} & = & \begin{pmatrix} -\sin \phi \cos \theta \\ -\sin \phi \sin \theta \\ \cos \phi \end{pmatrix} & (4) \\ 3 \times 1 & & 3 \times 1 & & 3 \times 1 & \end{matrix}$$

The above vectors may be written in matrix form to represent the transformation from the local tangent plane to the xyz coordinate system

$$\begin{matrix} \begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{pmatrix} \\ 3 \times 1 \end{matrix} = \begin{matrix} \begin{pmatrix} \hat{U} & \hat{E} & \hat{N} \end{pmatrix} \\ 3 \times 3 \end{matrix} \begin{matrix} \begin{pmatrix} \dot{U} \\ \dot{E} \\ \dot{N} \end{pmatrix} \\ 3 \times 1 \end{matrix} = \begin{matrix} \begin{pmatrix} \cos \phi \cos \theta \sin \theta & -\sin \phi \cos \theta \\ \cos \phi \sin \theta \cos \theta & -\sin \phi \sin \theta \\ \sin \phi & 0 & \cos \phi \end{pmatrix} \\ 3 \times 3 \end{matrix} \begin{matrix} \begin{pmatrix} \dot{U} \\ \dot{E} \\ \dot{N} \end{pmatrix} \\ 3 \times 1 \end{matrix} \quad (5)$$

The velocity vector in the tangent plane coordinates (Fig. 2) is

$$\begin{matrix} \vec{V} \\ 3 \times 1 \end{matrix} = \begin{matrix} \begin{pmatrix} \dot{U} \\ \dot{E} \\ \dot{N} \end{pmatrix} \\ 3 \times 1 \end{matrix} = |V| \begin{matrix} \begin{pmatrix} \sin \gamma \\ \cos \gamma \sin \sigma \\ \cos \gamma \cos \sigma \end{pmatrix} \\ 3 \times 1 \end{matrix} \quad (6)$$

Substituting equation (6) into (5) yields the desired transformation

$$\begin{matrix} V_{OUT} \\ 3 \times 1 \end{matrix} = \begin{matrix} \begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{pmatrix} \\ 3 \times 1 \end{matrix} = |V| \begin{matrix} \begin{pmatrix} \hat{U} & \hat{E} & \hat{N} \end{pmatrix} \\ 3 \times 3 \end{matrix} \begin{matrix} \begin{pmatrix} \sin \gamma \\ \cos \gamma \sin \sigma \\ \cos \gamma \cos \sigma \end{pmatrix} \\ 3 \times 1 \end{matrix}$$

RVIN

WDL-TR2184

```

* LABEL
* SYMBOL TABLE
SUBROUTINE RVIN(A,B,C)
DIMENSION A(6),B(3),C(3),D(3,3),E(3)
A(2) = A(2)*.017453293
A(3) = A(3)*.017453293
A(5) = A(5)*.017453293
A(6) = A(6)*.017453293
CP = COSF(A(2))
SP = SIN F(A(2))
CT = COSF(A(3))
ST = SIN F(A(3))
CG = COSF(A(5))
SG = SIN F(A(5))
CS = COSF(A(6))
SS = SIN F(A(6))
SPCT = SP*CT
SPST = SP*ST
CGSS = CG*SS
CGCS = CG*CS
CPCT = CP*CT
CPST = CP*ST
D(1,1) = CPCT
D(1,2) = -ST
D(1,3) = -SPCT
D(2,1) = CPST
D(2,2) = CT
D(2,3) = -SPST
D(3,1) = SP
D(3,2) = 0.
D(3,3) = CP
B(1) = A(1)*CPCT
B(2) = A(1)*CPST
B(3) = A(1)*SP
E(1) = A(4)*SG
E(2) = A(4)*CGSS
E(3) = A(4)*CGCS
DO 1 I=1,3
C(I) = 0.
DO 1 J=1,3
1 C(I) = C(I) + D(I,J)*E(J)
RETURN
END

```

```

RVIN
RVIN
RVIN0000
RVIN0010
RVIN0020
RVIN0030
RVIN0040
RVIN0050
RVIN0060
RVIN0070
RVIN0080
RVIN0090
RVIN0100
RVIN0110
RVIN0120
RVIN0130
RVIN0140
RVIN0150
RVIN0160
RVIN0170
RVIN0180
RVIN0190
RVIN0200
RVIN0210
RVIN0220
RVIN0230
RVIN0240
RVIN0250
RVIN0260
RVIN0270
RVIN0280
RVIN0290
RVIN0300
RVIN0310
RVIN0320
RVIN0330
RVIN0340
RVIN0350
RVIN0360
RVIN0370
RVIN0380
RVIN0390
RVIN

```

Subroutine: RVOUT

Purpose: To convert Cartesian position and velocity coordinates to inertial equatorial spherical coordinates.

Calling Sequence: -----

CALL RVOUT (A, B, C)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	A	3	X, Y, Z		Position coordinates
I	B	3	$\dot{X}, \dot{Y}, \dot{Z}$		Velocity coordinates
O	C	6	C(1) = R		Magnitude of position vector
			C(2) = ϕ	degrees	Declination
			C(3) = α	degrees	Right ascension
			C(4) = V		Magnitude of velocity vector
			C(5) = Γ	degrees	Flight path angle
			C(6) = Σ	degrees	Azimuth

Common storages used or required:

None

Subroutines required:

CORSS

Functions required:

ATANF, SORTF, ARKTNS, DOT,
ACOS, FNORM

Approximate number of storages required:

RVOUT

The transformations required to convert Cartesian coordinates to inertial equatorial spherical are the inverse of those required by, and described under, RVIN.

For the position coordinates:

$$R = \sqrt{X^2 + Y^2 + Z^2}$$

$$\Phi = \sin^{-1} \frac{Z}{R} \quad -90^\circ \leq \Phi \leq 90^\circ$$

$$\Theta = \tan^{-1} \frac{Y}{X} \quad \left. \begin{array}{l} + 0 \text{ for } X > 0 \\ + 180^\circ \text{ for } X \leq 0 \end{array} \right\}$$

For the velocity coordinates, \dot{X}' , \dot{Y}' , \dot{Z}' are obtained by applying the inverse of the transformation matrix $\begin{bmatrix} \hat{U} & \hat{E} & \hat{N} \\ 3 \times 3 \end{bmatrix}$ given in RVIN. Then:

$$|V| = \sqrt{\dot{X}^2 + \dot{Y}^2 + \dot{Z}^2}$$

$$\Gamma = \sin^{-1} \frac{\dot{X}'}{V} \quad -90^\circ \leq \Gamma \leq 90^\circ$$

$$\Sigma = \tan^{-1} \frac{\dot{Y}'}{\dot{Z}'} \quad \left. \begin{array}{l} + 0 \text{ for } \dot{Z}' > 0 \\ + 180 \text{ for } \dot{Z}' \leq 0 \end{array} \right\}$$


```
* LABEL
* SYMBOL TABLE
CEC2017 SUBROUTINE RVOUT
SUBROUTINE RVOUT(A,B,C)
DIMENSION A(3),B(3), C(6),E(3),G(3),H(3)
ACOSF(X) = ATANF(SQRTF(1.-X**2)/X)
C(1) = FNORM(A)
C(4) = FNORM(B)
C(2) = ATANF(A(3)/SQRTF(A(1)**2+A(2)**2))
C(3)=ARKTNS(360,A(1),A(2))
4 F = DOT(A,B)
ARG = F/(C(1)*C(4))
C(5) = ACOSF(ARG)
IF (ARG) 5,6,6
5 C(5) = -1.5707963 - C(5)
GO TO 7
6 C(5) = 1.5707963 - C(5)
7 CALL CROSS(A,B,E)
EN=FNORM(E)
DO 12 I=1,3
12 E(I)=E(I)/EN
CALL CROSS(E,A,G)
GN = FNORM(G)
DO 8 I=1,3
8 G(I) = G(I)/GN
H(1) = 0.
H(2) = 0.
H(3) = 1.
CALL CROSS(H,A,E)
ARG = DOT(E,G)
EN = FNORM(E)
ARG = ARG/EN
C(6) = ACOSF(ARG)
IF (G(3)) 9,10,10
9 C(6) = C(6) + 1.5707963
GO TO 11
10 C(6) = -C(6) + 1.5707963
11 CONTINUE
C(2) = C(2)*57.29578
C(3) = C(3)*57.29578
C(5) = C(5)*57.29578
C(6) = C(6)*57.29578
RETURN
END
```

```
RVOT
RVOT
RVOT
RVOT000
RVOT001
RVOT002
RVOT003
RVOT004
RVOT005
RVOT006
RVOT007
RVOT008
RVOT009
RVOT010
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RVOT022
RVOT023
RVOT024
RVOT025
RVOT026
RVOT027
RVOT028
RVOT029
RVOT030
RVOT031
RVOT032
RVOT033
RVOT034
RVOT035
RVOT036
RVOT037
RVOT038
RVOT039
RVOT
```

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Subroutine: SDEC

Purpose: To compute the total perturbation accelerations due to earth's oblateness, perturbing bodies, and Encke perturbations due to deviations from reference conic. These perturbations are obtained by calling OBLN, BODY, and ENCKE and placed in the T block for use in the integration package.

Calling Sequence:

CALL _____

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I					Quantities obtained from common
O					Quantities placed in common

Common storages used or required:

T, S, C, IC

Subroutines required:

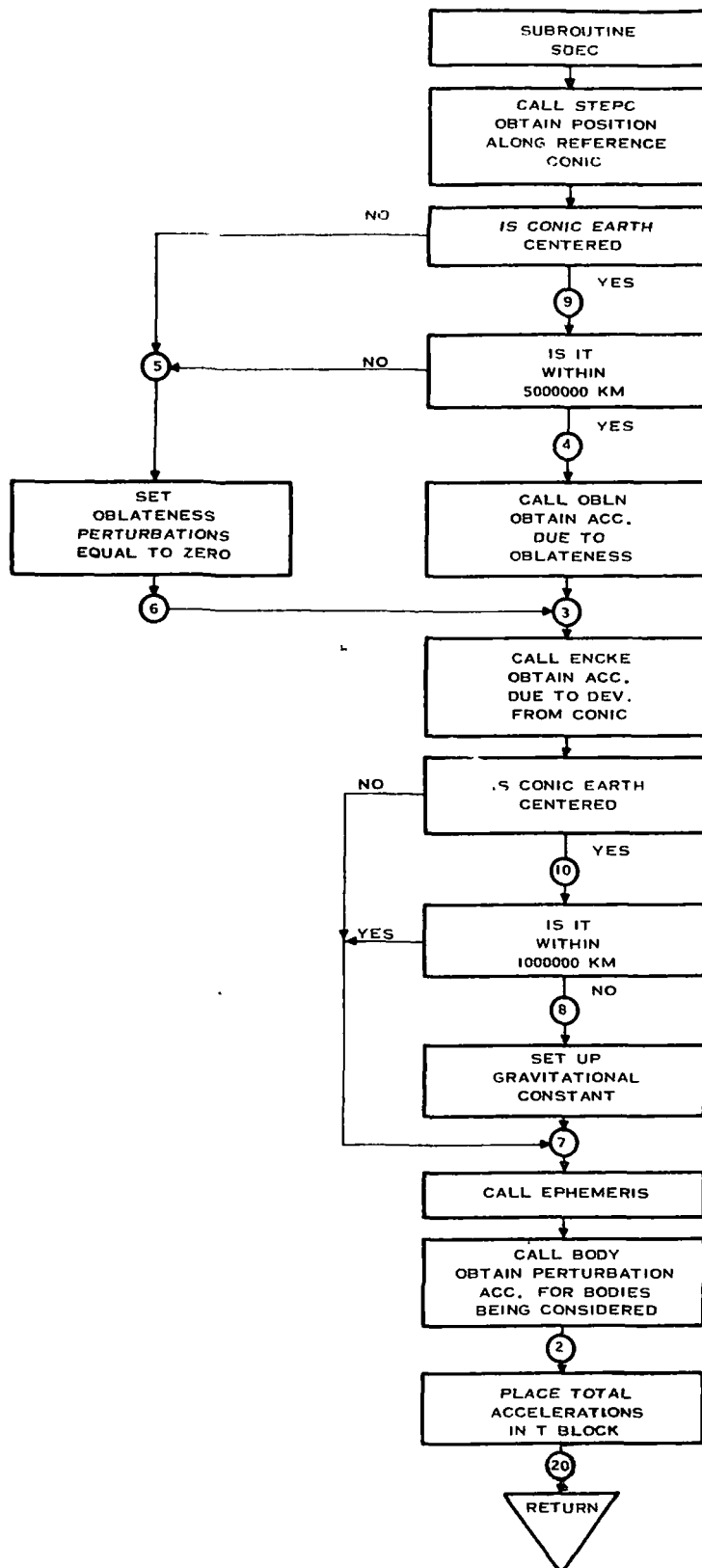
BODY, ENCKE, INTR, OBLN, STEP

Functions required:

None

Approximate number of storages required:

195 DEC



```
* LABEL
* SYMBOL TABLE
CEC2024 SUBROUTINE SDEC
SUBROUTINE SDEC
DIMENSION T(1360),S(1000),C(1000),IC(1)
DIMENSION RAD(3), X(3),VX(3),XP(3),
1 AE(3),AO(3),AP(3),PO(22),VE(22),CA(3),VKB(6),
2 RBO(6),RBOP(6) ,UM(6),VXP(3),AN(3,3),EN(3,3),EA(3,3)
3,BP(3,3) ,XSO(3),VXSO(3)
COMMON T,S,C,IC
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM)
EQUIVALENCE (S(11),VJ),(S(12),H),(S(13),D),(S(900),RAD)
EQUIVALENCE (C(10),TW),(C(11),TF),(C(13),TP1),(C(14),TP2)
1,(C(15),XP),(C(18),VXP),(C(21),AE),(C(24),AO),(C(27),CA)
2,(C(33),X),(C(36),VX)
4,(C(55),U),(C(56),VKB),(C(62),PO),(C(84),VE),(C(106),RBO) -
5,(C(112),RBOP),(C(120),EN),(C(129),EA),(C(138),AN),(C(171),BP)
7,(IC(1),N),(IC(2),IOR),(IC(3),NOR),(IC(4),KSTP),(IC(5),KTYPE)
8,(IC(6),ITARG),(S(14),RE),(C(46),XSO),(C(49),VXSO),(IC(231),NSTEP)
NEQ=3*N
CALL STEPC(NSTEP,T(2),XSO,VXSO,U,X,VX)
DO 1 I=1,3
1 XP(I) = X(I) + T(I+3)
IF(NOR=1)5,9,5
9 IF (RBOP-500000.) 4,5,5
4 CALL OBLN(XP,U,RE,VJ,H,D,AO,AN,BP,NEQ)
GO TO 3
5 DO 6 I=1,3
AO(I)=0.
DO 6 J=1,3
BP(I,J)=0.
6 CONTINUE
3 CALL ENCKE(U,X,T(4),AE)
IF(NOR=1)7,10,7
10 IF (RBOP-1000000.) 7,8,8
8 VKB(6) = UM(6)
7 NV = 0
NR1=NOR=1
TP2 = TF+T(2)/86400.
TWGN=0.
21 CONTINUE
IF(TP2)22,23,23
22 CONTINUE
TP2=TP2+1.
TWGN=TWGN-1.
GO TO 21
23 CONTINUE
TFP = INTF(TP2)
TP2 = TP2-TFP
TP1=TW+TFP+TWGN
CALL INTR(TP1,TP2,NR1,PO,NV,VE,RBOP)
```

SDEC (cont'd)

WDL-TR218

```
CALL BODY(XP,PO,VKB,RBO,RBOP,CA,NOR,BP,T,NEQ,U)
KJ=2*NEQ+3
DO 2 I=1,3
KI=KJ+I
2 T(KI) = AO(I) + AE(I) -CA(I)
20 RETURN
END
```

SDEC0480
SDEC0490
SDEC0500
SDEC0510
SDEC0520
SDEC0530
SDEC

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SDEC - 4

Subroutine: SETN

Purpose: SETN sets the logical tape numbers for input and output to conform with the system unit table.

Calling Sequence: _____

CALL SETN (NIN, NOUT) _____

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
0	NIN	1			Logical input tape unit
0	NOUT	1			Logical output tape unit

Common storages used or required:

None _____

Subroutines required:

None _____

Functions required:

None _____

Approximate number of storages required: _____

SETN

WDL-TR

* LABEL
CEC2023

SUBROUTINE SETN(NIN,NOUT)
C CALLING THIS SUBROUTINE RESULTS IN THE USE OF
C INPUT TAPE 2 AND OUTPUT TAPE 3
C USER MUST READ INPLT TAPE NIN, AND WRITE OUTPUT NOUT,
NIN=2
NOUT=3
RETURN
END

SETN
SETN0000
SETN001
SETN002
SETN0030
SETN004
SETN005
SETN0060
SETN0070
SETN

Subroutine: SHIFTP

Purpose: To change position and velocity coordinates from a coordinate system centered at body IOR to one centered at body NOR. SHIFTP also returns the new gravitational constant and the position and velocity of all bodies on the ephemeris tape referenced to the new center. (The latter is done by calling the ephemeris subroutine INTRI)

Calling Sequence:

CALL SHIFTP (IOR, NOR, U, UM, X, VX, PO, VE, TP1, TP2)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	IOR	1			Index of old central body
I	NOR	1			Index of new central body
O	U	1	μ	Km ³ /sec ²	Gravitational constant, body NOR
I	UM	6			Array of gravitational constants
I-O	X	3	X, Y, Z	Km	Positions } * w.r.t. body input: IOR
I-O	VX	3	$\dot{X}, \dot{Y}, \dot{Z}$	Km/sec	Velocities } w.r.t. body output: NOR
O	PO	22		Km	Positions of bodies on tape w.r.t.
O	VE	22		Km/sec	Velocities body NOR
I	TP1	1		seconds	Double precision time in sec-
I	TP2	1		seconds	onds since 1950.

Common storages used or required:

None

Subroutines required:

INTRI

Functions required:

None

Approximate number of storages required:

* with respect to

The sequence used in shifting centers is the following:

IOR (NOR)	CENTRAL BODY
1	Earth
2	Moon
3	Sun
4	Venus
5	Mars
6	Jupiter

```

* LABEL
* SYMBOL TABLE
SUBROUTINE SHIFTP(IOR,NOR,U,UM,X,VX,PO,VE,TF,TW,T2)
COMMON T,S,C,IC
DIMENSION T(1360),S(1000),C(1000),IC(1)
DIMENSION UM(6),X(3),VX(3),PO(22),VE(22)
EQUIVALENCE (T,TDUM),(S,SDUM),(C,CDUM),(C(14),TP2),(C(13),TP1)
N = NOR
IO = IOR
IOR = NOR
U = UM(N)
NV = 1
DIS = 1.E10
NR1 = NOR-1
CALL INTR1(TP1,TP2,NR1,PO,NV,VE,DIS)
DO 1 I=1,3
  J = 26-3*IO-I
  X(I) = X(I)+PO(J)
1 VX(I) = VX(I)+VE(J)
RETURN
END

```

```

SHTP
SHTP
SHTP000
SHTP001
SHTP002
SHTP003
SHTP004
SHTP005
SHTP006
SHTP007
SHTP008
SHTP009
SHTP010
SHTP011
SHTP012
SHTP013
SHTP014
SHTP015
SHTP016
SHTP017
SHTP

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Subroutine: STEPC

Purpose: To obtain the state, i.e., radius vector, R, and velocity vector, V, of a probe which is separated by a time increment, t, from a specified state, R_0 and V_0 , assuming an inverse-square central force law with gravitational constant u.

Calling Sequence:

CALL STEPC (N, T, R, V, U, RR, VV)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	N	1			Initializing index
I	T	1	Δt	sec	Incremental time
I	R	3	\vec{X}_0	Km	Initial Conic position (t_0)
I	V	3	$\dot{\vec{X}}_0$	Km/sec	Initial Conic Velocity (t_0)
I	U	1	μ	Km^3/sec^2	Gravitational constant
O	RR	3	\vec{X}	Km	Position on Conic ($t_0 + \Delta t$)
O	VV	3	$\dot{\vec{X}}$	Km/sec	Velocity on Conic ($t_0 + \Delta t$)

Common storages used or required:

None

Subroutines required:

DOT, GOTOR

Functions required:

ARKTNS, SQRT

Approximate number of storages required:

255 DEC

*Discussion

The inverse-square central force law is characterized by the equations

$$\begin{aligned}\dot{R} &= \frac{dR}{dt} = V \\ \dot{V} &= \frac{dV}{dt} = -\frac{u}{r^3} R\end{aligned}\quad (1)$$

where r is defined to be $+(R \cdot R)^{1/2}$.

The angular momentum vector, H , defined by the vector cross-product

$$H = R \times V \quad (2)$$

is a constant with respect to time, as seen by

$\dot{H} = \dot{R} \times V + R \times \dot{V} = V \times V + R \times \left(\frac{-u}{r^3} R \right) = 0$, so that $H = H_0 = R_0 \times V_0$. Because the magnitude, h_0 , of H_0 is generally nonzero, the plane equations

$$\begin{aligned}R \cdot H &= R \cdot H_0 = 0 \\ V \cdot H &= V \cdot H_0 = 0\end{aligned}\quad (3)$$

which follow from the definition of H , lead to the conclusion that all motion occurs in the plane normal to H_0 . That is, if R_0 and V_0 are non-zero and noncollinear vectors, any other vectors, such as R and V , must lie in the plane formed by R_0 and V_0 . Algebraically, one says that R and V may be expressed as linear combinations of R_0 and V_0 .

$$\begin{aligned}R &= f R_0 + g V_0 \\ V &= \dot{f} R_0 + \dot{g} V_0\end{aligned}\quad (4)$$

* Vectors will be denoted by capital letters and scalars by lower-case letters with the single exception of the rather standard symbol, E , for eccentric anomaly.

The second of equations (4) follows from (1) and from the fact that R_0 and V_0 are not functions of the time increment, t . The scalars, f , \dot{f} , g , and \dot{g} , are functions of R_0 , V_0 , and t . The discussion which follows concerns the determination of these scalars.

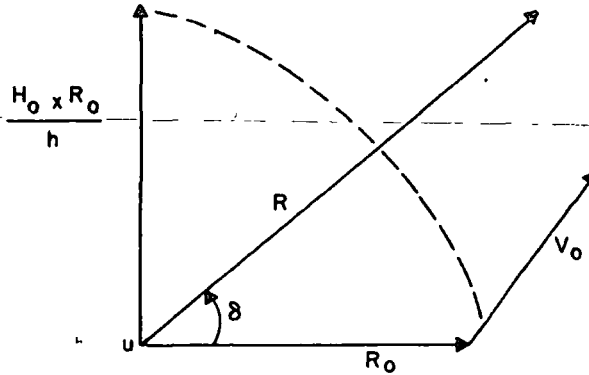


FIG 1

The vector $(H_0 \times R_0)/h$ is seen to be perpendicular to R_0 and to have the same magnitude, r_0 , as R_0 . Figure 1 shows that R may be written as the linear combination,

$$R = \frac{r}{r_0} \left[R_0 \cos \delta + \frac{H_0 \times R_0}{h} \sin \delta \right] \quad (5)$$

Equation (5) may be rewritten by expanding the vector triple cross-product,

$$H_0 \times R_0 = (R_0 \times V_0) \times R_0 = V_0 (R_0 \cdot R_0) - R_0 (R_0 \cdot V_0).$$

$$R = \frac{r}{r_0} \left[R_0 \left(\cos \delta - \frac{R_0 \cdot V_0}{h} \sin \delta \right) + V_0 \frac{r_0^2}{h} \sin \delta \right] \quad (5a)$$

Comparing equation (5a) with equation (4),

$$f = \frac{r}{r_o} \left(\cos \delta - \frac{R_o \cdot V_o}{h} \sin \delta \right)$$

$$g = \frac{rr_o}{h} \sin \delta. \quad (6)$$

At this point, the reader should note that while r_o , $R_o \cdot V_o$, and h are computable directly from R_o and V_o , the quantities r and δ have not been specifically defined in terms of R_o , V_o , and t . In order to do so, it is necessary to examine the conic solution to the inverse-square law equations of motion.

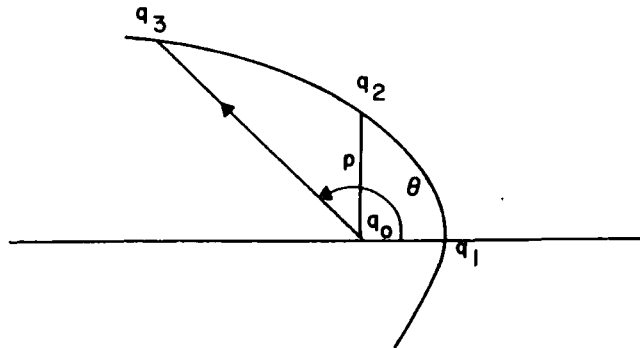


FIG 2

Figure 2 shows a conic section with focus at q_o and pericenter at q_1 . The point q_3 on the conic is specified, in polar coordinates originating at q_o , by the radius, r , and true anomaly, θ , θ being measured positive counter-clockwise from the line $q_o q_1$. The length $q_o q_2$ is called the semi-latus rectum and is denoted by p . The parameter specifying the shape of the conic is the eccentricity, e , which may be calculated from the equation

$$e = \frac{q_o q_2}{q_o q_1} - 1. \quad \text{The conic equation in an often-used form is,}$$

$$r = \frac{p}{1 + e \cos \theta} \quad (7)$$

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STPC - 4

Conic sections are characterized by eccentricity as follows:

circular	if	$e = 0$
elliptical	if	$0 < e < 1$
parabolic	if	$e = 1$
hyperbolic	if	$e > 1$

The two cases of great interest here are the elliptical and hyperbolic cases. Figure 3 below shows an ellipse.

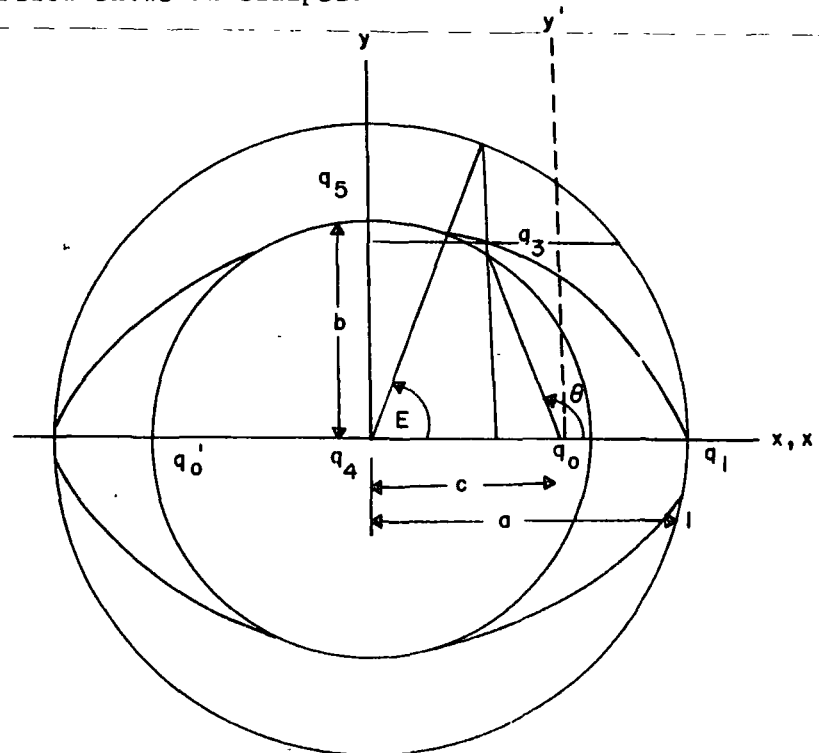


FIG. 3

The semi-major axis, a , is the distance from the point of symmetry, q_4 , to the pericenter, q_1 . The semi-minor axis, b , is the length $\overline{q_4 q_5}$. The eccentricity is equal to the ratio

$$c/a = \frac{\sqrt{a^2 - b^2}}{a}$$

The eccentric anomaly, E , is the argument of the projection of the point, q_3 , from the line $\overline{q_4 q_1}$ onto a circle of radius, a , concentric with the ellipse. That is, the Cartesian coordinates of q_3 relative to q_4 are

$$\begin{aligned} x &= a \cos E \\ y &= b \sin E \end{aligned} \quad (8)$$

Equations (8) give rise to the familiar equation of the ellipse

$$\frac{x^2}{a^2} + \frac{y^2}{b^2} = \cos^2 E + \sin^2 E = 1.$$

Relative to coordinates centered at q_0 , q_3 is described by

$$\begin{aligned} x' &= r \cos \theta = a \cos E - ea \\ y' &= y = r \sin \theta = b \sin E = a \sqrt{1-e^2} \sin E. \\ r &= x'^2 + y'^2 = a(1-e \cos E) \end{aligned} \quad (8a)$$

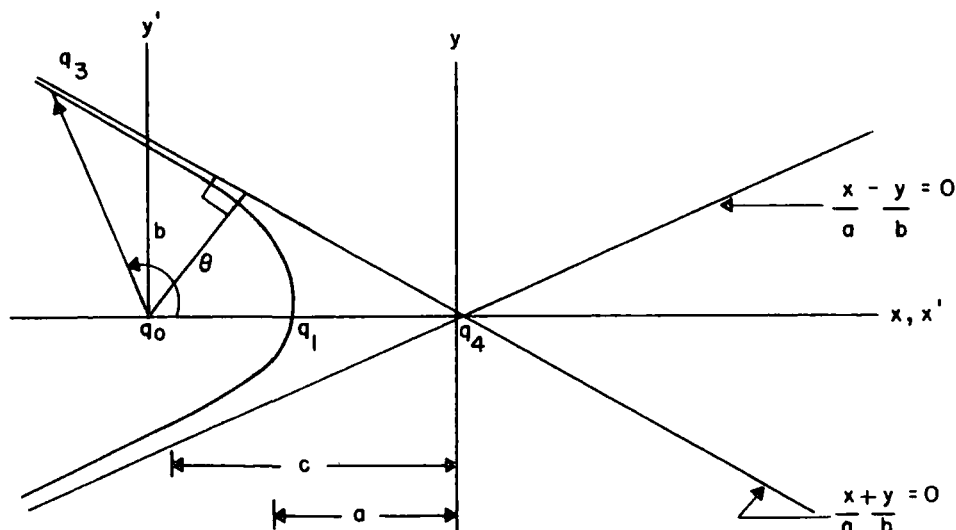


FIG 4

Figure 4 shows a conic section which is hyperbolic. The lines $\frac{x}{a} - \frac{y}{b} = 0$ and $\frac{x}{a} + \frac{y}{b} = 0$ are the asymptotes of the hyperbola. The semi-major axis, a , is again the distance from the point of symmetry, q_4 , to the pericenter, q_1 . The semi-minor axis, b , is defined as the distance from the focus, q_0 , to one of the asymptotes. Eccentricity is given by the ratio

$$c/a = \sqrt{\frac{a^2 + b^2}{a^2}}.$$

The eccentric anomaly, E , (sometimes called F) is too difficult to picture to be included in Fig. 4. E is defined in such a way that q_3 is described in Cartesian coordinates by

$$\begin{aligned} x &= -a \cosh E \\ y &= b \sinh E, \end{aligned} \tag{9}$$

leading to the familiar hyperbolic equation

$$\frac{x^2}{a^2} - \frac{y^2}{b^2} = \cosh^2 E - \sinh^2 E = 1$$

The Cartesian coordinates of q_3 relative to q_0 are given by

$$\begin{aligned} x' &= r \cos \theta = ea - a \cosh E \\ y' &= r \sin \theta = b \sinh E = a \sqrt{e^2 - 1} \sinh E. \\ r &= \sqrt{x'^2 + y'^2} = a(e \cosh E - 1) \end{aligned} \tag{9a}$$

Solution of the differential equations (1) yields p , a , and e as constants of the motion.

It is easily verified that

$$h = \sqrt{r_o^2 v_o^2 - (R_o \cdot v_o)^2} = r^2 \dot{\theta} \quad \text{angular momentum magnitude}$$

$$p = h^2/u \quad \text{semi-latus rectum}$$

$$a = \frac{r_o}{\left| 2 - \frac{r_o v_o^2}{u} \right|} \quad \text{semi-major axis}$$

$$e^2 = 1 - p/a \quad \text{eccentricity}$$

$$n = \sqrt{u/a^3} \quad \text{mean motion}$$

It should be observed that p is non-negative so that a negative semi-major axis corresponds to an eccentricity greater than one; that is, to the hyperbolic case. Some useful identities are listed as equations (11).

$$\frac{R \cdot V}{r} = \frac{d}{dt} (R \cdot R)^{1/2} = \dot{r} = \frac{ep\theta \sin\theta}{(1+e\cos\theta)^2} = \frac{ue}{h} \sin\theta$$

$$\cos\theta = \mp \frac{a}{r} (cE - e)$$

$$\sin\theta = \frac{a}{r} \sqrt{|e^2 - 1|} \quad sE = \sqrt{\frac{a}{u}} \frac{h}{r} \quad sE$$

$$esE = \frac{R \cdot V}{\sqrt{ua}}$$

$$ecE = 1 \pm \frac{r}{a} \quad (11)$$

The convention has been adopted that when a double sense sign \pm is used, the upper pertains to the hyperbolic case and the lower to the elliptical.

The symbols sE and cE mean $\sin E$ and $\cos E$ for the elliptical case, but $\sinh E$ and $\cosh E$ for the hyperbolic case. Hence, if we let

$\Phi = E - E_0$, it follows that

$$s\Phi = sEcE_0 - cEsE_0$$

$$c\Phi = cEcE_0 + sEsE_0$$

and

$$sE = s\Phi cE_0 + c\Phi sE_0$$

$$cE = c\Phi cE_0 + s\Phi sE_0 \quad (12)$$

This angle, δ , of equation (5) is seen to represent the incremental true anomaly on the conic section containing R_0 and R . Thus, we can

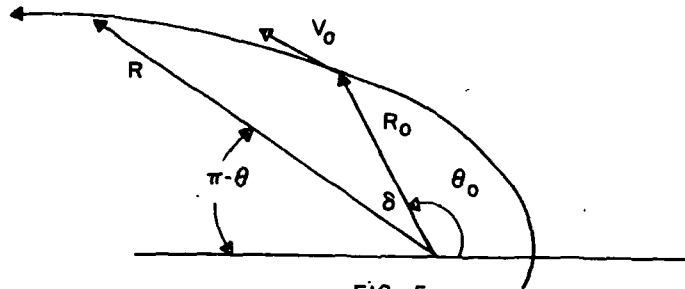


FIG. 5

find expressions for $\sin \delta$ and $\cos \delta$ in terms of θ and θ_0 .

$$\sin \delta = \sin (\theta - \theta_0) = \sin \theta \cos \theta_0 - \cos \theta \sin \theta_0$$

$$\cos \delta = \cos (\theta - \theta_0) = \cos \theta \cos \theta_0 + \sin \theta \sin \theta_0. \quad (13)$$

The incremental true anomaly may now be related to R_0 and V_0 through substitution of equations (11) and (12) into (13).

$$\begin{aligned}
\sin \delta &= \sin \theta \cos \theta_o - \cos \theta \sin \theta_o \\
&= \sqrt{\frac{a^3}{u}} \frac{h}{rr_o} (\mp s E c E_o \pm e s E \mp e s E_o \pm c E s E_o) \\
&= \frac{h}{nrr_o} (\mp s \phi \pm e s E \mp e s E_o) \\
&= \frac{h}{nrr_o} (\mp s \phi \pm e c E_o s \phi \pm e s E_o c \phi \mp e s E_o) \\
&= \frac{h}{nrr_o} \left(\frac{r_o}{a} s \phi \pm \frac{R_o \cdot V_o}{\sqrt{ua}} (c \phi - 1) \right)
\end{aligned}$$

$$\begin{aligned}
\cos \delta &= \cos \theta \cos \theta_o + \sin \theta \sin \theta_o \\
&= \frac{a^2}{rr_o} \left[c E c E_o - e c E - e c E_o + e^2 \pm (e^2 - 1) s E s E_o \right] \\
&= \frac{a^2}{rr_o} \left[c \phi - e c E - e c E_o + e^2 \pm e^2 s E s E_o \right] \\
&= \frac{a^2}{rr_o} \left[c \phi - e c \phi c E_o \mp e s \phi s E_o - e c E_o + e^2 \pm e^2 s E_o c E_o s \phi \pm e^2 s^2 E_o c \phi \right] \\
&= \frac{a^2}{rr_o} \left[\mp \frac{r_o}{a} c \phi + \frac{r_o}{a} \frac{R_o \cdot V_o}{\sqrt{ua}} s \phi + 1 \pm \frac{p}{a} - 1 \mp \frac{r_o}{a} \pm \frac{(R_o \cdot V_o)^2}{ua} c \phi \right] \\
&= \frac{a^2}{rr_o} \left[\mp \frac{r_o}{a} (c \phi + 1) + \frac{r_o}{a} \frac{R_o \cdot V_o}{\sqrt{ua}} s \phi \pm \frac{r_o^2 v_o^2}{ua} \pm \frac{(R_o \cdot V_o)^2}{ua} (c \phi - 1) \right] \\
&= \frac{a^2}{rr_o} \left[\mp \frac{r_o}{a} (c \phi - 1) + \frac{r_o}{a} \frac{R_o \cdot V_o}{\sqrt{ua}} s \phi + \frac{r_o}{a} \left(\frac{r_o v_o^2}{u} - 2 \right) \right. \\
&\quad \left. \pm \frac{(R_o \cdot V_o)^2}{ua} (c \phi - 1) \right] \\
&= \frac{a^2}{rr_o} \left[\mp \left[\frac{(R_o \cdot V_o)^2}{ua} - \frac{r_o}{a} \right] (c \phi - 1) + \frac{r_o}{a} \frac{R_o \cdot V_o}{\sqrt{ua}} s \phi + \frac{r_o^2}{a^2} \right]
\end{aligned}$$

The coefficients, f and g , of equation (6) are finally found to be:

$$\begin{aligned}
 f &= \frac{r}{r_o} \left(\cos \delta - \frac{R_o \cdot V_o}{h} \sin \delta \right) \\
 &= \frac{a^2}{r_o^2} \left[\pm \left[\frac{(R_o \cdot V_o)^2}{ua} - \frac{r_o}{a} - \frac{(R_o \cdot V_o)^2}{ua} \right] (c\Phi - 1) + \frac{r_o}{a} \left[\frac{R_o \cdot V_o}{\sqrt{ua}} - \frac{R_o \cdot V_o}{\sqrt{ua}} \right] s\Phi \right. \\
 &\quad \left. + \frac{r_o^2}{a^2} \right] = \mp \frac{a}{r_o} (c\Phi - 1) + 1
 \end{aligned} \tag{14}$$

$$\begin{aligned}
 g &= \frac{rr_o}{h} \sin \delta \\
 &= \frac{1}{n} \frac{r_o}{a} s\Phi + \frac{R_o \cdot V_o}{\sqrt{ua}} (c\Phi - 1)
 \end{aligned} \tag{15}$$

The velocity coefficients, \dot{f} and \dot{g} , are found by noting that

$$\dot{\Phi} = \dot{E} = \sqrt{\frac{u}{a}} \frac{1}{r}$$

$$\text{and therefore } \dot{f} = \mp \frac{a}{r_o} \frac{d}{dt} (c\Phi) = - \frac{a}{r_o} \dot{E} s\Phi = - \frac{\sqrt{ua}}{rr_o} s\Phi \tag{16}$$

$$\begin{aligned}
 \dot{g} &= \frac{\dot{E}}{n} \left(\frac{r_o}{a} c\Phi + \frac{R_o \cdot V_o}{\sqrt{ua}} s\Phi \right) \\
 &= \frac{a}{r} \left(\frac{r_o}{a} c\Phi + \frac{R_o \cdot V_o}{\sqrt{ua}} s\Phi \right)
 \end{aligned} \tag{17}$$

where

$$\begin{aligned}
 \frac{r}{a} &= \mp (1 - ecE) = \mp (1 - ec\Phi cE_o \mp es\Phi sE_o) \\
 &= \mp \left(1 - c\Phi \left(1 \pm \frac{r_o}{a} \right) \mp s\Phi \frac{R_o \cdot V_o}{\sqrt{ua}} \right) \\
 &= \pm (c\Phi - 1) + \frac{r_o}{a} c\Phi + \frac{R_o \cdot V_o}{\sqrt{ua}} s\Phi
 \end{aligned} \tag{18}$$

Kepler's equation presents the incremental time, t , in terms of Φ

$$\begin{aligned}
 nt &= \bar{r} (E - esE) \pm (E_0 - esE_0) \\
 &= \bar{r} (\Phi - esE + esE_0) \\
 &= \bar{r} (\Phi - es\Phi cE_0 - ec\Phi sE_0 + esE_0) \\
 &= \bar{r} \left[\Phi - s\Phi \left(1 \pm \frac{r_0}{a} \right) - (c\Phi - 1) \frac{R_0 \cdot V_0}{\sqrt{ua}} \right] \\
 &= \bar{r} (\Phi - s\Phi) + \frac{r_0}{a} s\Phi \pm \frac{R_0 \cdot V_0}{\sqrt{ua}} (c\Phi - 1) \quad (19)
 \end{aligned}$$

In order to solve equation (19) for Φ as a function of R_0 , V_0 and t , an iterative method is required. Any solution obtained is necessarily unique, since the right side of (19) is seen to be monotonically increasing for all Φ .

Equation (19) may be used to simplify equations (15) and (17).

$$\begin{aligned}
 g &= \frac{1}{n} \left[\frac{r_0}{a} s\Phi + nt \pm (\Phi - s\Phi) - \frac{r_0}{a} s\Phi \right] \\
 &= t \pm \frac{1}{n} (\Phi - s\Phi) \quad (15a)
 \end{aligned}$$

$$\begin{aligned}
 \dot{g} &= 1 \pm \frac{\dot{E}}{n} (1 - c\Phi) \\
 &= 1 \mp \sqrt{\frac{u}{a}} \frac{1}{nr} (c\Phi - 1) \\
 &= 1 \mp \frac{a}{r} (c\Phi - 1) \quad (17a)
 \end{aligned}$$

Subroutine Description

The subroutine will calculate

$$(1) \quad R = R(R_o, V_o, t)$$

$$V = V(R_o, V_o, t)$$

$$\delta = \delta(R_o, V_o, t)$$

The first time STEP is called with a given R_o and V_o ($N=1$), those coefficients which are dependent only on R_o and V_o are calculated. Thereafter, these coefficients are considered to be constants with respect to t .

CalculationFORTAN Name

$$r_o = \sqrt{R_o \cdot R_o}$$

RM

$$v_o = \sqrt{V_o \cdot V_o}$$

VM

$$a = \frac{r_o}{\left| 2 - \frac{r_o v_o^2}{u} \right|}$$

A

$$n = \frac{1}{a} \sqrt{\frac{u}{a}}$$

RAT

$$R_o \cdot V_o = R_o \cdot V_o$$

RV

$$h = \sqrt{r_o^2 v_o^2 - (R_o \cdot V_o)^2}$$

H

STEPC calls Subroutine GOTOR to solve equation (19),

$$nt = \bar{r} (\bar{\phi} - s\bar{\phi}) + \frac{r_o}{a} s\bar{\phi} + \frac{R_o \cdot V_o}{\sqrt{ua}} (c\bar{\phi} - 1) \text{ for } \bar{\phi}.$$

GOTOR returns a vector F where

	<u>Elliptical</u>	<u>Hyperbolic</u>
F(1) =	$\bar{\phi} - \sin \bar{\phi}$	$\sinh \bar{\phi} - \bar{\phi}$
F(2) =	$1 - \cos \bar{\phi}$	$\cosh \bar{\phi} - 1$
F(3) =	$\sin \bar{\phi}$	$\sinh \bar{\phi}$
F(4) =	$\cos \bar{\phi}$	$\cosh \bar{\phi}$

The coefficients, f, g, \dot{f} and \dot{g} , are then calculated.

<u>Calculation</u>	<u>FORTTRAN Name</u>
$f = - \frac{r_o}{a} F(2) + 1$	EF
$g = - \frac{F(1)}{n} + t$	GE
$\frac{r}{a} = F(2) + \frac{r_o}{a} F(4) + \frac{R_o \cdot V_o}{\sqrt{ua}} F(3)$	ROA
$\dot{f} = - \frac{a n F(3)}{r_o} \frac{(r_o r)}{a}$	EFD
$\dot{g} = - \frac{a}{r} F(2) + 1$	GED
$\delta = \tan^{-1} \frac{hg}{f_o^2 f + R_o \cdot V_o g}$	TA
$R = fR_o + gV_o$	RR
$V = \dot{f}R_o + \dot{g}V_o$	VV

Reference: NASA X-640-63-71, ITEM Program Manual, Goddard Space Flight Center, Greenbelt, Maryland.

```

      LABEL
      * SYMBOL TABLE
CEC2023 SUBROUTINE STEPC
      SUBROUTINE STEPC(N,T,R,V,U,RR,VV)
      DIMENSION R(3),V(3),RR(3),VV(3),C(2),F(4)
      GO TO (1,2),N
      1 CONTINUE
      PI=3.141592654
      R2=DOT(R,R)
      RM=SQRTF(R2)
      V2=DOT(V,V)
      RV=DOT(R,V)
      VM=SQRTF(V2)
      A=RM/(2,-RM*V2/U)
      ABA=ABSF(A)
      RAT=SQRTF(U/ABA)/ABA
      C(1)=RM/ABA
      C(2)=RV/SQRTF(U+ABA)
      IF(A)3,3,4
      4 CONTINUE
      K=1
      E1=RAT*T
      GO TO 15
      3 CONTINUE
      K=2
      E1=0.
      15 CONTINUE
      2 CONTINUE
      T IS THE INCREMENTAL TIME IN ORBIT
      EMDT=RAT*T
      CALL GOTOR(K,EMDT,C,F,E1)
      EF=-F(2)/C(1)+1,
      GE=-F(1)/RAT*T
      TA=ARKTNS(360,R2*EF+RV*GE,H*GE)
      ROA=F(2)+C(1)*F(4)+C(2)*F(3)
      EFD=-ABA*RAT*F(3)/(RM*ROA)
      GED=-F(2)/ROA+1,
      8 CONTINUE
      DO 10 I=1,3
      RR(I)=EF*R(I)+GE*V(I)
      VV(I)=EFD*R(I)+GED*V(I)
      10 CONTINUE
      RETURN
      END

```

```

STPC
STPC
STPC
STPC000
STPC001
STPC002
STPC003
STPC004
STPC005
STPC006
STPC007
STPC008
STPC009
STPC010
STPC011
STPC012
STPC013
STPC014
STPC015
STPC016
STPC017
STPC018
STPC019
STPC020
STPC021
STPC022
STPC023
STPC024
STPC025
STPC026
STPC027
STPC028
STPC029
STPC030
STPC031
STPC032
STPC033
STPC034
STPC035
STPC036
STPC037
STPC038
STPC039
STPC

```

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Subroutine: TIMEC

Purpose: To compute whole days and fractional days since January 1, 1950, from calendar date input. This input is in the form (Years from 1900) $\times 10^2 + (\text{Month of Year}) + (\text{Day of Month}) \times 10^{-2}$, and (Hour of Day) $\times 10^2 + (\text{Minutes of Hour}) + (\text{Seconds of Minute}) \times 10^{-2}$. [See examples under input description]. The input date must be 1961 or later.

Calling Sequence:

CALL TIMEC (T1, T2, T3, T4)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	T1	1			Year, month, day.
					Jan. 12, 1965 = 6501.12.
I	T2	1			Hour, minutes, seconds.
					1 PM, 1 min, 30.3 sec = 1301.303
O	T3	1		days	Whole number of days since 1950.
O	T4	1		days	Fractional number of days past
					T3.

Common storages used or required:

None

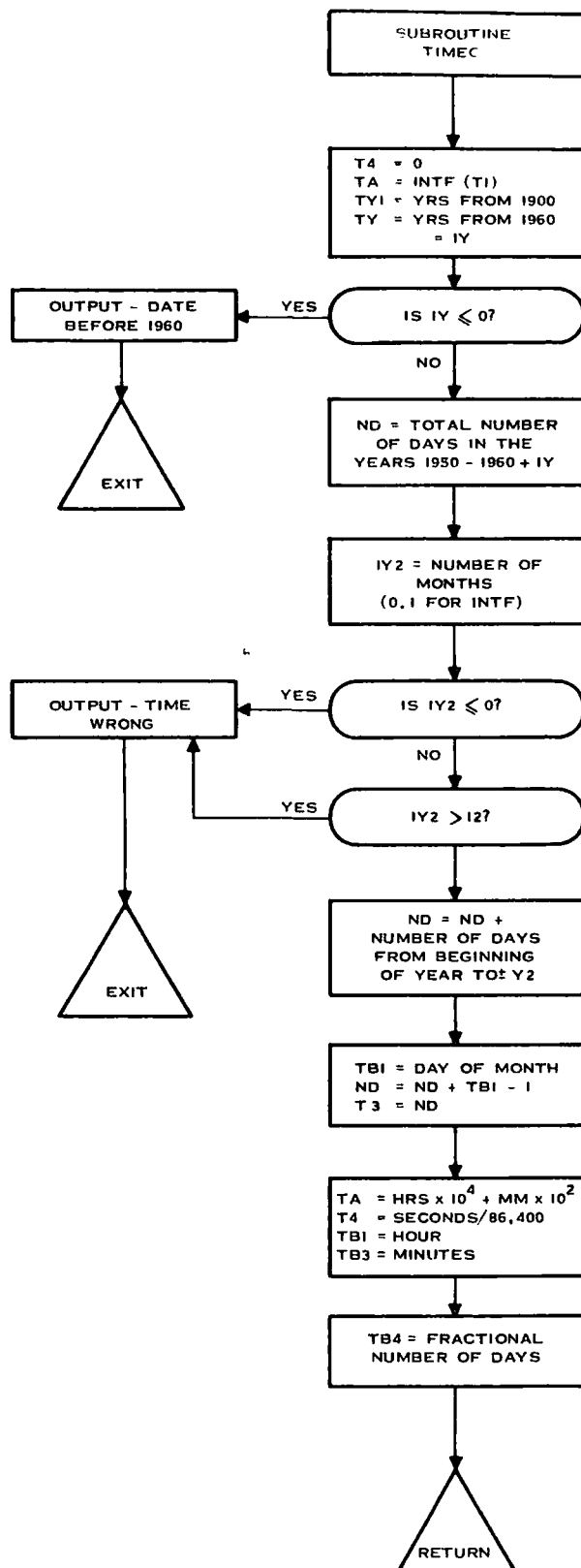
Subroutines required:

EXIT

Functions required:

INTF

Approximate number of storages required:



```

* LABEL
* SYMBOL TABLE
SUBROUTINE TIMEC(T1,T2,T3,T4)
T1 IS AN INPUT IN FORM (YEARS FROM 1900)(MONTH OF YEAR)
(DAY OF MONTH
WRITTEN AS 6501.12 FOR JAN. 12, 1965
T2 IS AN INPUT IN FORM (HOUR OF DAY)(MINUTE OF HOUR)
(SECOND OF MINUTE)
WRITTEN AS 1301.3032 FOR 1PM, 1 MINUTE, 30.32 SECOND
T3 IS WHOLE DAYS FROM 1950 OUTPUT
CALL SETN(NIN,NOUT)
T4=0.
TA=INTF(T1)
TA1=TA/100.+.01
TY1=INTF(TA1)
TY=TY1-60.
IY=TY
IF (IY) 15,15,16
15 CONTINUE
WRITE OUTPUT TAPE NOUT,17
17 FORMAT (37H EXIT FROM TIMEC. DATE 1960 OR BEFORE)
CALL EXIT
16 CONTINUE
ND=3652
K=1
DO 1 I=1, IY
KK=K-I
IF (KK) 2,2,3
2 CONTINUE
ND=ND + 366
K=K+4
GO TO 1
3 CONTINUE
ND=ND + 365
1 CONTINUE
TY2=TA-TY1*100.+.1
IY2=INTF(TY2)
IF (IY2) 10,10,11
11 CONTINUE
IF (12-IY2) 10,12,12
10 CONTINUE
WRITE OUTPUT TAPE NOUT,13
13 FORMAT(37H INPUT TIME IS WRONG. EXIT FROM TIMEC)
CALL EXIT
12 CONTINUE
DO 4 I=1,IY2
I=I
JAN FEB MAR APRIL MAY JUNE JULY AUG SEPT OCT NOV
GO TO (4,6,7,6,8,6,8,6,6,8,6,8),I
6 CONTINUE
ND=ND + 31

```

```

TIMC
TIMC
TIMC000
TIMC001
TIMC002
TIMC003
TIMC004
TIMC005
TIMC006
TIMC007
TIMC007
TIMC008
TIMC009
TIMC010
TIMC011
TIMC012
TIMC013
TIMC014
TIMC015
TIMC016
TIMC017
TIMC018
TIMC019
TIMC020
TIMC021
TIMC022
TIMC023
TIMC024
TIMC025
TIMC026
TIMC027
TIMC028
TIMC029
TIMC030
TIMC031
TIMC032
TIMC033
TIMC034
TIMC035
TIMC036
TIMC037
TIMC038
TIMC039
TIMC040
TIMC041
TIMC042
TIMC043
TIMC044
TIMC045
TIMC046
TIMC047

```

TIMEC (cont'd)

WDL-TR218

GO TO 4
7 CONTINUE
IF (KK-1) 9, 14, 9
14 CONTINUE
ND=ND +29
GO TO 4
9 CONTINUE
ND=ND +28
GO TO 4
8 CONTINUE
ND=ND +30
4 CONTINUE
TB1=(T1-TA)*100.+.1
ND=ND +XINTF(TB1)
ND=ND-1
T3=ND
TA=INTF(T2)
T4=(T2-TA)/864.
TB=TA/100.+.1
TB1=INTF(TB)
TB2=TA-TR1*100.+.1
TB3= INTF(TB2)
T4=T4+TB1/24.+TB3/24./60.
RETURN
END

TIMC0480
TIMC0490
TIMC0500
TIMC0510
TIMC0520
TIMC0530
TIMC0540
TIMC0550
TIMC0560
TIMC0570
TIMC0580
TIMC0590
TIMC0600
TIMC0610
TIMC0620
TIMC0630
TIMC0640
TIMC0650
TIMC0660
TIMC0670
TIMC0680
TIMC0690
TIMC0700
TIMC0710
TIMC

S-394

TIMEC - 4

Subroutine: TIMED

Purpose: To convert an input time from the format DAYS HOURS·MIN SEC to seconds. If the input is negative, it is assumed to be in seconds, and returned positive.

Calling Sequence:

CALL TIMED (T1, T2)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	T1	1		-seconds	or (DAYS + 10^2 + HOURS + MIN
					$\times 10^{-2}$ + SEC $\times 10^{-4}$)
O	T2	1		seconds	

Common storages used or required:

None

Subroutines required:

None

Functions required:

INTF

Approximate number of storages required:

TIMED

WDL-TR2

```
* LABEL
* SYMBOL TABLE
SUBROUTINE TIMED (T1,T2)
IF(T1)1,1,2
1 CONTINUE
T2=-T1
RETURN
C SUBROUTINE ACCEPTS T1 IN SEC IF THE SIGN IS INPUT NEGATIVE AND
C GIVES T2 IN + SEC IF T1 IS + AND ARRANGED AS (DAYS HOURS.MIN SEC)
C IT CONVERTS OUTPUT T2 TO SEC
2 CONTINUE
TDH=INTF(T1)
TMS=T1-TDH
TM1=TMS*100,+.01
TM=INTF(TM1)
TS=(TMS*100,-TM)*100,+.01
TD=INTF(TDH/100,+.01)
TH=TDH-TD*100,+.01
TH=INTF(TH)
TS=INTF(TS)
T2=TD*86400, +TH*3600, +TM*60, +TS
RETURN
END
```

```
TIMD
TIMD
TIMD0000
TIMD0010
TIMD0020
TIMD0030
TIMD0040
TIMD0050
TIMD0060
TIMD0070
TIMD0080
TIMD0090
TIMD0100
TIMD0110
TIMD0120
TIMD0130
TIMD0140
TIMD0150
TIMD0160
TIMD0170
TIMD0180
TIMD0190
TIMD
```

Subroutine: TRAC

Purpose: To obtain the vector from a body center to a tracking station and the unit up, east, and north vectors. The coordinate system is a rotating body fixed system. The body may be treated as an oblate spheroid.

Calling Sequence:

CALL TRAC (TO, AT, H, GHA, U, E, EN, RT, AC, SL, CL, ST, CT, A, B)

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
I	TO	1		RAD	Tracker longitude
I	AT	1		RAD	Tracker latitude
I	H	1		Km	Tracker Altitude
I	GHA	1		RAD	Greenwich hour angle
O	U	3	\hat{U}		Up unit vector
O	E	3	\hat{E}		East unit vector
O	EN	3	\hat{N}		North unit vector
O	RT	3			Radius vector to tracker

(Cont'd.)

Common storages used or required:

None

Subroutines required:

None

Functions required:

SIN, COS, SORT

Approximate number of storages required:

194 DEC

(Cont'd.)

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
O	AC	1			Constant used in program
O	SL	1			Sin LAT
O	CL	1			Cos LAT
O	ST	1			Sin LONG
O	CT	1			Cos LONG
I	A	1	R_E	Km	Body's equatorial radius
I	B	1	R_p	Km	Body's polar radius

Derivation of Vectors obtained in TRAC

A. Derivation of Unit U, E, and N

The coordinate system of concern is shown in Fig. 1 below.

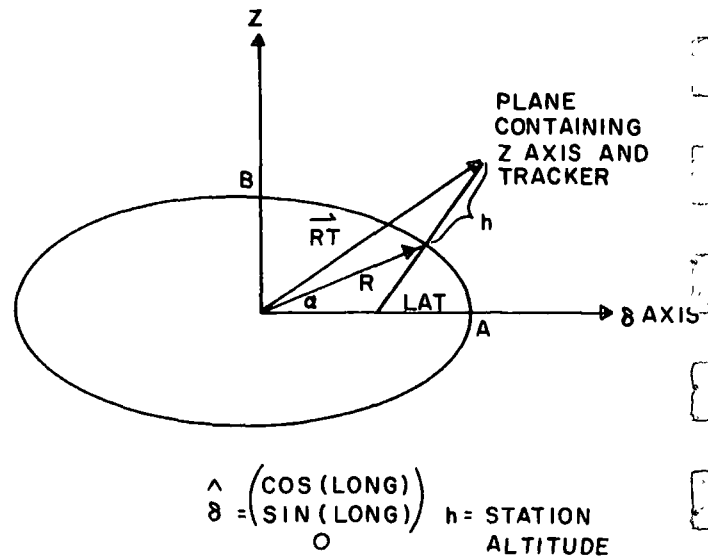
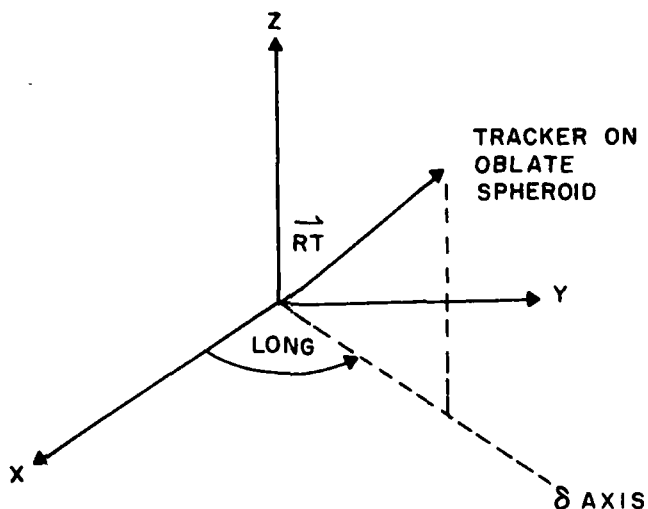


FIG 1

The unit up vector, U, may be written as:

$$\hat{U} = \begin{pmatrix} \cos(\text{LAT}) \cos(\text{LONG}) \\ \cos(\text{LAT}) \sin(\text{LONG}) \\ \sin(\text{LAT}) \end{pmatrix}$$

The unit east vector, E, is:

$$\hat{E} = \frac{\hat{K} \times \hat{U}}{|\hat{K} \times \hat{U}|} = \begin{pmatrix} -\sin(\text{LONG}) \\ \cos(\text{LONG}) \\ 0 \end{pmatrix}$$

The unit north vector, N, is:

$$\hat{N} = \hat{U} \times \hat{E} = \begin{pmatrix} -\sin(\text{LAT}) \cos(\text{LONG}) \\ -\sin(\text{LAT}) \sin(\text{LONG}) \\ \cos(\text{LAT}) \end{pmatrix}$$

B. Derivation of Radius Vector, RT, to Tracker.

$$\vec{RT} = \vec{R} + h \hat{U}$$

$$\vec{R} = |R| \cos \alpha \begin{pmatrix} \cos(\text{LONG}) \\ \sin(\text{LONG}) \\ 0 \end{pmatrix} + |R| \sin \alpha \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

Equation of ellipse in Z-δ plane

$$\frac{Z^2}{B^2} + \frac{\delta^2}{A^2} = 1$$

Substituting for Z, δ

$$R^2 \left(\frac{\sin^2 \alpha}{B^2} + \frac{\cos^2 \alpha}{A^2} \right) = 1$$

$$\frac{dZ}{d\delta} = - \frac{B^2}{A^2} \frac{\delta}{Z}$$

$$\tan(\text{LAT}) = \frac{A^2}{B^2} \frac{Z}{\delta}$$

$$\tan \alpha = \frac{Z}{\delta}$$

$$R = \frac{AB}{(A^2 \sin^2 \alpha + B^2 \cos^2 \alpha)^{1/2}} \quad \therefore \tan \alpha = \frac{B^2}{A^2} \tan(\text{LAT})$$

$$R \cos \alpha = \frac{A}{\left(\frac{A^2}{B^2} \tan^2 \alpha + 1\right)^{1/2}} \quad R \sin \alpha = \frac{B}{\left(1 + \frac{B^2}{A^2} \cot^2 \alpha\right)^{1/2}}$$

Substituting for $\tan \alpha$ yields

$$R \cos \alpha = \frac{A}{\left(\frac{B^2}{A^2} \tan^2(\text{LAT}) + 1\right)^{1/2}} \quad R \sin \alpha = \frac{B}{\left(1 + \frac{A^2}{B^2} \cot^2(\text{LAT})\right)^{1/2}}$$

$$RT(1) = \left\{ \frac{A}{\left[\frac{B^2}{A^2} \sin^2(\text{LAT}) + \cos^2(\text{LAT})\right]^{1/2}} + h \right\} U(1)$$

$$RT(2) = \left\{ \frac{A}{\left[\frac{B^2}{A^2} \sin^2(\text{LAT}) + \cos^2(\text{LAT})\right]^{1/2}} + h \right\} U(2)$$

$$RT(3) = \left\{ \frac{B^2}{\left[B^2 \sin^2(\text{LAT}) + A^2 \cos^2(\text{LAT})\right]^{1/2}} + h \right\} U(3)$$



* LABEL	TRAC
* SYMBOL TABLE	TRAC
CEC2009	TRAC
SUBROUTINE TRAC (TO,AT,H,GHA,U,E,EN,RT,AC,SL,CL,ST,CT,A,B)	TRAC0000
DIMENSION RT(3),U(3),E(3),EN(3)	TRAC0010
C TO AND LAT MUST BE INPUTED IN RAD,H IS ALTITUDE IN KM	TRAC0020
SL=SINF(AT)	TRAC0030
CL=COSE(AT)	TRAC0040
TA=TO+GHA	TRAC0050
C GHA IS GREENWICH HOUR ANGLE,U IS 'UP,E IS EAST,	TRAC0060
C EN IS NORTH UNIT VECTORS	TRAC0070
ST = SINF(TA)	TRAC0080
CT = COSE(TA)	TRAC0090
C = SQRTF(CL*CL+B*B*SL*SL/(A*A))	TRAC0100
AC=A/C	TRAC0110
U(1) = CL*CT	TRAC0120
U(2) = CL*ST	TRAC0130
U(3) = SL	TRAC0140
RT(1) = (A/C+H)*U(1)	TRAC0150
RT(2) = (A/C+H)*U(2)	TRAC0160
RT(3) = (B*B/(A*C)+H)*U(3)	TRAC0170
4 E(1) = -ST	TRAC0180
E(2) = CT	TRAC0190
E(3) = 0.	TRAC0200
EN(1) = -SL*CT	TRAC0210
EN(2) = -SL*ST	TRAC0220
EN(3) = CL	TRAC0230
RETURN	TRAC0240
END	TRAC

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Subroutine: TRANSH

Purpose: To transform the partial matrix from equator and equinox of date to equator and equinox of 1950. The logic key is used to indicate if the last three partials are zero (LL = 1) or if all six partials have values (LL = 2).

Calling Sequence:

CALL TRANSH

Input and Output

I/O	Symbolic Name or Location	Program Dimensions	Mathematical Symbol	Data Dimensions or Units	Definition
IO	H	(1,6)	$\frac{\partial \text{MEAS}}{\partial \text{STATE}}$		Partials of measurements WRT*
					the state
I	LL	1			Logic key
					* With Respect To

Common storages used or required:

T, S, C, IC

Subroutines required:

None

Functions required:

None

Approximate number of storages required:

TRANSH

WDL-TR 4

```
* LABEL
* SYMBOL TABLE
SUBROUTINE TRANSH(H,LL)
C SUBROUTINE TRANSFORMS H MATRIX TO EQUINOX 1950
EQUIVALENCE(T,TDUM),(S,SDUM),(C,CDUM),(C(138),AN)
DIMENSION H(6),AN(3,3),DUM(1,6),T(1360),S(1000),C(1000),IC(1)
COMMON T,S,C,IC
LL=LL
DO 1 I=1,3
K=I+3
DUM(I)=0.
DUM(K)=0.
DO 1 J=1,3
DUM(I)=DUM(I)+AN(J,I)*H(J)
GO TO(1,2),LL
2 CONTINUE
L=J+3
DUM(K)=DUM(K)+AN(J,I)*H(L)
1 CONTINUE
DO 3 I=1,6
H(I)=DUM(I)
3 CONTINUE
RETURN
END
```

TRAN
TRAN
TRAN000
TRAN001
TRAN0020
TRAN003
TRAN004
TRAN0050
TRAN0060
TRAN007
TRAN0080
TRAN0090
TRAN010
TRAN011
TRAN0120
TRAN013
TRAN014
TRAN0150
TRAN0160
TRAN017
TRAN018
TRAN0190
TRAN020
TRAN

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